

Sheffield Hallam University

Unidirectional solidification studies of ingot mould cast irons

HORNBY, Sara A.

Available from the Sheffield Hallam University Research Archive (SHURA) at:

<http://shura.shu.ac.uk/19826/>

A Sheffield Hallam University thesis

This thesis is protected by copyright which belongs to the author.

The content must not be changed in any way or sold commercially in any format or medium without the formal permission of the author.

When referring to this work, full bibliographic details including the author, title, awarding institution and date of the thesis must be given.

Please visit <http://shura.shu.ac.uk/19826/> and <http://shura.shu.ac.uk/information.html> for further details about copyright and re-use permissions.

101 381 276 X



269624

ProQuest Number: 10699995

All rights reserved

INFORMATION TO ALL USERS

The quality of this reproduction is dependent upon the quality of the copy submitted.

In the unlikely event that the author did not send a complete manuscript and there are missing pages, these will be noted. Also, if material had to be removed, a note will indicate the deletion.



ProQuest 10699995

Published by ProQuest LLC (2017). Copyright of the Dissertation is held by the Author.

All rights reserved.

This work is protected against unauthorized copying under Title 17, United States Code
Microform Edition © ProQuest LLC.

ProQuest LLC.
789 East Eisenhower Parkway
P.O. Box 1346
Ann Arbor, MI 48106 – 1346

UNIDIRECTIONAL SOLIDIFICATION STUDIES

OF

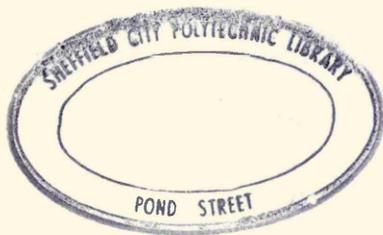
INGOT MOULD CAST IRONS

by

SARA ANN HORNBY, B.Sc., A.I.M. TECH., TECH. C.E.I.

This thesis is submitted in part fulfilment of the requirements for the degree of Doctor of Philosophy in Industrial Metallurgy of the Council of National Academic Awards. The work was carried out at Sheffield City Polytechnic, Department of Metallurgy, in collaboration with Swinden Laboratories, British Steel Corporation.

February 1980



7903034

	Page
Figure 1. The Iron-Carbon Equilibrium Diagram	1
2. A Schematic Cooling Curve for a Hypoeutectic Grey Cast Iron	2
3. The Influence of Cooling Rate on the Temperature of Solidification of the Eutectic in Cast Iron	3
4. The Effect of Nucleation Rate on the Eutectic Solidification Temperature with Various Rates of Cooling	4
5. The Effect of Silicon on the Eutectic Equilibrium Freezing Temperatures (after Morrogh (1))	5
6. The Effect of Chromium on the Eutectic Equilibrium Freezing Temperatures (after Morrogh (1))	6
7. Sectional Views of the Furnace as used in the Initial Experiments	7
7A. Sectional Views of the Finally Modified Furnace	8
8. A Sectional Plan View of the Furnace	9
9. A Detailed Sectional View of the Mould Inside the Furnace used in the Initial Experiments	10
9A. A Detailed Sectional View of the Mould Inside the Finally Modified Furnace	11
Table 1. Material Compositions	12
Plates 1 and 2. Experimental Apparatus	13
3 and 4	14
5 and 6	15
7 and 8	16
9 and 10	17
11	18
12 and 13	19
14	20
15 and 16	21
17	22
Table 2. Mould Preheating Furnace Specifications	23
3. Crucilite Element Specifications	24
4. Radial Temperature Distribution within the Mould Cavity in the Presence of the Original Vitreosil Diffuser	24
Figure 10. Overall Furnace Circuit Diagram	25
11. Circuit Diagram for the Middle Furnace Elements	26
12. Circuit Diagram for Top and Bottom Furnace Elements	27
13. The Internal Profile of the Mould	28

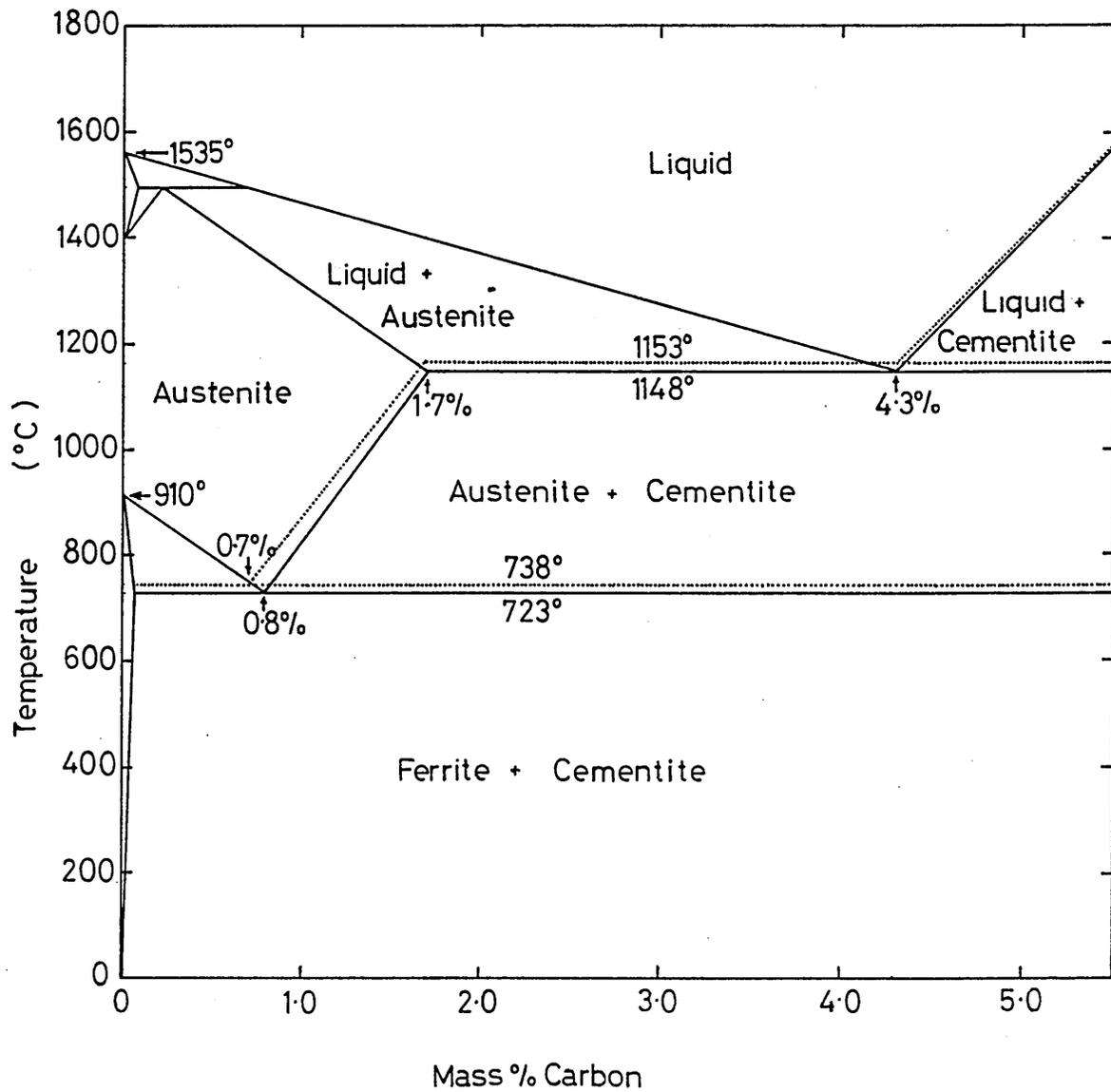
Table 5.	Mould Specifications	29
6.	Molochite Suspension	29
7.	Copper Chill Specifications	29
8.	Thermocouple Assemblies	30
9.	The Effect of Carbon 'Pick-Up' on the Composition of Induction Melted Cast Iron	31
10.	The Variation of Carbon, Sulphur and Manganese Content with Holding Time After Melting in a Pre-Heated 'Zircon' Coated Graphite Susceptor - Melt Practice A	32
11.	A Summary of the Procedures for Melts 6-17	33
12.	Analytical Methods	34
13.	Specified Performance Data - Credshire 500 Analogue Scanner	35
14.	Performance Data - 220 Drive Cassette Unit	36
Figures 14-21	Cooling Curves for the White Iron Melts	37-44
Plate 18.	Fractured Casting from Melt 7	45
19.	Fractured Casting from Melt 8	46
20.	Fractured Casting from Melt 10	47
21.	Fractured Casting from Melt 12	48
22.	Fractured Casting from Melt 13	49
23.	Fractured Casting from Melt 14	50
24.	Fractured Casting from Melt 16	51
	Introduction to White Iron Microstructures	52
25 and 26.	Melt 16 Microstructures	53
27.	Fractured Casting from Melt 17	54
28 and 29.)	Melt 17 Microstructures	55
30 and 31.))	56
32 and 33.))	57
34)	58
Table 15.	Cast Compositions for the Grey Iron Melt Programme -	
	15a. Low Nitrogen Melts	59
	15b. High Nitrogen Melts	60
	Introduction to Cooling Curves - Figures 22 to 60	61
Figures 22-60.	Grey Iron Melt Programme Cooling Curves	62-100
Table 16.	The Cooling Rate ($^{\circ}\text{C}/\text{min}$) for the 1160-1100 $^{\circ}\text{C}$ Temperature Range	101
17.	The Cooling Rate ($^{\circ}\text{C}/\text{min}$) for the 1160-700 $^{\circ}\text{C}$ Temperature Range	102
18.	Actual Thermocouple Displacement (mm).	103
19.	Statistical Analysis of Cooling Rates for Thermocouples in the Aim Positions (Table 8b).	104

	with Distance from the Chill/Metal Interface	105
62.	The Variation of Overall Cooling Rate Between 1160-700°C	
	with Distance from the Chill/Metal Interface	106
Plate 35.	Fractured Castings for the Low Nitrogen Melt Programme	107
	Introduction to the Grey Iron Microstructures	108
Plates 36 to 39		109
	40 to 43	110
	44 and 45	111
	46 to 48	112
	49 to 51	113
	52 to 55	114
	56 to 58	115
	59 Additional Base Low Nitrogen Casts	116
	60 to 62	117
	63 and 64	118
	65 to 68	119
	69 and 70	120
	71 to 74	121
	75 to 78	122
	79 to 82	123
	83 to 86	124
	87 to 89	125
	90 to 93	126
	94 to 96	127
	97 to 100	128
	101 to 104	129
Table 20.	Microstructural Criteria for the Low Nitrogen Grey Iron Castings	130
Plates 105 to 108		131
	109 to 112	132
	113 to 116	133
	117 to 120	134
	121 to 124	135
	125 to 128	136
	129 to 132	137
	133	138
	134 to 136 Additional Low Nitrogen Casts	139
Table 21.	Microstructural Criteria for the Additional Castings	140
Plates 137 and 138		141
	139 Fractured Castings for the High Nitrogen Melt Programme	142

Table 22.	Microstructural Criteria for the High Nitrogen Grey	
	Iron Castings	143
Plates	140 to 142	144
	143 to 145	145
	146 to 148	146
	149 to 152	147
	153 and 154	148
	155 The Fractured Casting of Melt Ala	149
	156 to 159	150
	160 to 162	151
	163 to 166	152
	167 to 170	153
	171 to 174	154
	175 to 178	155
	179 to 182	156
	183 to 186	157
	187 to 189	158
	190 and 191 Fractured Castings of Additional High Nitrogen	
	Casts	159
	192	160
	<u>Scanning Electron Micrographs</u>	
	193	161
	194	162
	195	163
	196	164
	197	165
	198	166
	199	167
	Introduction to Plate 200	168
	200	169
	Introduction to Plate 201	170
	201	171
	Introduction to Plate 202	172
	202	173
	203	174
	Introduction to Plate 204	175
	204	176
Table 23.	Equivalent Cooling Rates ($^{\circ}\text{C}/\text{min}$) for the Low Nitrogen	
	Casts' Microstructural Criteria Given in Table 20 for	
	the 1160-1100 $^{\circ}\text{C}$ Temperature Range	177

Table 24.	Table 23 Subdivided into General Groups According to the Effect of Titanium Additions on the Solidification Mode ($^{\circ}\text{C}/\text{min}$)	178
25.	Equivalent Cooling Rates ($^{\circ}\text{C}/\text{min}$) for the High Nitrogen Casts' Microstructural Criteria in Table 22 for the 1160-1100 $^{\circ}\text{C}$ Temperature Range	179
26.	Table 25 Subdivided into General Groups According to the Effect of Titanium Additions on the Solidification Mode ($^{\circ}\text{C}/\text{min}$)	180
Figure 63.	The Effect of Titanium Concentration on the Maximum Cooling Rate for the Formation of the Graphitic Eutectic Cells	181
64.	The Effect of Titanium Concentration on the Maximum Cooling Rate for the Formation of Streamer Graphite	182
65.	The Effect of Titanium Concentration on the Maximum Cooling Rate for the 'Grey' Start	183
Table 27.	Equivalent Cooling Rates ($^{\circ}\text{C}/\text{min}$) for the Microstructural Criteria for the Additional Casts in Table 21 for the 1160-1100 $^{\circ}\text{C}$ Temperature Range	184
28.	Equivalent Cooling Rates ($^{\circ}\text{C}/\text{min}$) for the Microstructural Criteria for the Low Nitrogen Casts in Table 20 for the 1160-700 $^{\circ}\text{C}$ Temperature Range	185
29.	Equivalent Cooling Rates ($^{\circ}\text{C}/\text{min}$) for the Microstructural Criteria for the High Nitrogen Casts in Table 21 for the 1160-700 $^{\circ}\text{C}$ Temperature Range	186
Figure 66.	The Manganese-Sulphur Equilibria for the Liquid Ingot Mould Cast Iron from Appendix 2	187

Figure 1 : The iron-carbon equilibrium diagram .



——— The iron - Fe₃C system .
 The iron - graphite system .

Figure 2 : A schematic cooling curve for a hypoeutectic grey cast iron .

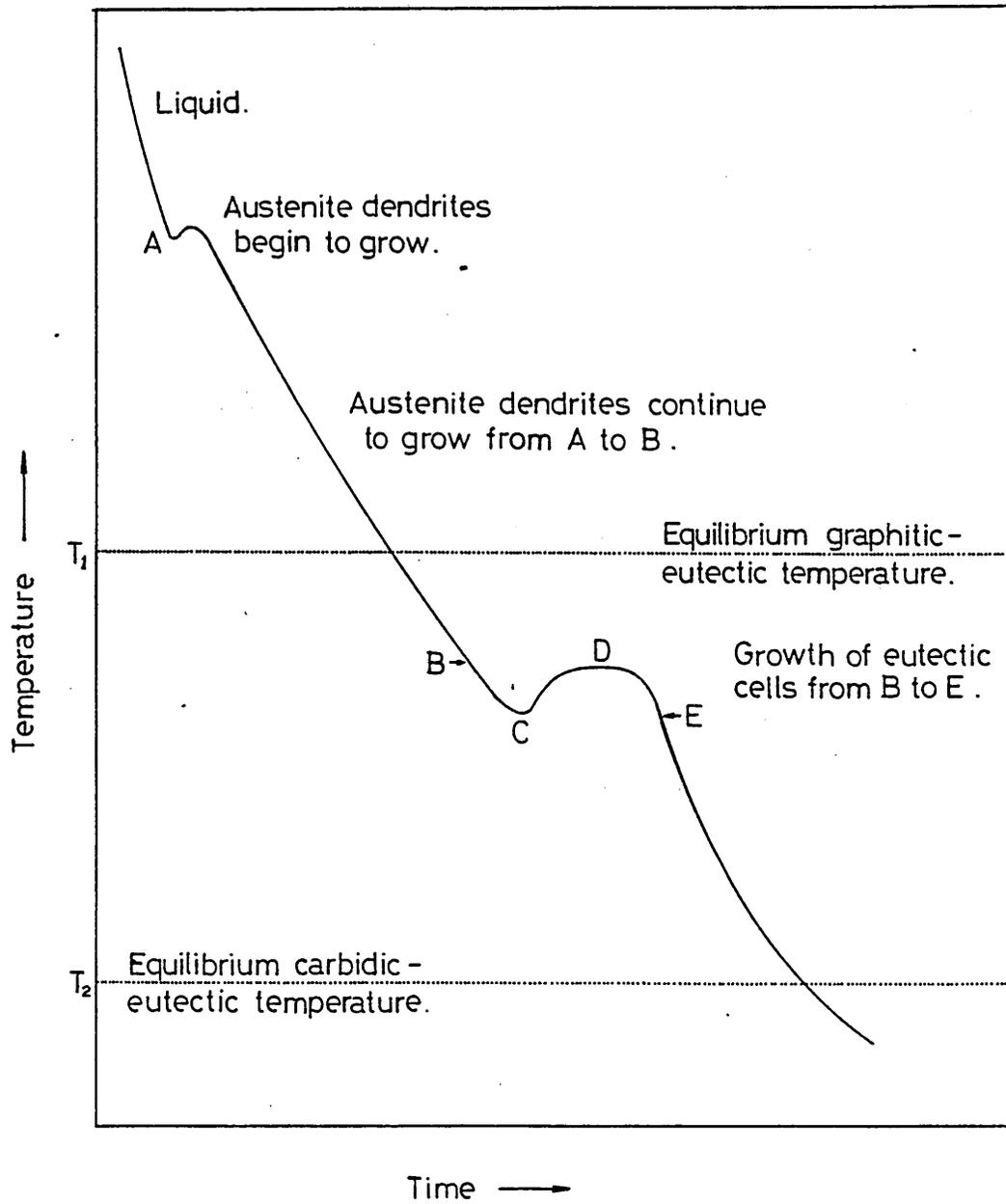


Figure 3 : The influence of cooling rate on the temperature of solidification of the eutectic in cast iron .

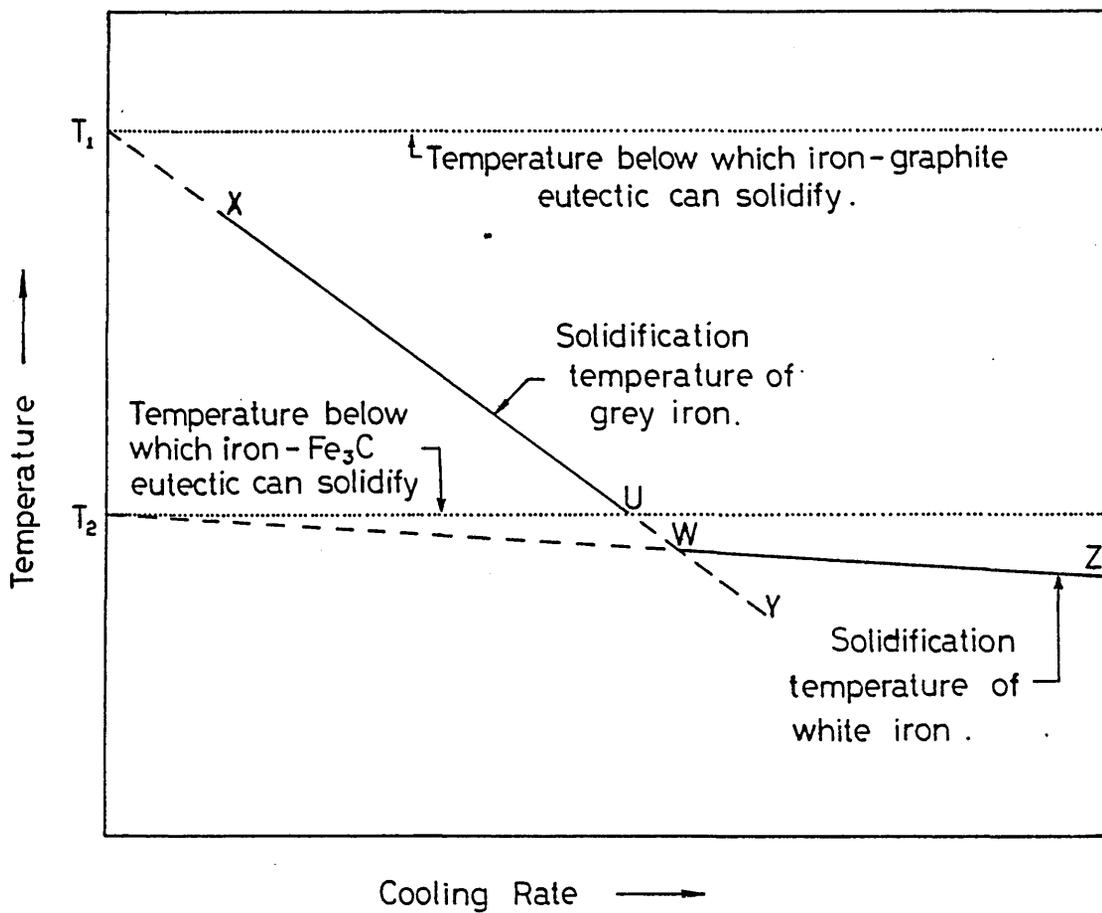
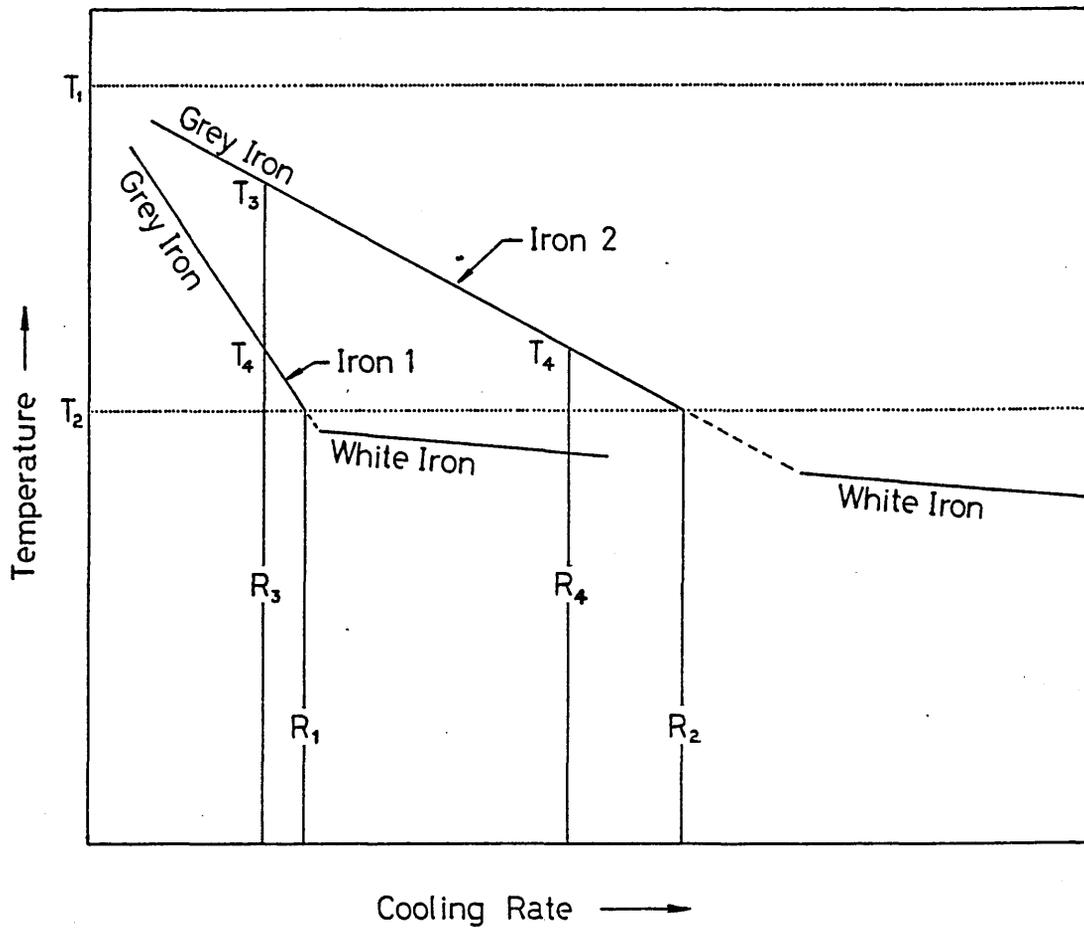


Figure 4 : The effect of nucleation rate on the eutectic solidification temperature with various rates of cooling .



Iron1 : A cast iron which has not been inoculated.

Iron2 : An inoculated cast iron with a nucleation rate greater than that of Iron 1.

Figure 5 : The effect of silicon on the eutectic equilibrium freezing temperatures (after Morrogh [1]).

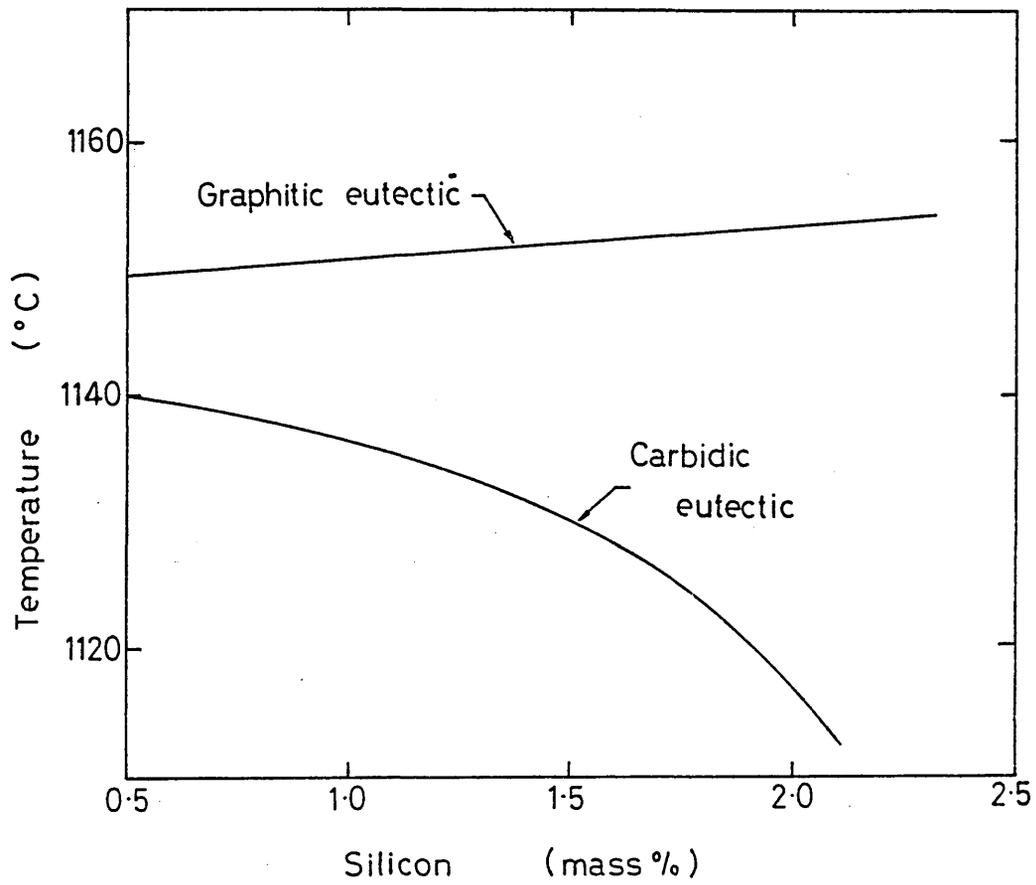


Figure 6 : The effect of chromium on the eutectic equilibrium freezing temperatures (after Morrogh [1]).

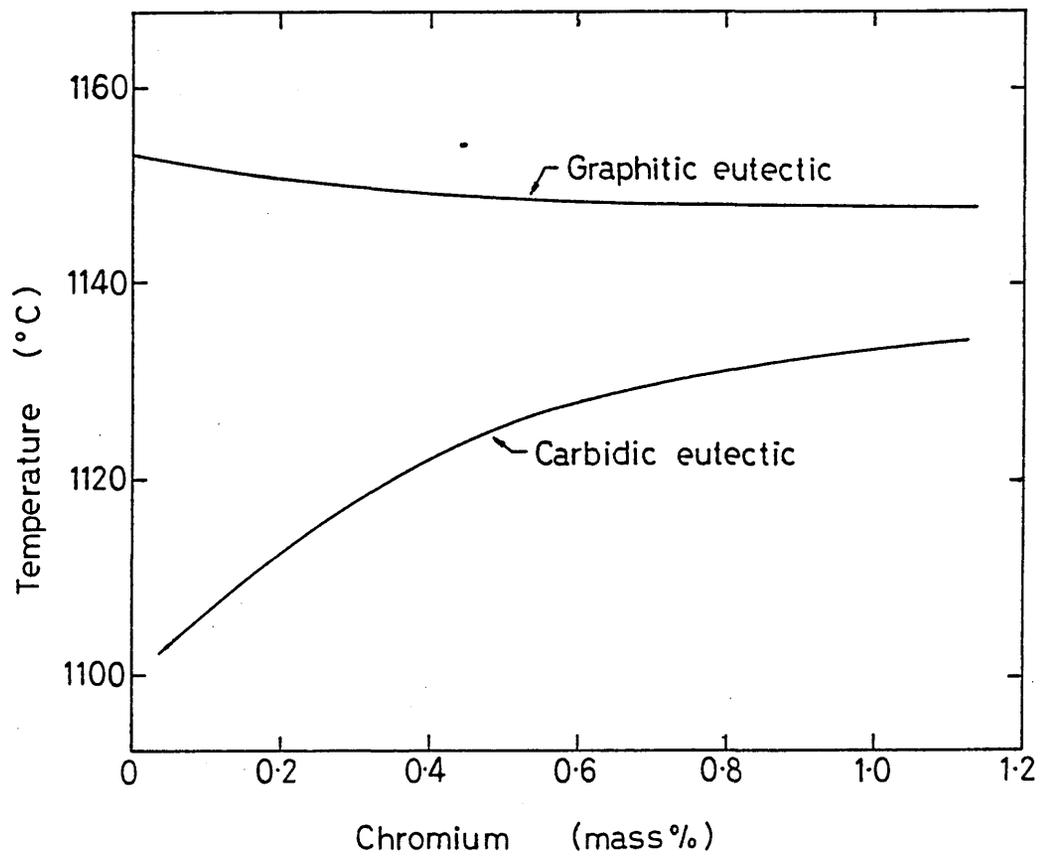


Figure 7 : Sectional views of the furnace as used in the initial experiments .

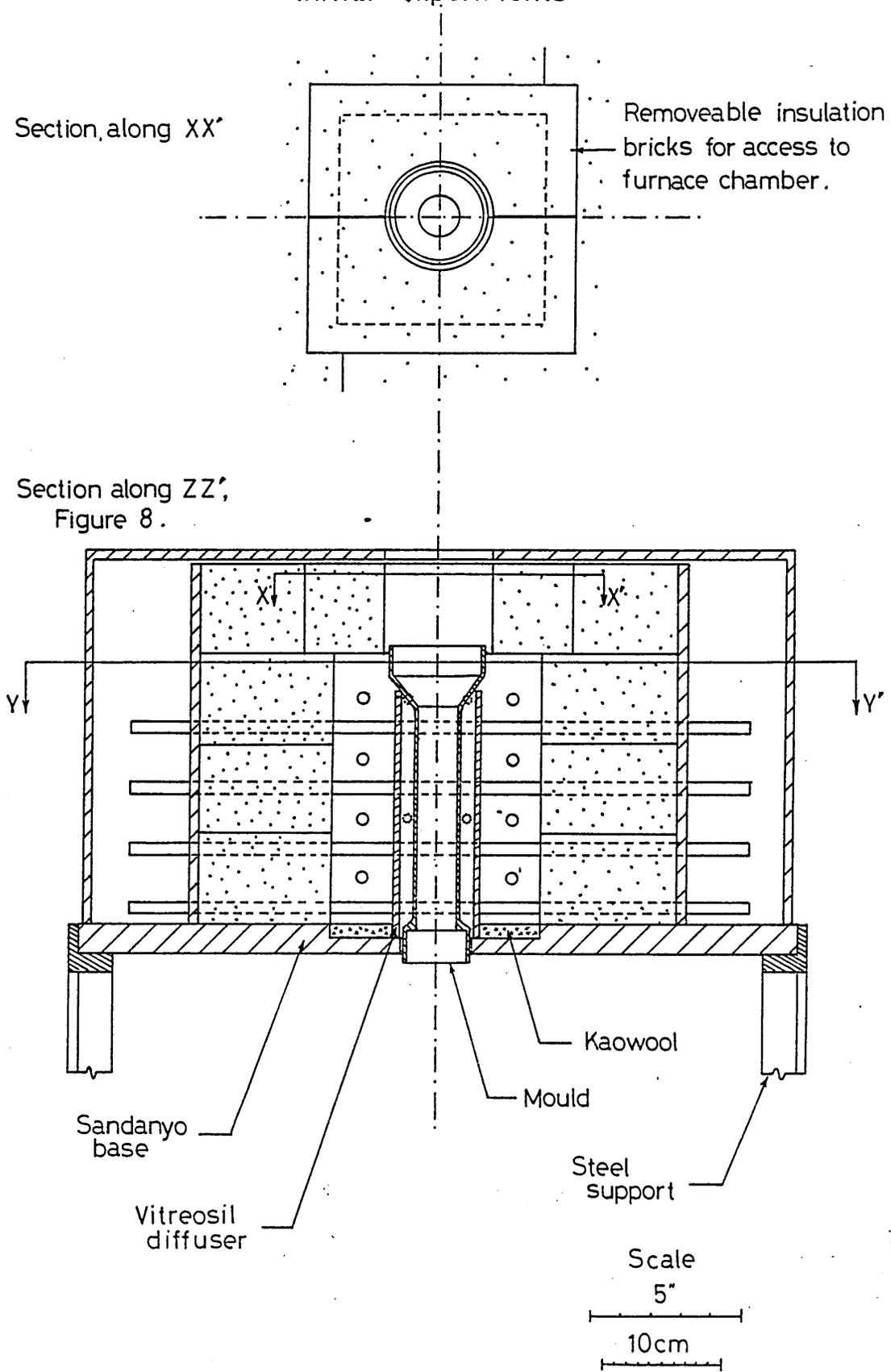


Figure 7A : Sectional views of the finally modified furnace .

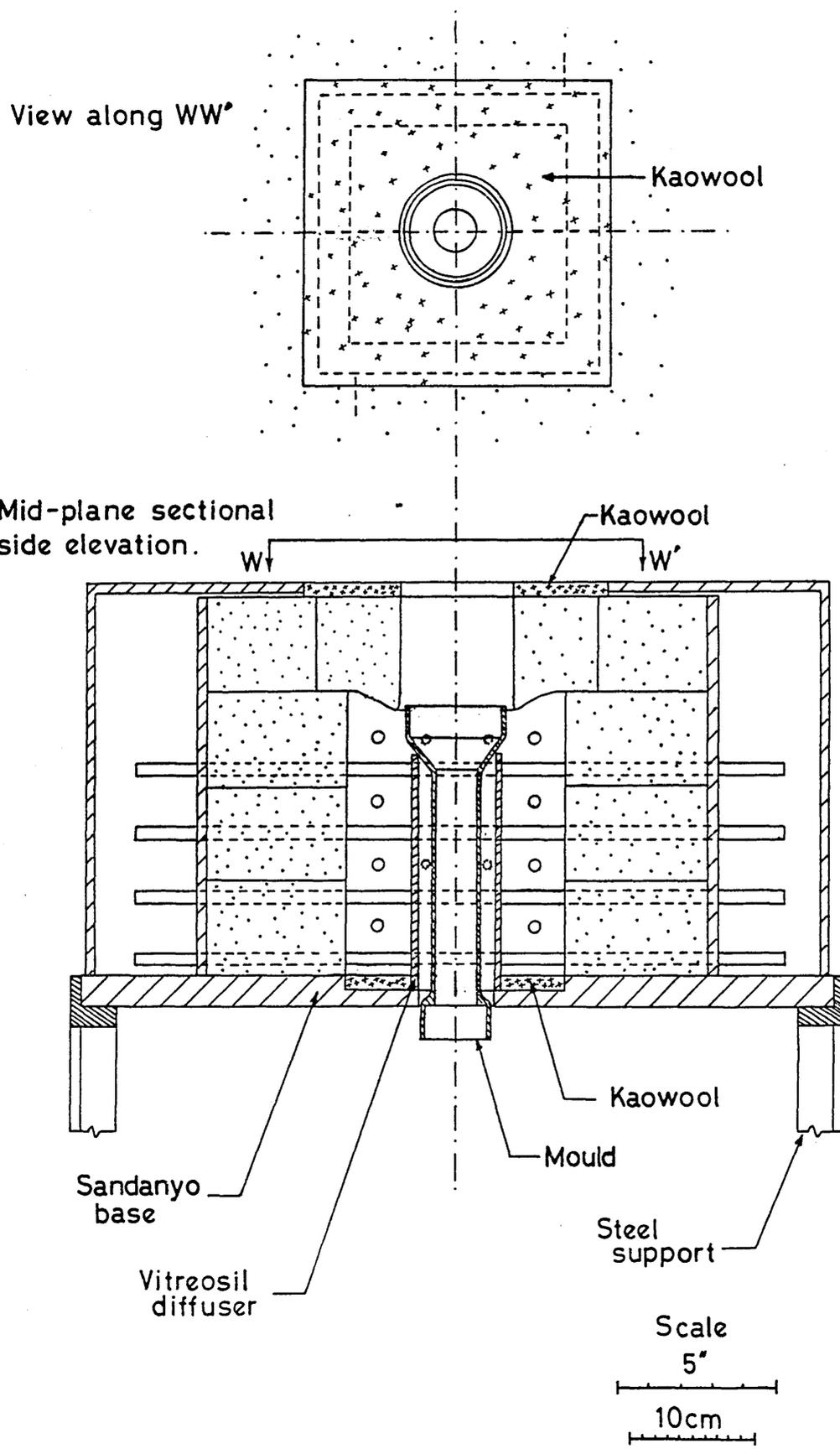
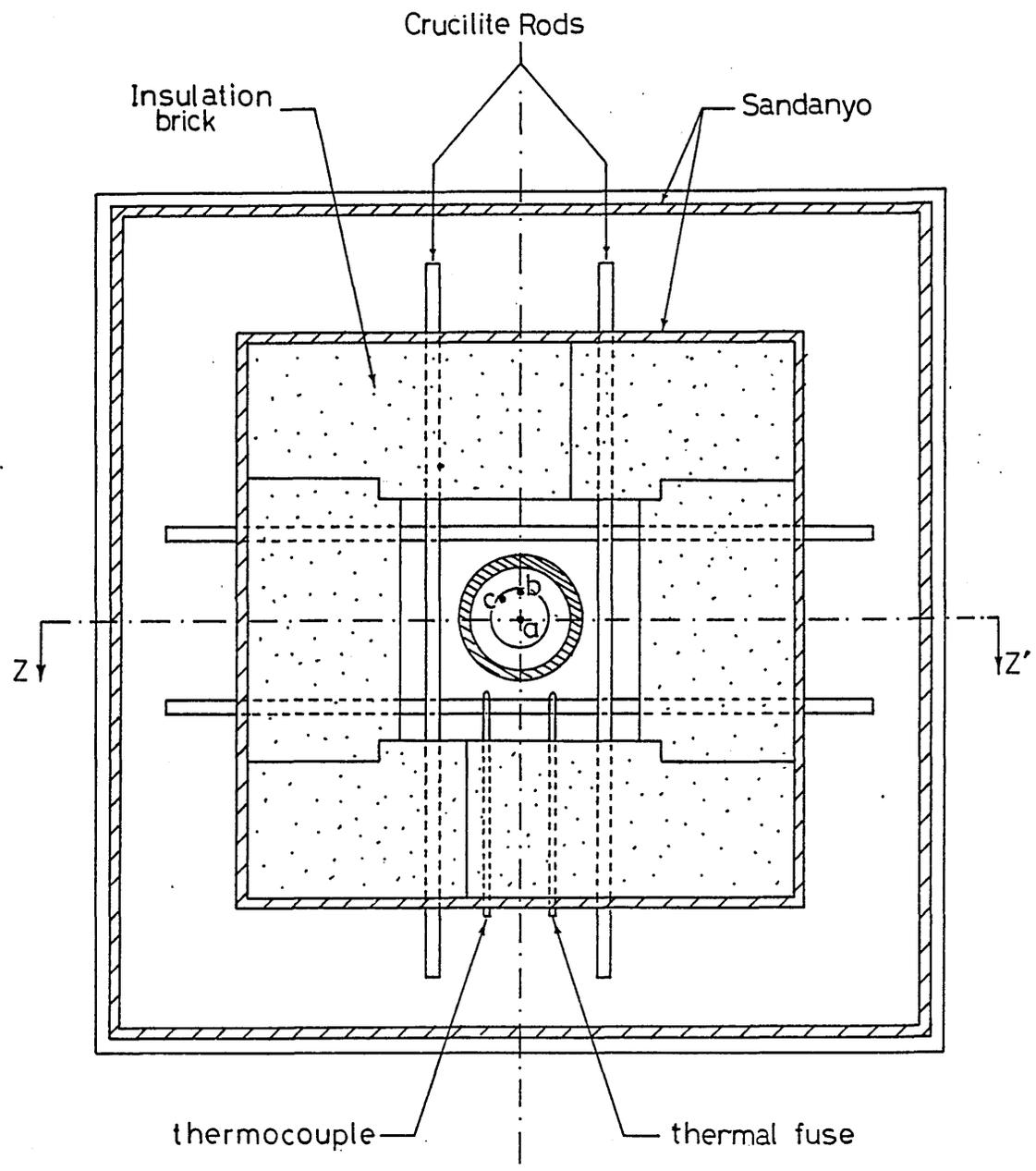


Figure 8 : A sectional plan view of the furnace .



Section along YY',
Figure 7 .

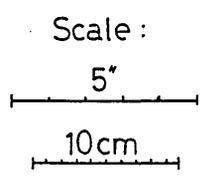
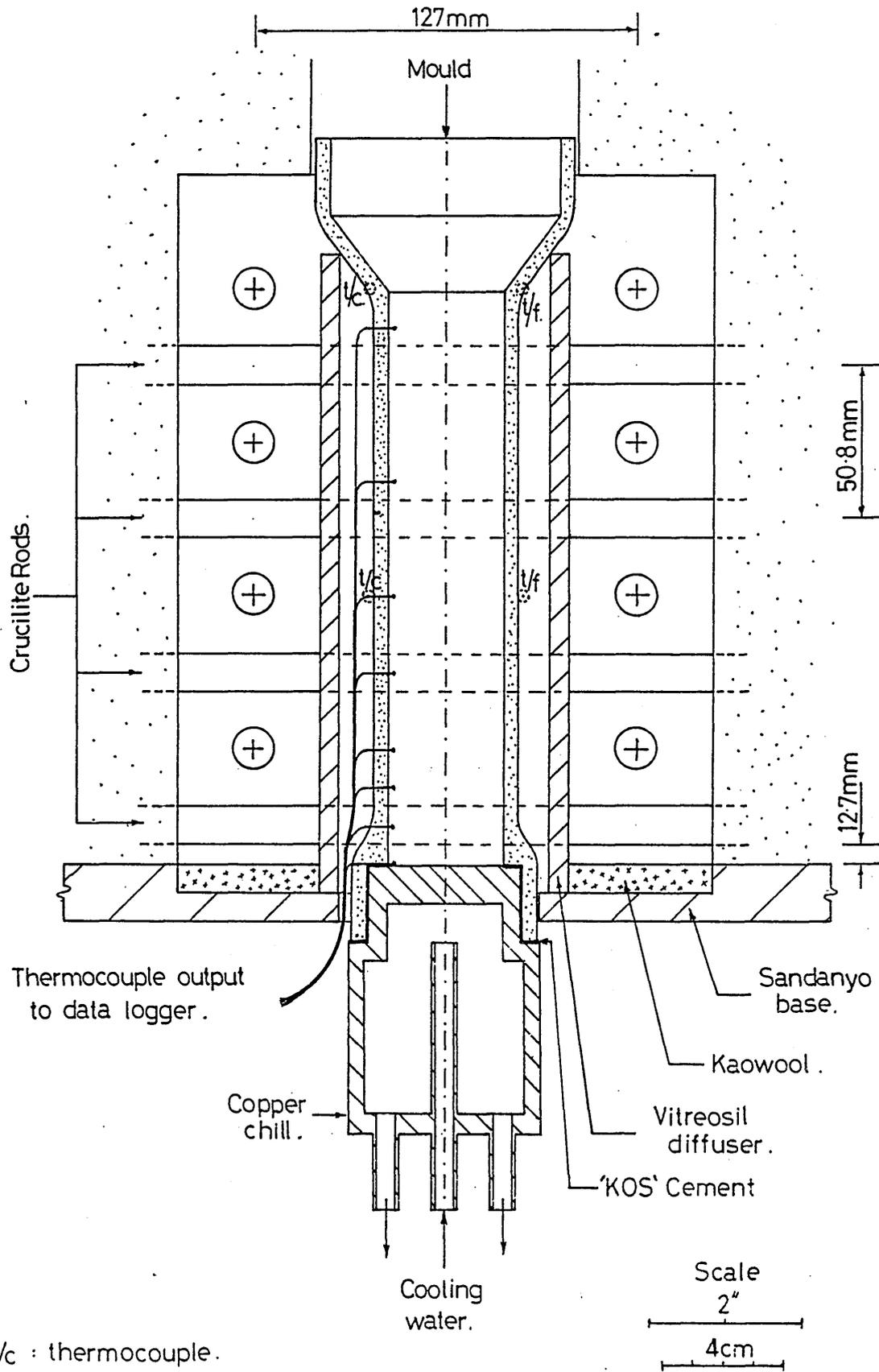


Figure 9 : A detailed sectional view of the mould inside the furnace used in the initial experiments.



t/c : thermocouple.
t/f : thermal fuse.

Figure 9A : A detailed sectional view of the mould inside the finally modified furnace .

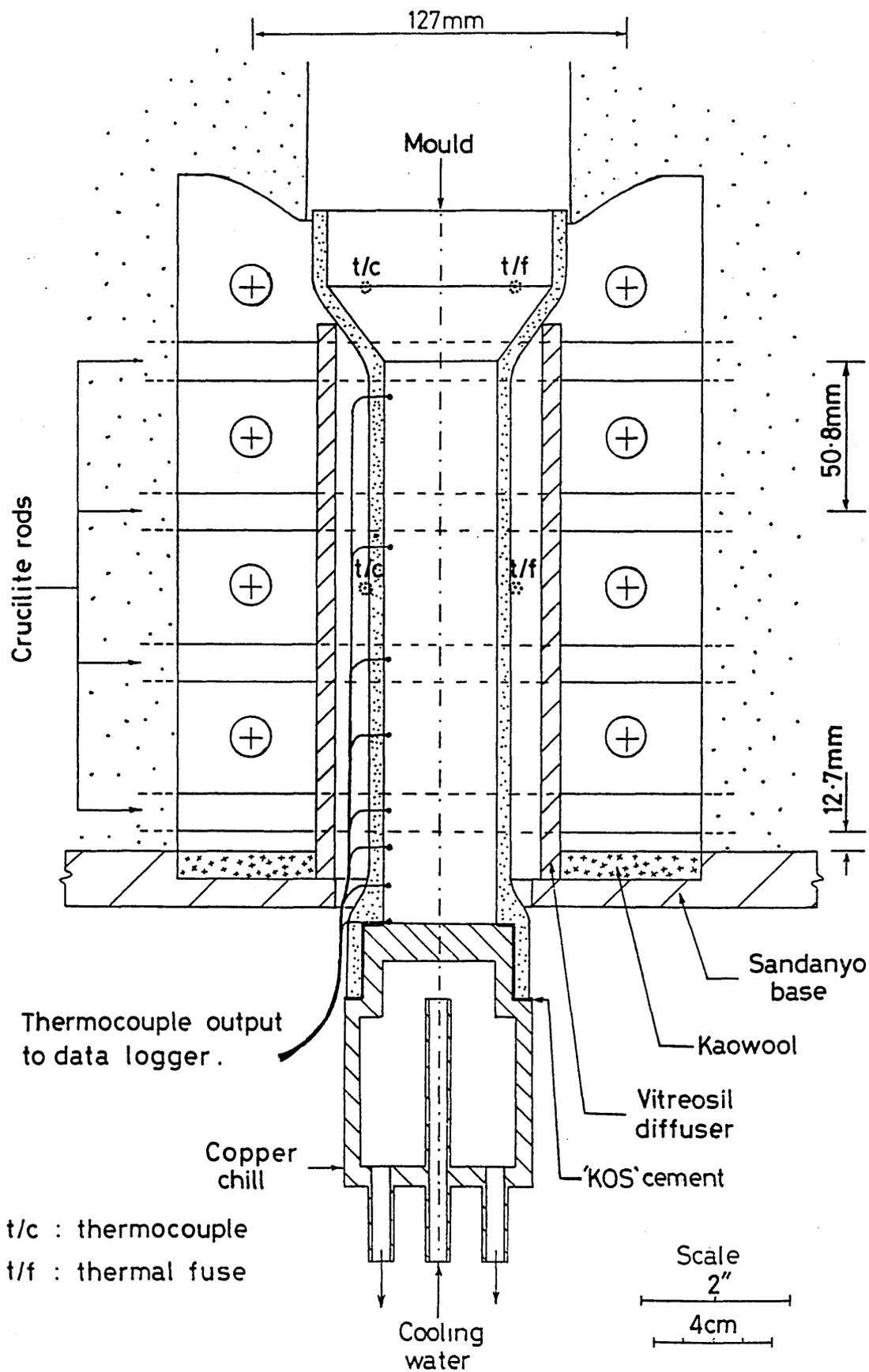


TABLE I - MATERIEL COMPOSITIONS

MATERIEL	COMPOSITION (MASS PER CENT)																	
	Fe	C	Si	P	Mn	S	N ₂	Ni	Mo	Cr	Ti	B	MgO	Al ₂ O ₃	CaO	SiO ₂	FeO	
Warner Iron I	95.86	3.74	0.11	0.025	0.18	0.025		0.045	0.015									
White Iron II	97.003	2.2	0.04	0.162	0.415	0.18												
B.S.C Base Iron III	94.706	3.8	1.23	0.02	0.2	0.04	0.0036											
Iron Sulphide	75.3					24.7												
High N ₂ FeMn	11.67	0.68	0.54		81.3		5.81											
Low N ₂ FeMn	17.09	0.10	1.11		81.7													
High C FeCr	22.78	5.93	1.69							69.6	15.25							
Ferrotitanium	84.75									99.8								
Chromium																		
Ferroboreon	80											20						
Rammed H.F. Lining													84.6	10.0	2.0	1.8		1.3

PLATE 1

The two central bricks are removed to show the ceramic mould seated upon the vitreosil diffuser within the furnace hot zone. The bricks have been deepened, by addition of insulating cement and a thin layer of brick, to compensate for the lowering of the mould into the furnace hot zone (Section 3.2.1). The Crucilite elements (2 sets of 4 pairs) intersect at right angles.

PLATE 2

The ceramic mould is held rigidly in place in the furnace cavity by inserting a Kaowool plug between the mould and the two central insulating bricks.

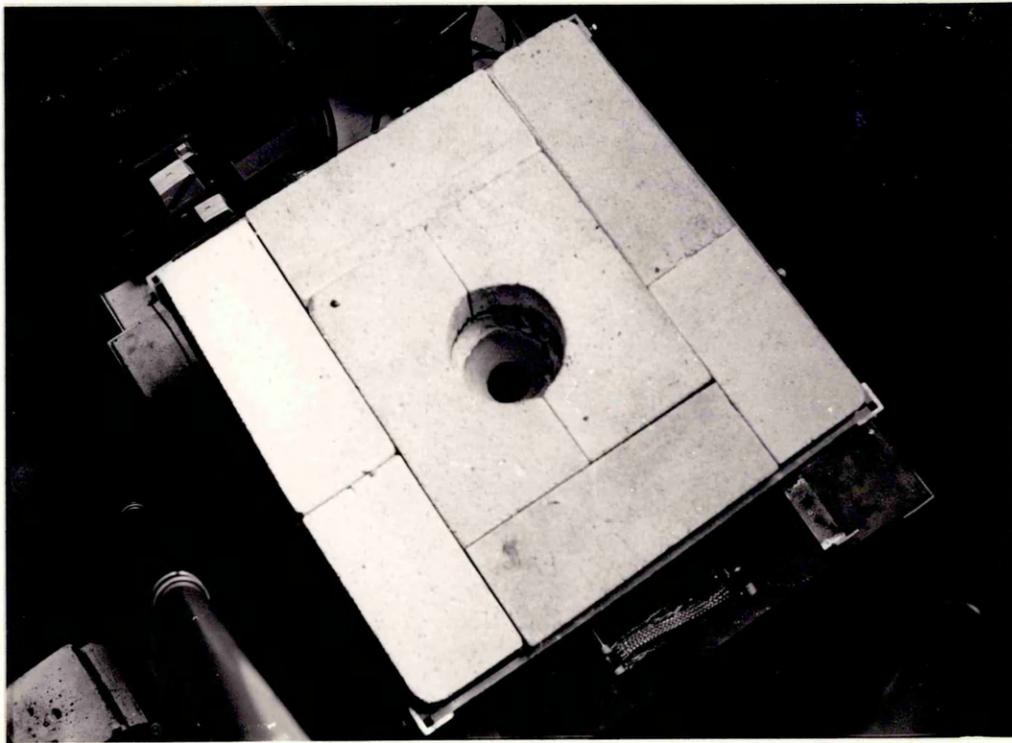
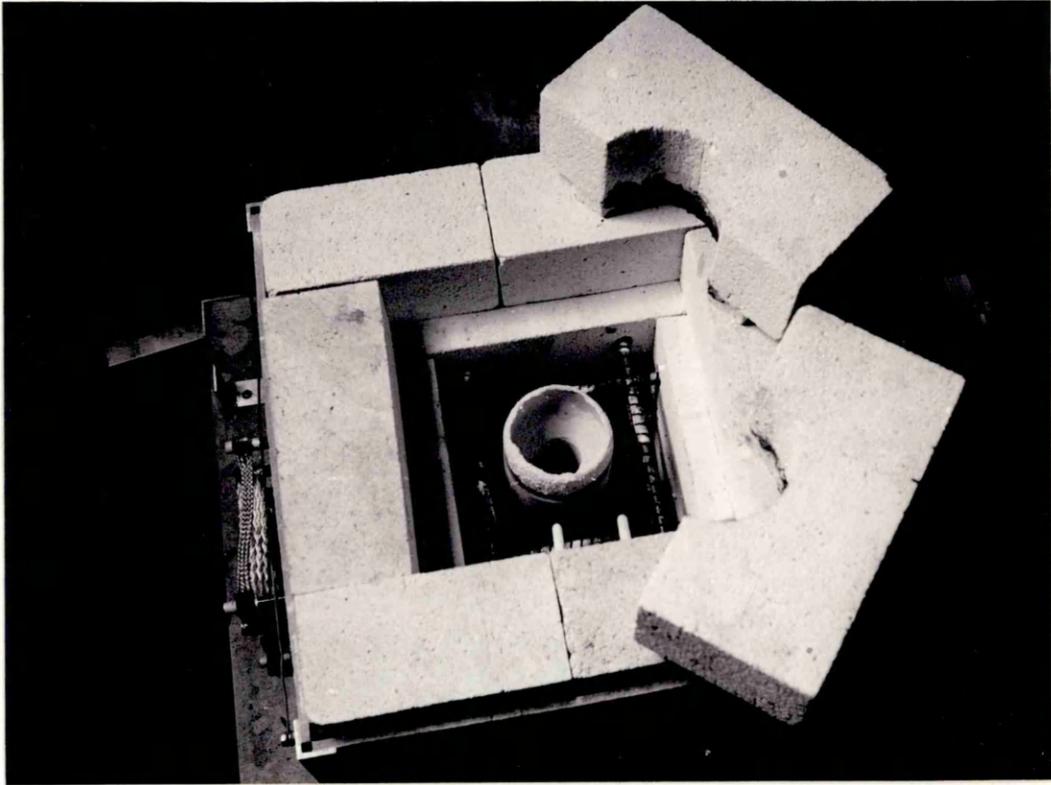


PLATE 3

Unidirectional heat flow is induced by the presence of a water cooled copper chill held in position at the base of the mould by a clamp stand. A steel furnace support permits the location of the copper chill and connection of the thermocouples to the compensating leads.

PLATE 4

The supported copper chill and the modified (earthed) thermocouple arrangement (Section 3.10.2). All thermocouples and compensating leads are wrapped with aluminium foil and earthed via an external source (See Plate 17).

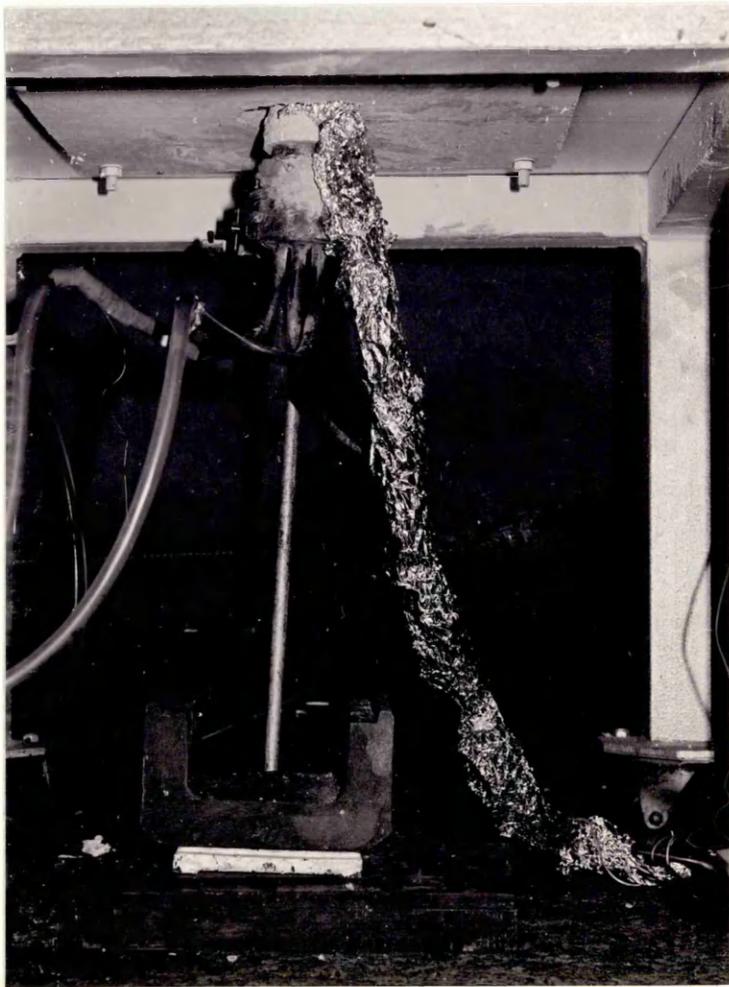
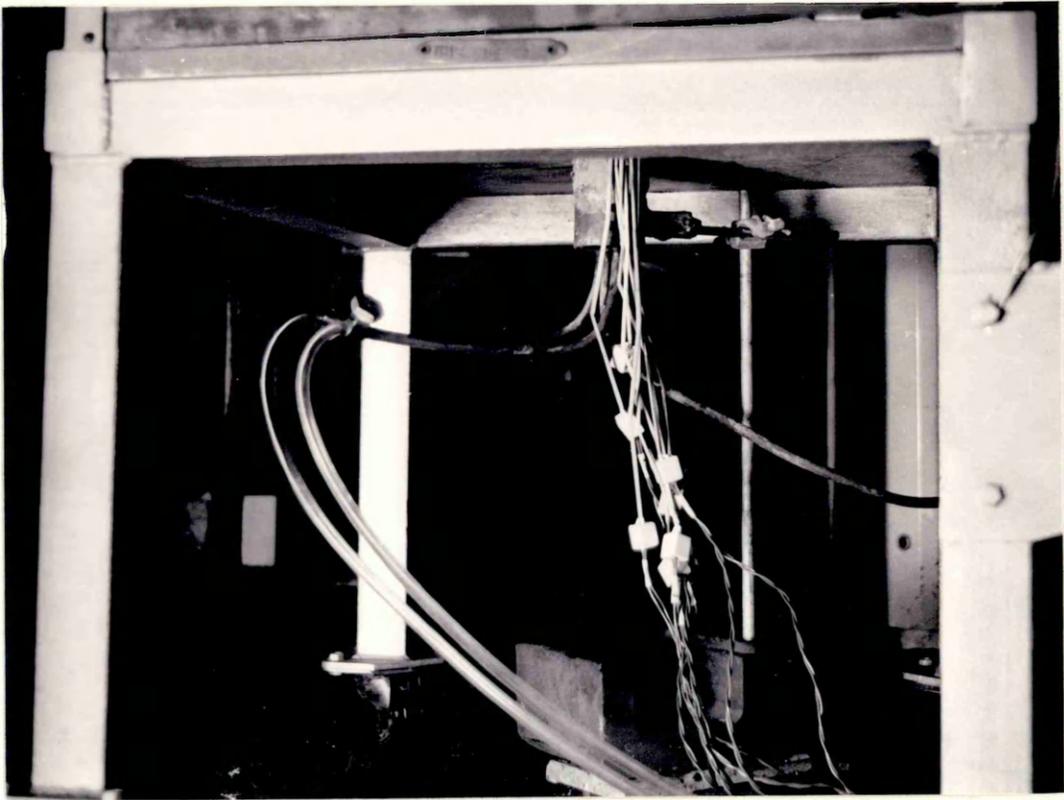


PLATE 5

The mould preheating furnace, the Credshire 500 Analoguer and the 200 cassette unit. The furnace's outer removable Sandanyo cover provides protection for the Crucilite heating elements and electrical connections.

PLATE 6

The protective Sandanyo cover is removed permitting access to the mould cavity (prior to the modifications (see Plate 9)), the 16 Crucilite rods and the electrical connections.

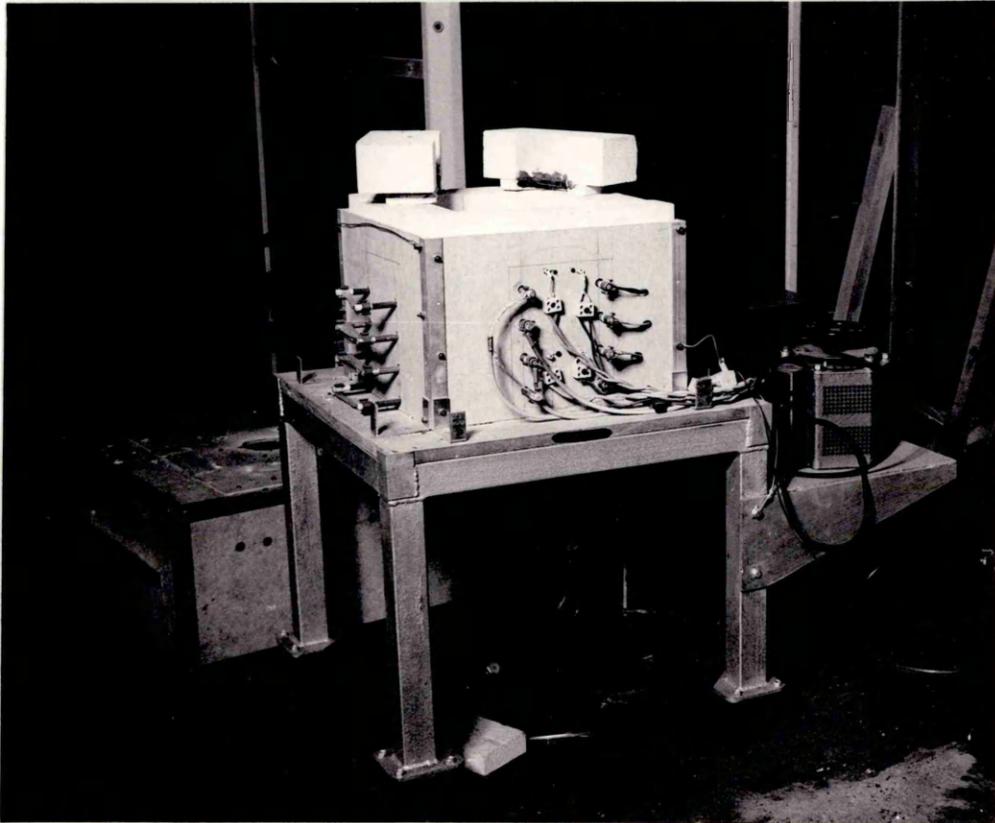
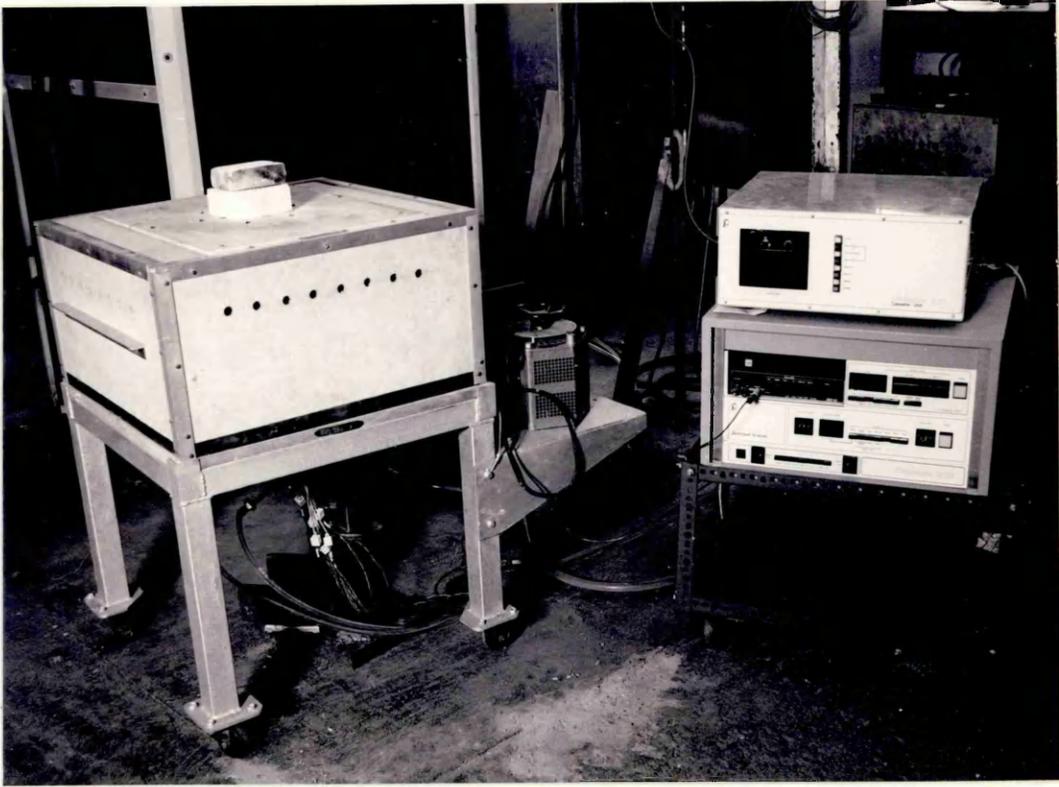


PLATE 7

The two central bricks removed to expose the Crucilite heating rods and vitreosil diffuser in the furnace hot zone. These bricks were deepened to compensate for repositioning the mould in the furnace hot zone to prevent thermal losses via the feeder head (see Section 3.2.1).

PLATE 8

The mould in position in the furnace. A Kaowool seal between the mould and the deepened central bricks ensures mould rigidity and prevents metal penetration to the hot zone during teeming. The number 8 thermocouple position is just visible at the top of the vertical sample section, on the furnace diagonal.

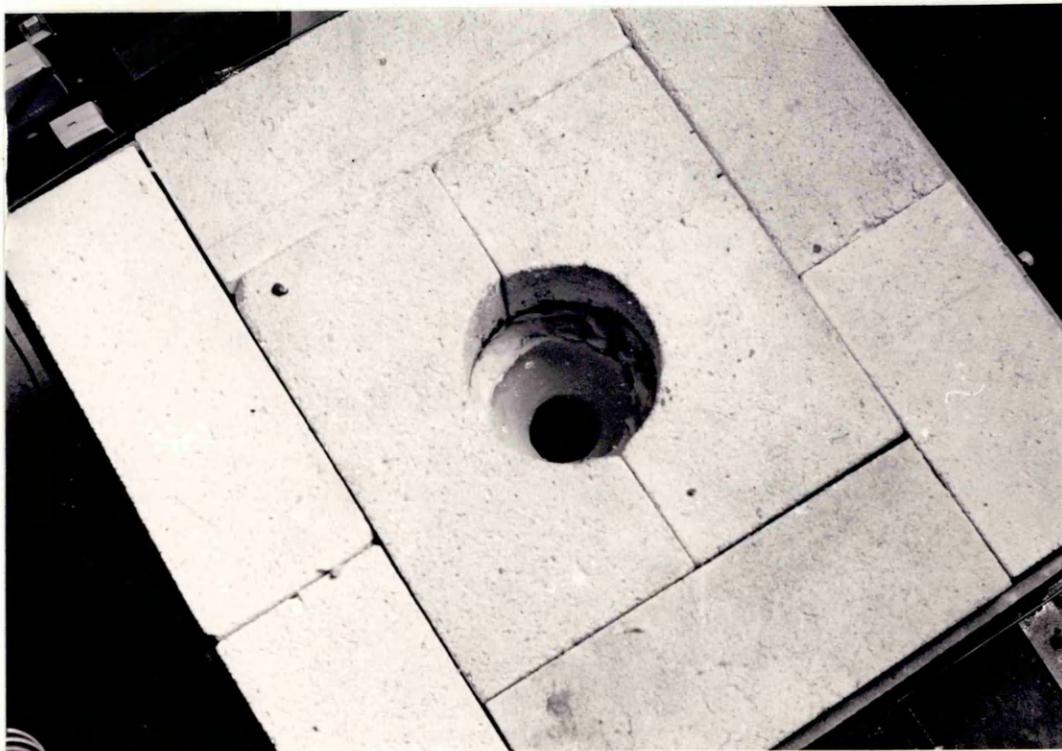
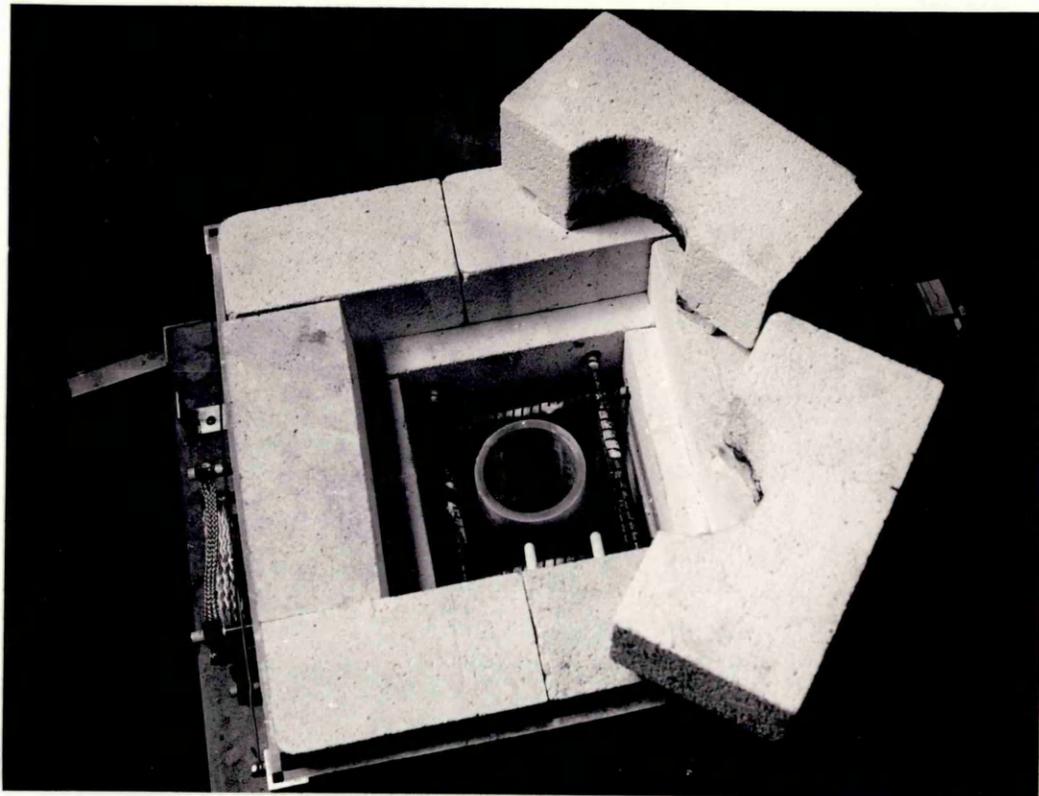


PLATE 9

A 237.5mm square hole cut in the furnace's outer Sandanyo cover permits access to the furnace hot zone without necessitating total removal of the cover.

PLATE 10

The Kaowool seal between the mould and the bricks prevents metal penetration to the hot zone and ensures mould rigidity. The new arrangement for access to the hot zone and the earthing of the melt (Sections 3.2.1 and 3.10.2 respectively) is evident.

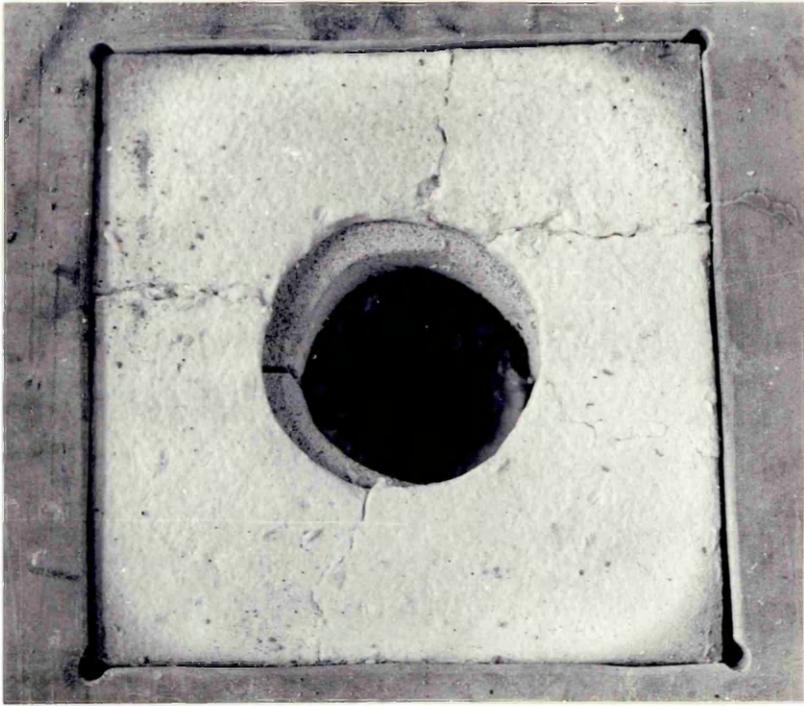
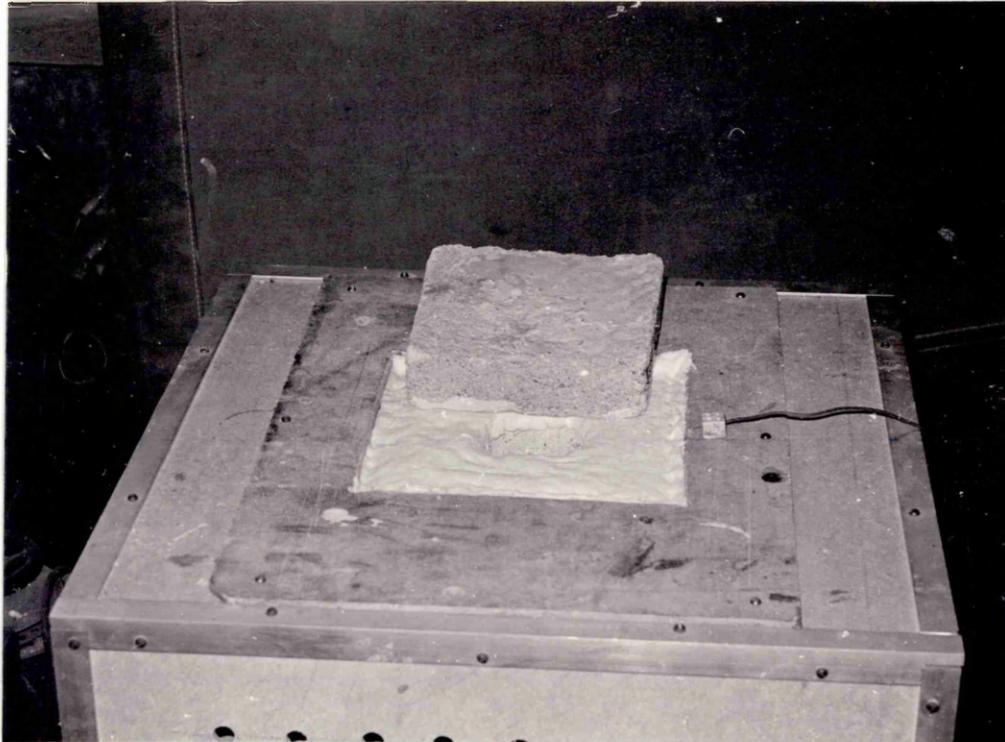


PLATE 11.

A Kaowool insert, placed on top of the two central bricks and the melt earthing wire, re-establishes the thermal insulation at the top of the furnace partially destroyed by the 'access' hole. The central Kaowool plug situated in the area above the feeder head is supplemented by an insulating brick.



PLATES 12 AND 13

The ceramic mould with Pt./Pt. 13% Rh. thermocouples cemented in position (Table 6b) using 'KOS' thermal cement. The cement seal prevents metal penetration from the mould cavity to the furnace hot zone. The thermocouple wires are silica sheathed.

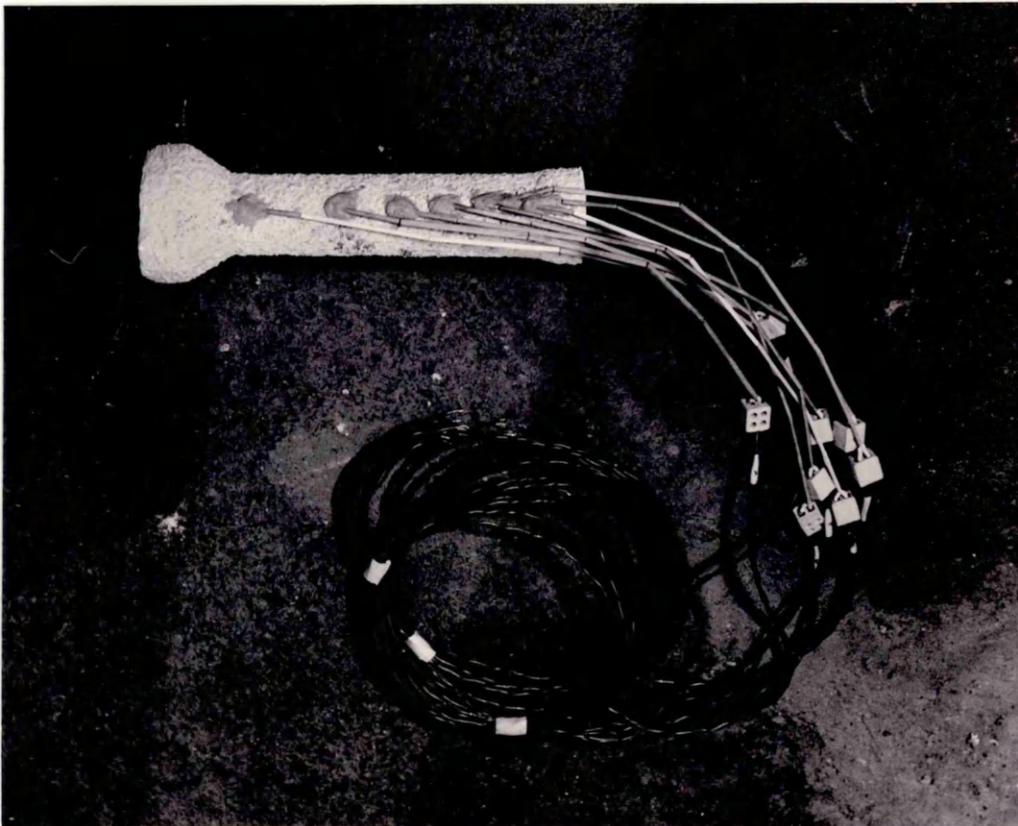
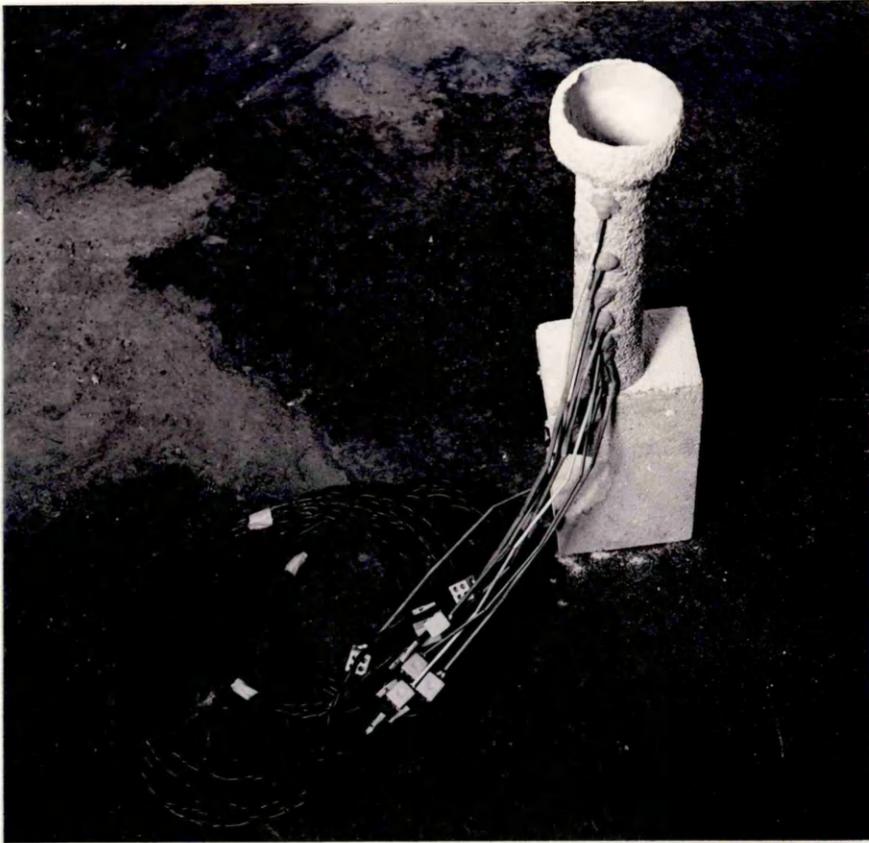


PLATE 14

Teeming the molten cast iron from the transfer ladle to the mould situated in the mould preheating furnace.



PLATE 15

The two rear panels which complete the 'isothermal box' at the rear of the data logger are removed to show the patchboards and the thermocouple connections.

PLATE 16

The two panels in position at the rear of the data logger. The compensating leads protrude through the foam plastic gland which completes the isothermal chamber.

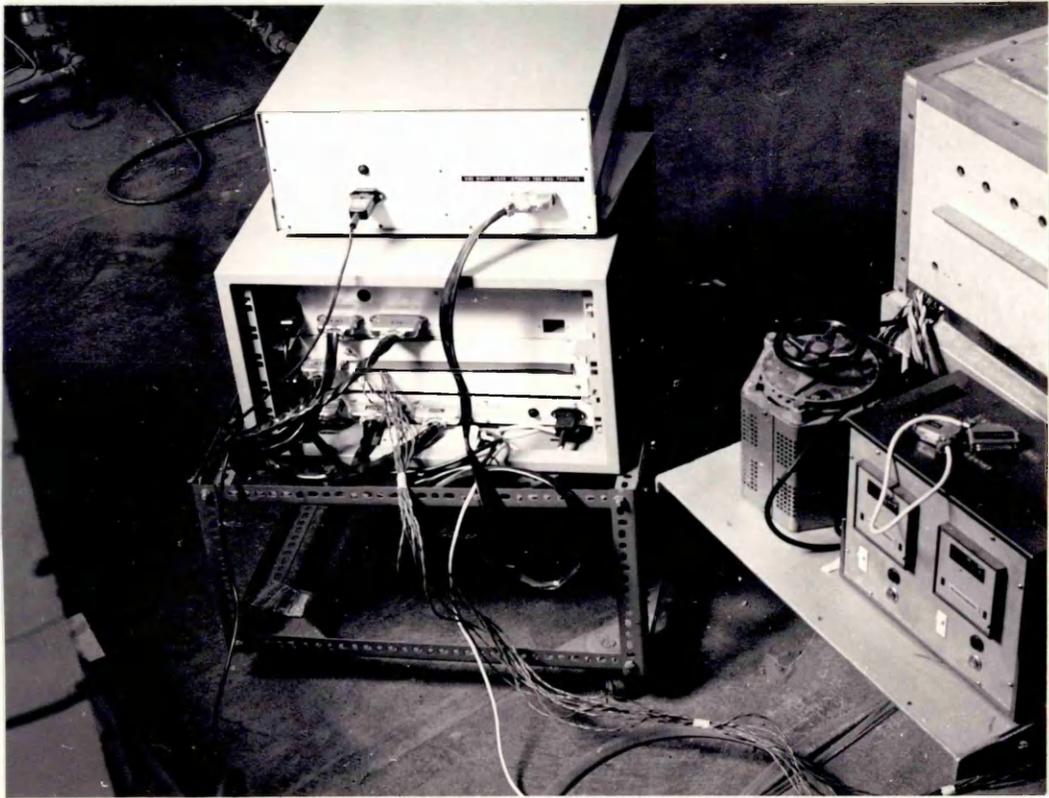
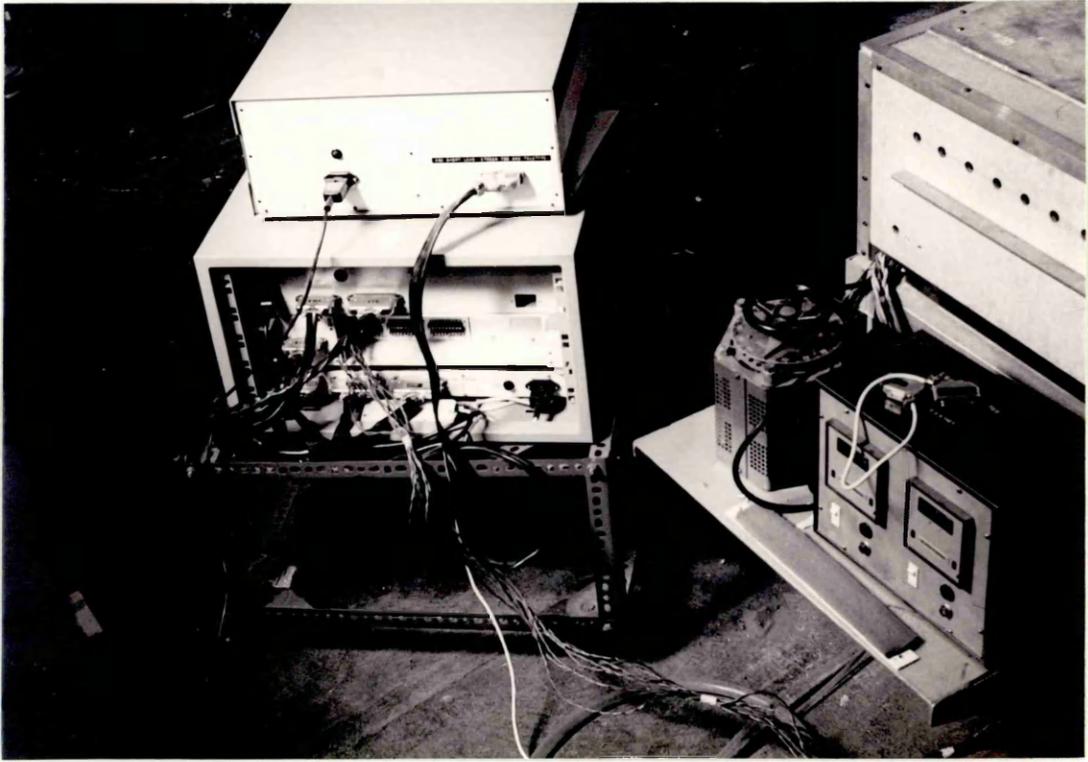


PLATE 17

The furnace and the rear of the Credshire 500 Analogue Scanner. The isothermal chamber is complete and the thermocouple compensating leads are earthed via an aluminium foil sheath which, together with the melt earth lead (Plates 10 and 11), is connected to the external earth.

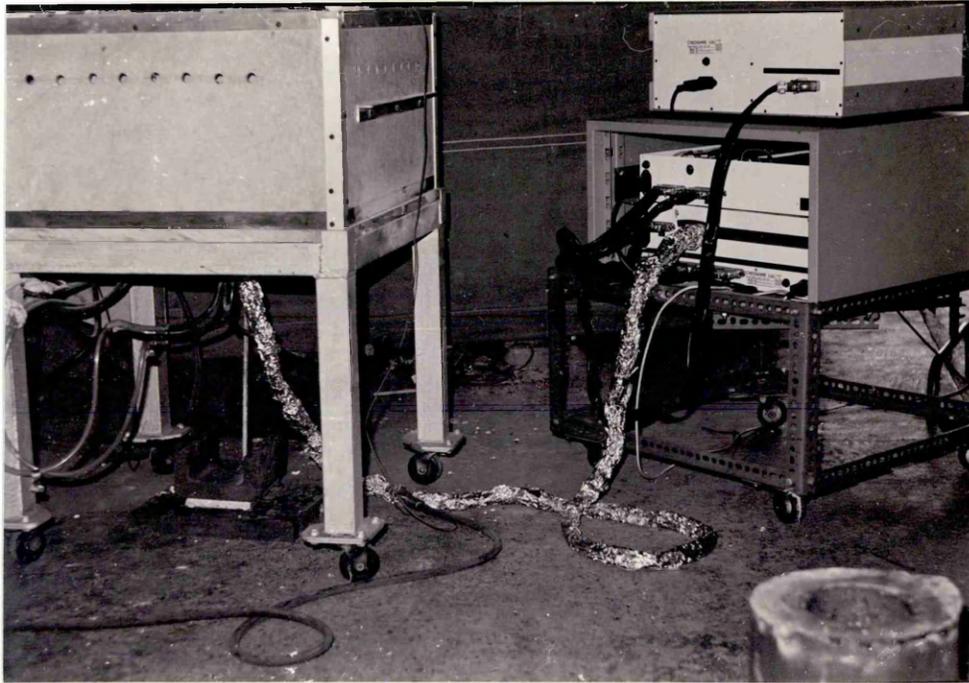


TABLE 2 - MOULD PREHEATING FURNACE SPECIFICATIONS

PARAMETER	HORIZONTAL DIMENSIONS (mm)	DEPTH (mm)
Sandanyo Furnace Base	650 square	18.78
External Sandanyo Cover	601 square	306.8
Original Access Hole	95 diameter	
Final Access Hole	243 square	
Internal Sandanyo Box (Hot Zone Casing)	436 square	305.5
Outer Brickwork	406 square	305
Brick Size (Hot Zone)	101.5 square	75.1
Top 2 Removable Bricks	225.3 x 112.65	75.1
Hole in Removable Bricks	95 diameter	75.1
Hot Zone Cavity	107.8 square	225.3
Original Diffuser	70 diameter	197
Final Diffuser	70 diameter	177.8

TABLE 3 - CRUCILITE ELEMENT SPECIFICATIONS

PARAMETER	DIMENSIONS (mm)
Rod	10.0 diam. x 540 length
Rod Hot Zone Length	184.2
Horizontal Axial Spacing	127.0
Vertical Axial Spacing	25.4
Vertical Displacement of Basal Elements	12.7

TABLE 4 - RADIAL TEMPERATURE DISTRIBUTION WITHIN THE MOULD CAVITY IN THE PRESENCE OF THE ORIGINAL VITREOSIL DIFFUSER

DISPLACEMENT* mm (inches)	TEMPERATURE IN °C					
	THERMOCOUPLE POSITION W.R.T. HEATING RODS					
	(a)	(a)	(b)	(b)	(c)	(c)
254 (10)	830	837	863	861	790	779
228.6 (9)	896	920	914	909	890	889
203.2 (8)	935	961	949	947	950	945
177.8 (7)	978	986	983	980	982	981
152.4 (6)	1001	1000	1001	1000	1001	1001
127 (5)	1007	1008	1006	1008	1007	1008
101.6 (4)	1008	1009	1009	1010	1010	1011
76.2 (3)	1008	1007	1007	1007	1008	1009
50.8 (2)	1001	987	1000	992	997	1004
25.4 (1)	985	986	985	987	982	992
0 (0)	949	956	954	952	949	958

* The 'displacement' of the thermocouple hot junction is measured vertically from the pseudo-chill interface.

Figure 10 : Overall furnace circuit diagram.

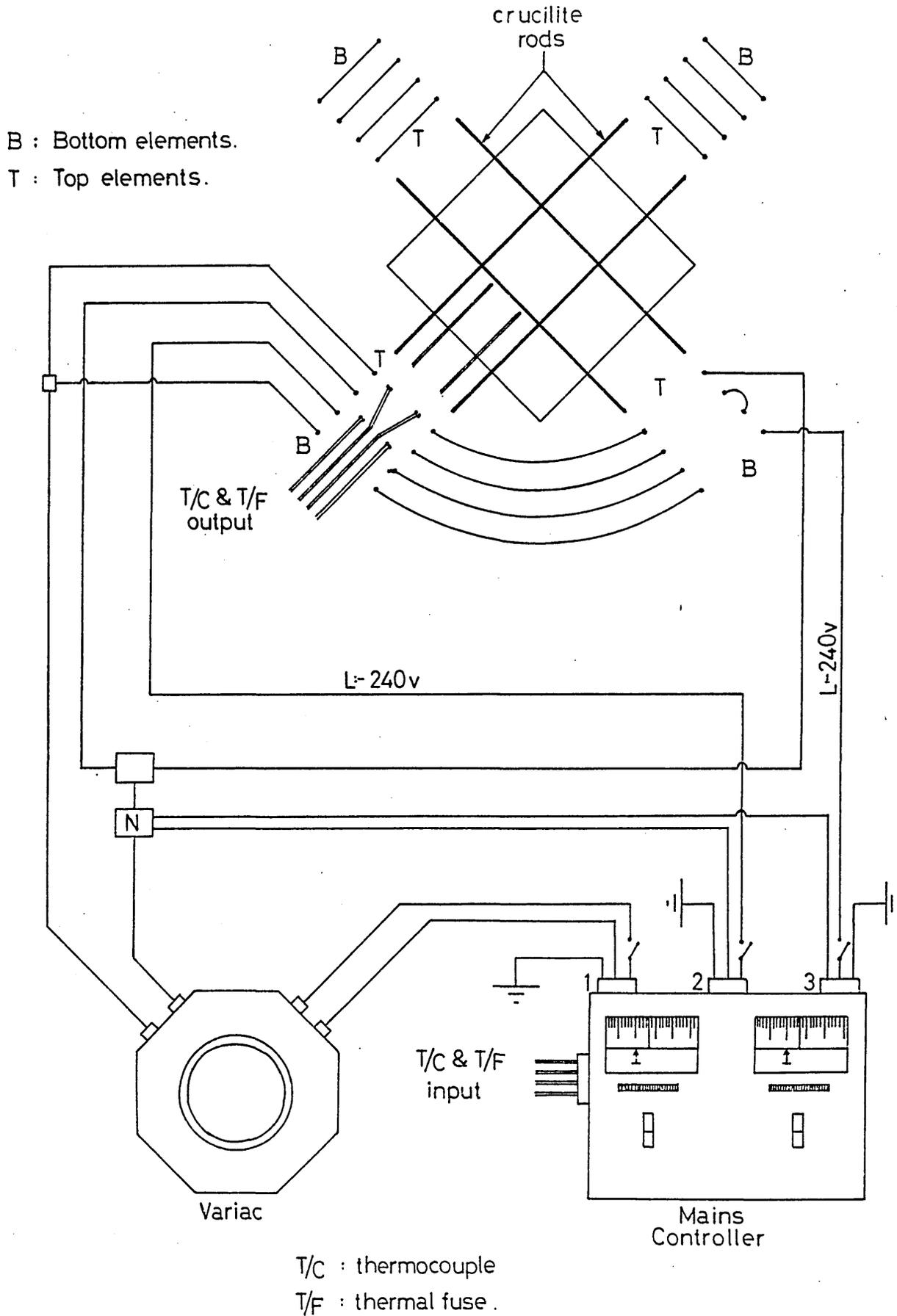


Figure 11 : Circuit diagram for middle furnace elements.

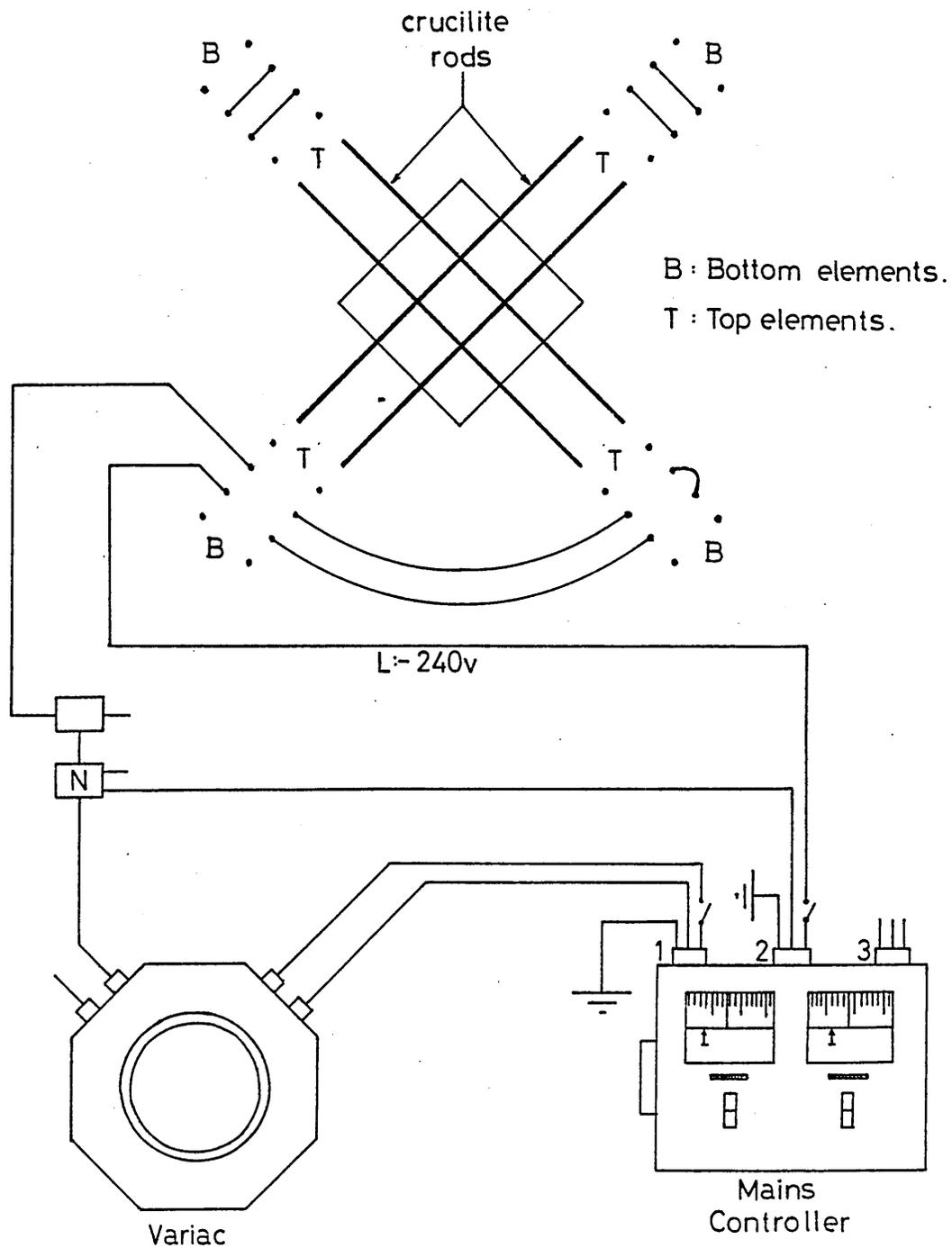


Figure 12 : Circuit diagram for top and bottom furnace elements .

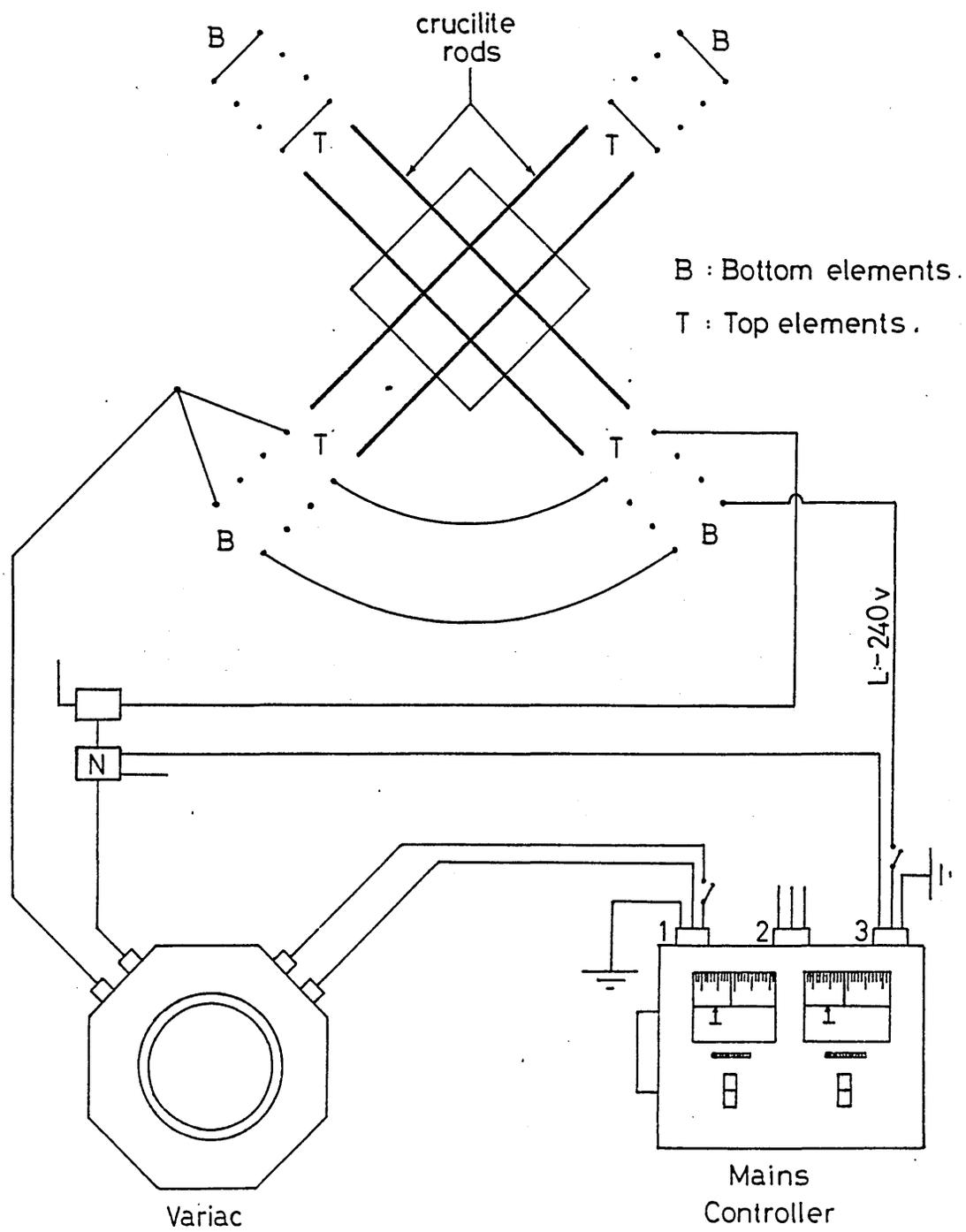
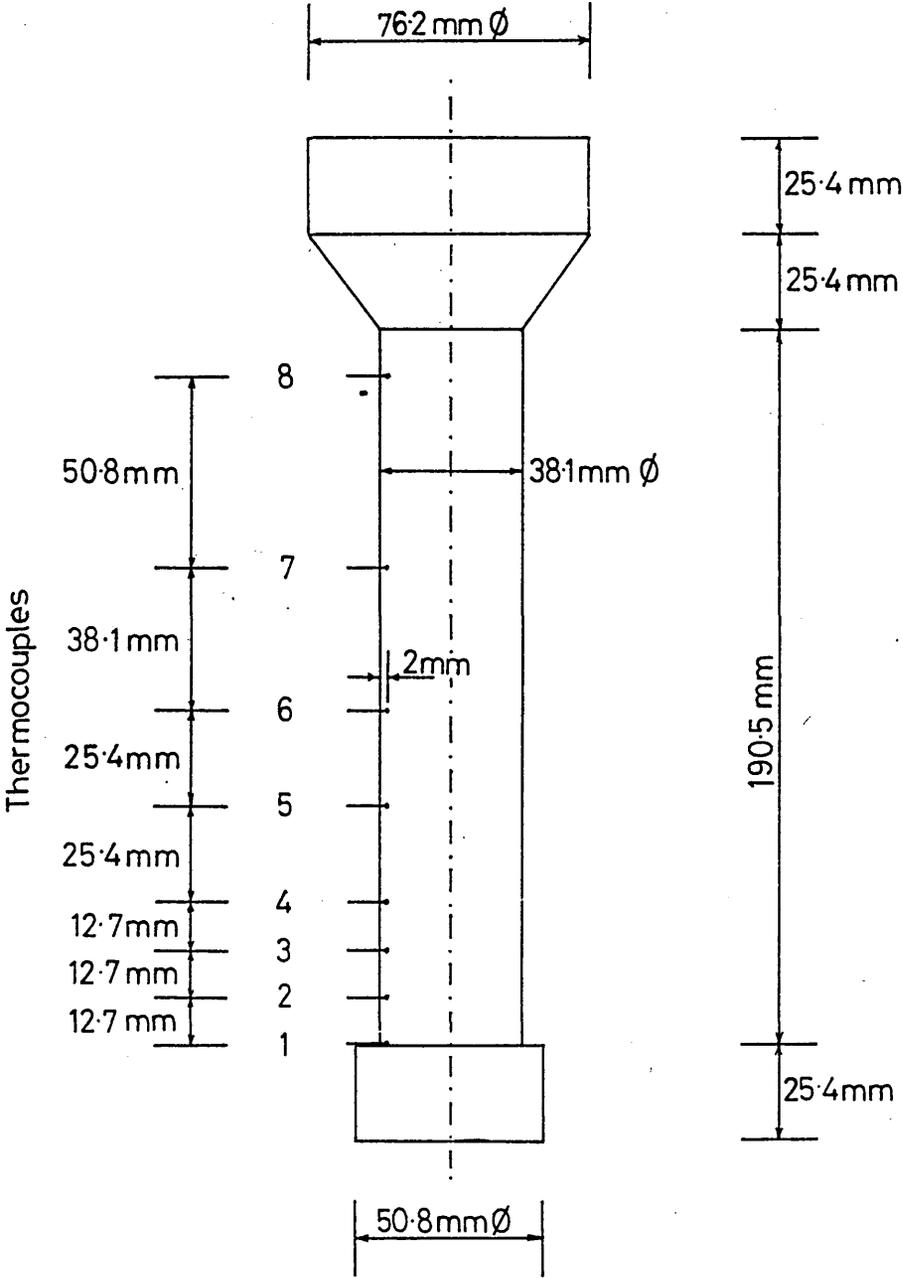


Figure 13 : The internal profile of the mould .



Scale
 2"
 4cm

TABLE 5 MOULD SPECIFICATIONS

MOULD COMPONENT	HEIGHT (mm)	INTERNAL DIAMETER (mm)
Feeder Head	50.8	Upper 76.2 Lower 38.1
Sample Section	190.5	38.1
Chill Seat	25.4	44.5
Overall	267.0	-

TABLE 6 MOLOCHITE SUSPENSION

Solution Composition (cm ³)	: 4546 Syton; 6 Lissapol; 12 Octanol
Specific Gravity	: 1.85 (100 mesh suspension)
Powder Specifications	: 200 and 100 mesh

TABLE 7 COPPER CHILL SPECIFICATIONS

CHILL PARAMETERS	HEIGHT (mm)	EXTERNAL DIAMETER (mm)
Overall	88.9	-
Locating Section	25.4	44.5
Base Section	63.5	63.5
Inlet Pipe/ Chill Face Separation	9.5	-

TABLE 8 THERMOCOUPLE ASSEMBLIES

INITIAL ASSEMBLY	POSITION IN MOULD	FINAL ASSEMBLY
(a)	mm (inches)	(b)
k	190.5 (7.5)	
	177.8 (7)	8
j	152.4 (6)	
i	127.0 (5)	7
h	101.6 (4)	
	88.9 (3.5)	6
g	76.2 (3)	
f	63.5 (2.5)	5
e	50.8 (2)	
d	38.1 (1.5)	4
c	25.4 (1)	3
b	12.7 (1.5)	2
a	0 (0)	1

Thermocouples: Pt - Pt, 13% Rh; 0.50mm diameter wire

TABLE 9 - THE EFFECT OF CARBON 'PICK-UP' ON THE COMPOSITION
OF INDUCTION MELTED CAST IRON

SUSCEPTOR SPECIFICATION (MELT NUMBER)	CARBON CONTENT (MASS %)				COMMENTS BASE MELT III (TABLE 1)
	SAMPLING TIME				
	0	5	10	15	
Cold Uncoated (1)	-	4.36	-	4.57	Excessive Carbon 'Pick-up' necessitates the use of 'Zircon' coated Susceptors.
Hot Uncoated (2)	4.12	4.35	4.40	4.40	
'Zircon' Coated (3)	3.68	3.78	3.79	3.792	Spalling prior to melting the metal.
Hot 'Zircon' Coated (4)	3.69	3.64	3.742	3.84	Spalling prior to charge addition.

TABLE 10 - THE VARIATION OF CARBON, SULPHUR AND MANGANESE CONTENT WITH HOLDING TIME AFTER MELTING IN A PRE-HEATED 'ZIRCON' COATED GRAPHITE SUSCEPTOR - MELT PRACTICE A

MELT NO.	SAMPLE TIME (Mins)	COMPOSITION (MASS %)			COMMENTS
		C	S	Mn	
5	0	4.24	0.492	0.18	BASE MELT COMPOSITION III - TABLE 1 S Addition as FeS, Table 1 = 1.65% Total S = 1.668%. S loss = 0.018% (15 mins.) Mn addition = 0. Total Mn = 0.2% Mn loss = 0.03% (15 mins)
	5	4.24	0.645	0.18	
	10	4.19	1.425	0.15	
	15	4.13	1.650	0.17	
6	0	4.26	0.176	0.88	S Addition = 0.185%. Total S = 0.203% S Loss: (gain 0.013% after 10 mins.) Mn Addition (High N ₂ Fe-Mn Table 1) = 0.8 mass% Mn. Total Mn = 1.00%. Mn loss 0.12% (10 mins.)
	5	-	-	-	
	10	4.57	0.216	0.88	
	15	-	-	-	

TABLE II. A SUMMARY OF THE PROCEDURES FOR MELTS 6 TO 17.

MELT NO.	MELT PRACTICE (3.7)	IRON COMPOSITION TABLE I	ADDITIONS TABLE I % S, % Mn % Cr. as FeCr:PURE	POURING TEMP. °C.	T/C POSITION TABLE 8	FURNACE CONDITIONS		DATA LOGGER (3.10)	FIGURE NUMBER	FRACTURE		COMMENTS
						CONSTRUCTION (3.3)	TEMP. °C (3.3)			PLATE NO.	COLOUR	
6	A	III	0.18% S 0.87% Mn	1250	127mm only	Unsectioned	-	I	-	-	Grey	Mould supported outside the furnace by clamp stands. This demonstrated effectiveness of KOS cement in sealing the T/Cs and Cu chill in place. Casting was used to develop the fracture technique.
7	A	I	-	1320	a	"	1150	I	14	18	Grey	Cooling rates were generally too high. The furnace 'switch-off' times delayed. The cooling curves show heat loss from the top of the casting incomplete filling of the feeder head.
8	A	I	3% pure Cr.	1240	a	"	1150	I	15	19	White	D/L malfunction. Complete cooling curves were only obtained for T/Cs 'b' only. The fracture showed evidence of non-unidirectional heat flow ensate for this the mould preheating furnace was sectionalised.
9	A	II	-	1240	b	"	1150	-	-	-	-	The melt 'ran-out' due to the mould cracking.
FURNACE COOLING PROFILE - NO METAL IN THE MOULD												
10	A	II	-	1250	b	Sectioned	1150	2	-	20	Grey	Inflections on the cooling curves showed the effectiveness of sectioning the furnace on reducing the cooling rate. The D/L malfunctioned after no cooling curves were obtained due to the D/L malfunctioning.
11	B	II	0.001% Bi FeCr. Pure	1480	b	"	1150	2	-	-	-	The melt 'ran-out' due to the mould cracking, possibly as a result of temperature required for the addition of Bi to the melt. Hereafter, additions are to be made to achieve a white iron structure.
12	B	II	2.71% 2.6%	1300	b	"	1250	2	17	21	White	Variations of ± 600°C indicated that the data logger had malfunctioned casting exhibited a good unidirectional alignment of structure.
13	B	(12) II&III	3.03% 2.89% 3.03% 2.89%	1310 1310	b b	" "	1250 1250	2 2	- -	- -	- -	The data logger malfunction precluded the obtaining of cooling curves. Casting was very porous and was subsequently melted down for Melt 15.
14	B	III	3.09% 2.50%	1310	b	"	1250	2	18	22	White	The melt was earthed through the no. 8 T/C via a C.R.O. The D/L performed satisfactorily. Inflections on the cooling curves concurrent with the 'switch-off' times suggests excess heat input. The 'switch-off' times were further delayed. The cast structure was satisfactory.
15	B	(13) II&III	1.80% 1.00% 2.8% from melt (13)	1310	b	"	1250	2	19	23	White	The melt was earthed via the D/L patch-board. The performance was satisfactory. Cooling curve inflections suggest the need for further reducing the 'switch-off' times of the top elements. The cast was reheated and the output from the T/C was monitored via a C.R.O.. The cast structure was satisfactory.
16	B	III	3.24% 2.33%	1300	b	"	1250	2	20	24	White	The data logger was not earthed. The melt was isolated from earth by the clamp stand on a Sandanyo board. The D/L performed satisfactorily. Positioning of the no. 7 and 8 thermocouples suggests heat loss from the casting. Hereafter a Kaowool plug is to be placed above the feeder.
17	B	III	3.10% 2.40%	1315	b	"	1250	2	21	27	White	The earthing of the system was as for melt 16. The no. 7 and 8 T/Cs were electrically insulated by Silica sheaths. Temperature variations of ± 100°C were observed. Inflections encountered on all cooling curves indicate a need to further reduce the furnace 'switch-off' times to 0,12,20 mins.. Structure

C.R.O. - Cathode Ray Oscilloscope D/L - Data Logger T/C - Thermocouple

ELEMENT	SEPARATION METHOD	ABSORPTION	TITRANT	COMMENTS
Carbon + 1% of reported composition)	Roasting turnings to produce CO + CO ₂	Dimethyl Formamide Methanolamine (to absorb H ₂ O) and indicator	Non-aqueous. Tetrabutyl ammonium hydroxide (N/10) *Problems could be incurred if graphite is weighed with iron.	The titrant severs the CO + CO ₂ bonds with hexagonals thus altering the alkalinity*
Sulphur + 1% of reported composition)	Roasting turnings to produce SO ₂	Weak peroxide solution	Sodium tetraborate	
Phosphorus (error - 0.002%)	Turnings dissolved to precipitate the phosphomolybdate which removes alkalinity	Standard caustic soda solution	Back titration - Nitric acid to end Point.	Back titration produces alkalinity which is proportional to the phosphorus percentage
Chromium (error - 0.005%)	Turnings produce Cr 7 by oxidation on hot plate.	Cr 7 reduced to Cr 3 with ferrous ammonium sulphate.	Back titrate with excess iron sulphide solution which reoxidises chromium to Cr 7 state.	Solution colour changes from green to yellow.
Silicon + 1% of reported composition)	Silicon (turnings) is hydrated to silica; filtered on to a pulp pad, carbonaceous material is removed by burning at 900°C. The silica remaining is weighed and converted to silicon percent by multiplying by a factor compensating for the oxygen. (Inhomogeneity causes problems).			
Manganese (error - 1% of reported composition).	Colourimetric. Turnings dissolved in spekka acid (H ₂ SO ₄ + H ₃ PO ₄). The magenta solution is analysed on an absorption spectrophotometer.			
Titanium (error - 1% of reported composition)	Colourimetric. Turnings are dissolved in sulphuric acid; Hydrogen peroxide is used to colour the solution yellow (time is required for completion); The solution is analysed on an absorption spectrophotometer. Segregation is likely in the sample. Analysis is viable for soluble and total but not combined titanium. Time dependent titration.			
Nitrogen	Kjeldahl process. Error impossible to ascertain as stated (3.10.2). This was performed on both types of samples (Performed by B.S.C.).			
Titanium	Both wet and spectrographic methods were used by B.S.C. using turnings and white samples respectively. The result quoted is for total and soluble titanium.			

TABLE 13 - SPECIFIED PERFORMANCE DATA

CREDSHIRE 500 ANALOGUE SCANNER

Max. Signal Input	:	100 volts
Type	:	D.C. or Peak A.C.
Channel Arrangement	:	100 Dipole (5 x 20)
Max. Scan speed	:	10 Channels/sec
Min. Scan speed	:	1 Channel/sec
Scan Mode	:	Auto or Manual
Max. No. Channels	:	999

TABLE 14 - PERFORMANCE DATA - 220 DRIVE CASSETTE UNIT.

Character Storage	50,000
Single Line Accommodation	70 Characters
Out-put Format	9 Characters/Channel
Print-out Format/Channel:	Characters
Channel No.	2
Polarity	1
Temperature	5
Space	1
Time	4 at each line end
Max. Word Count	(70 - 4 =) 66
Word Count/Line - Present Work	4
Total Scan	2 Lines

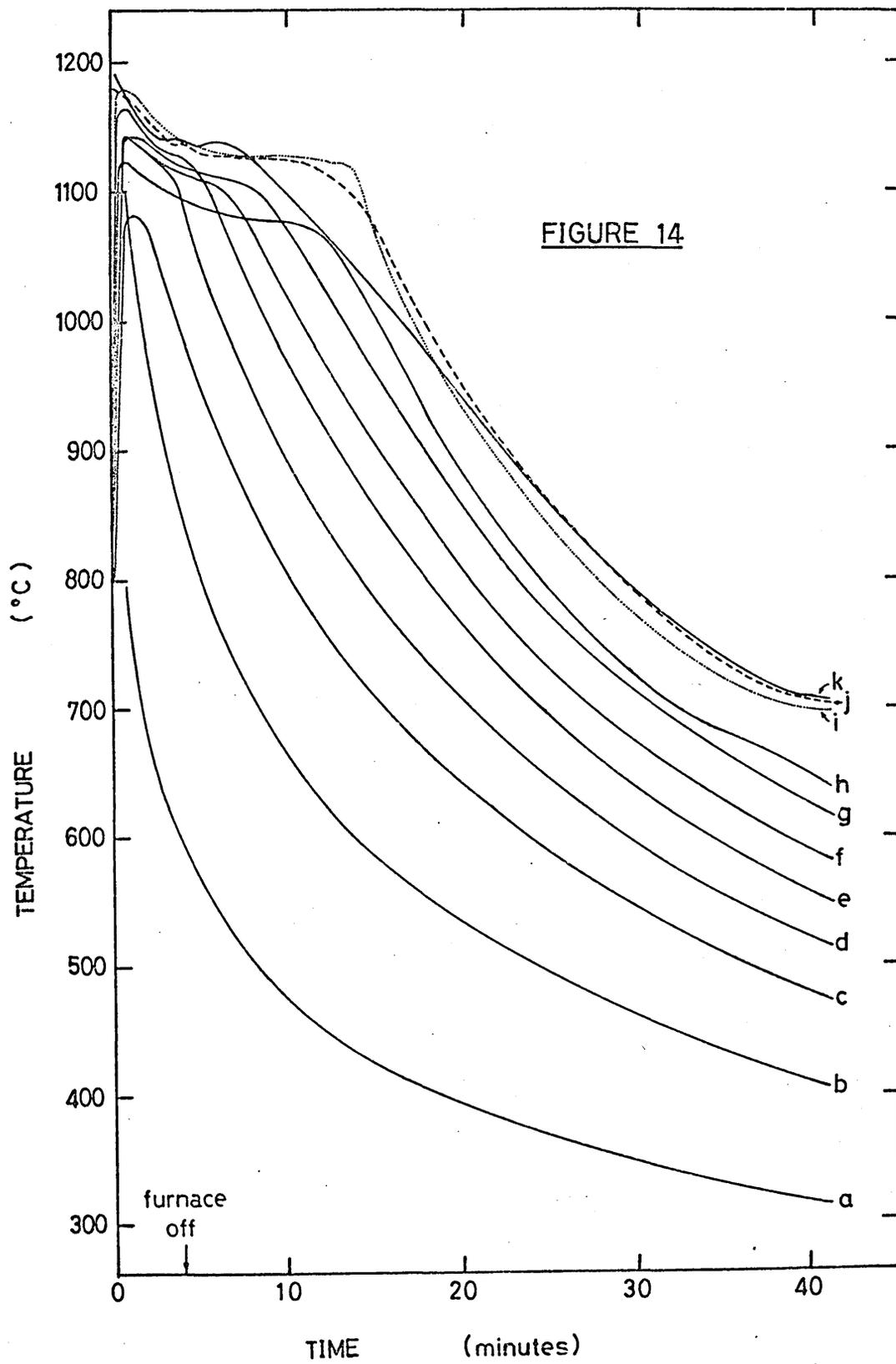


FIGURE 18

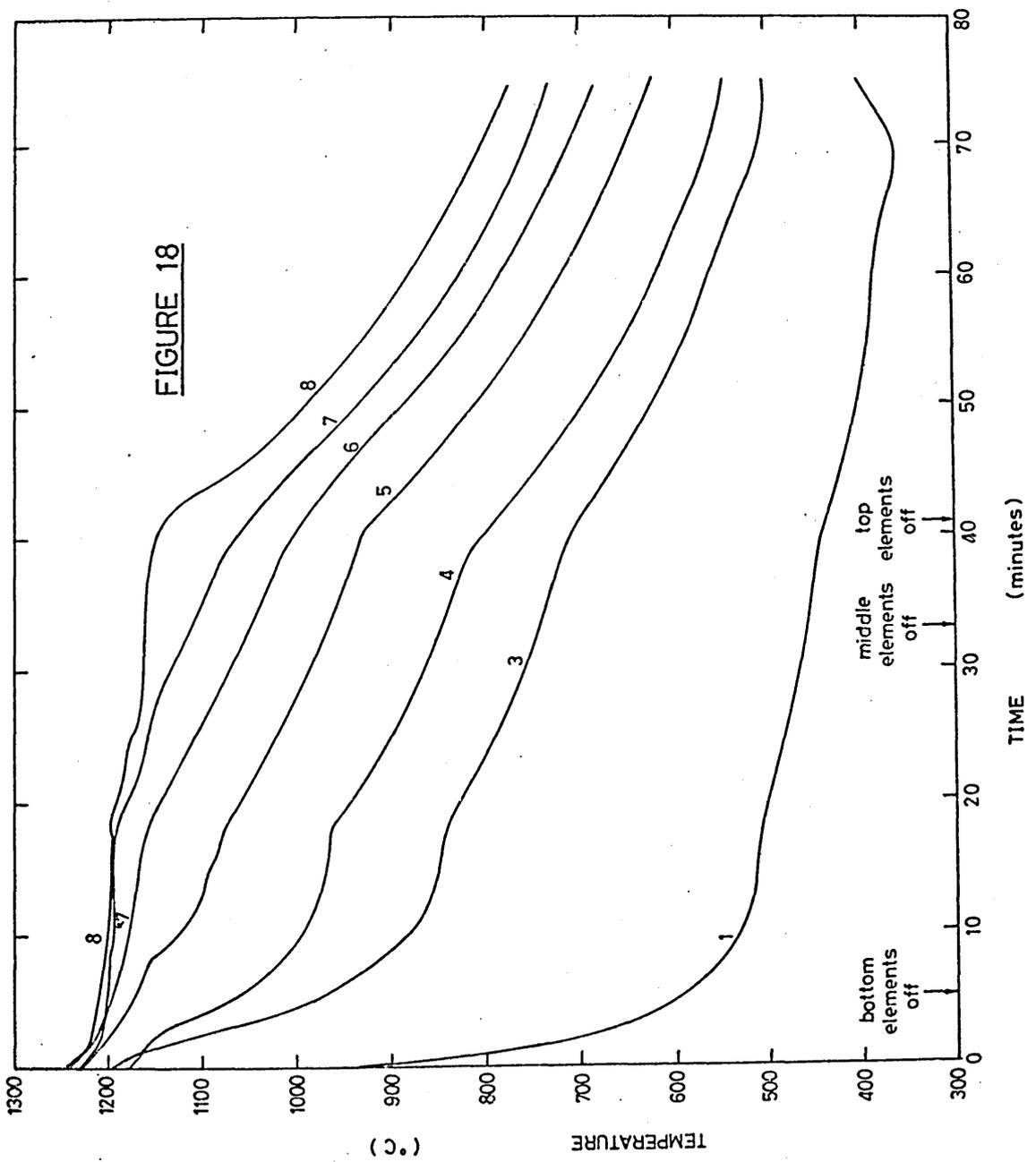
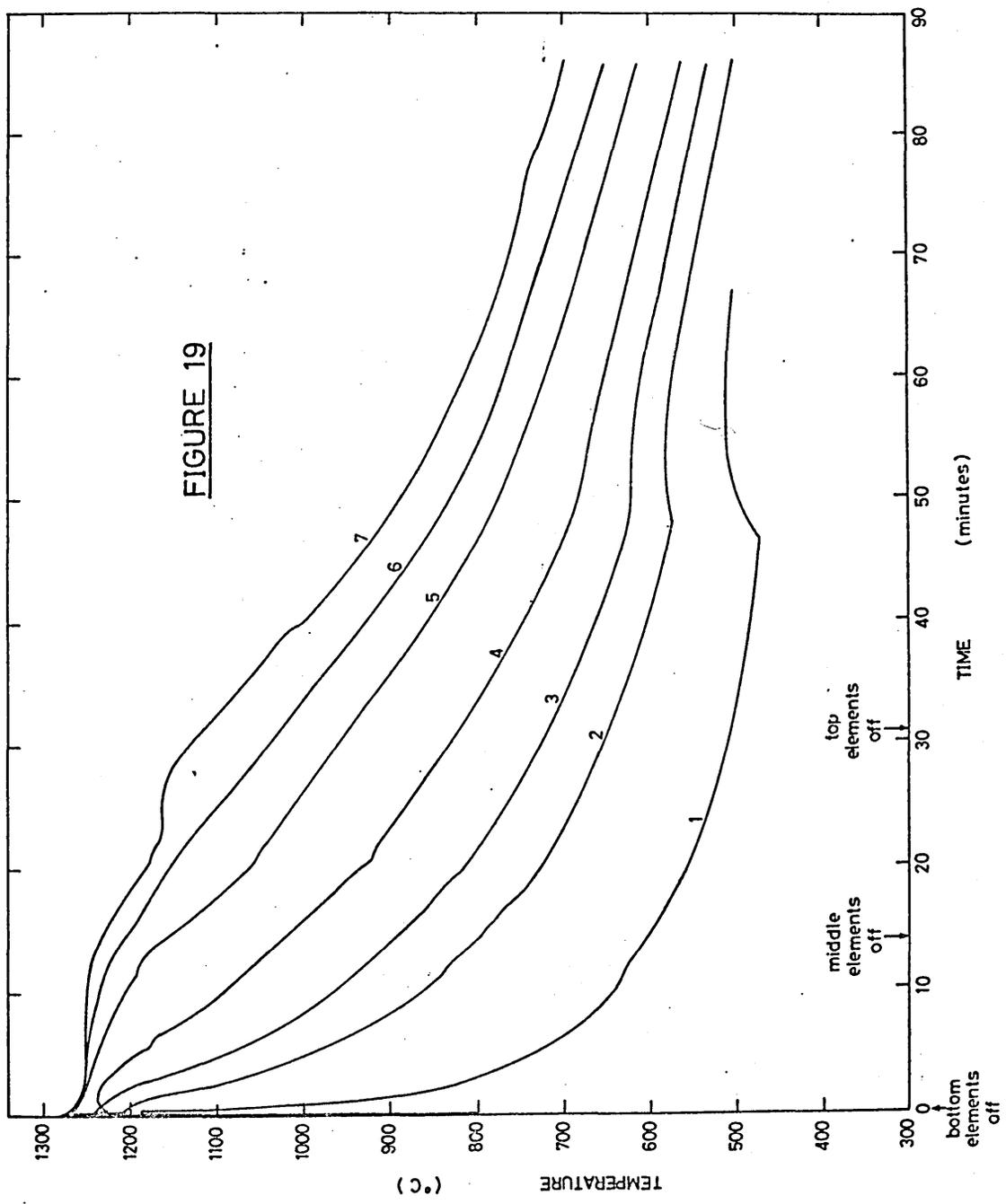


FIGURE 19



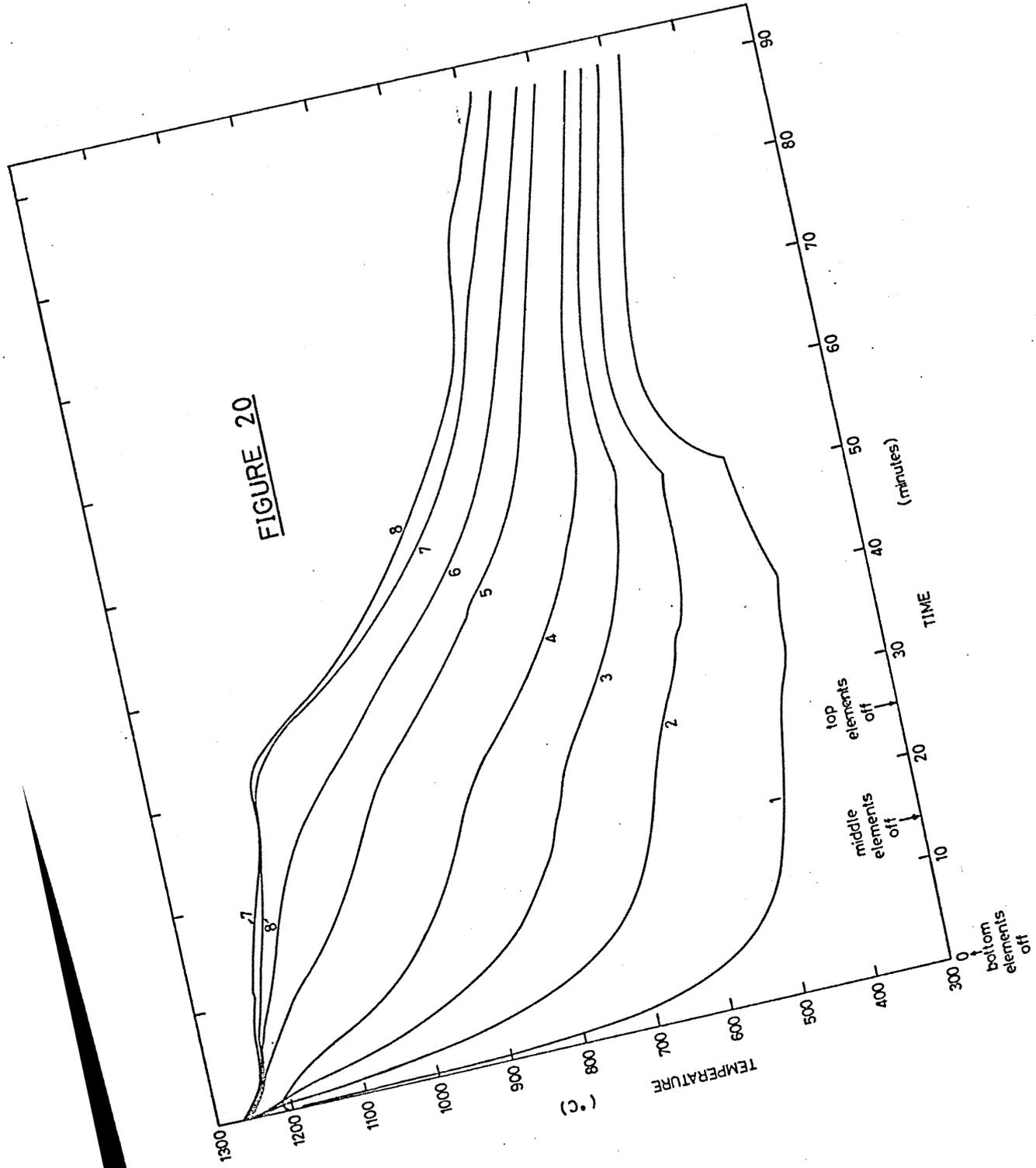
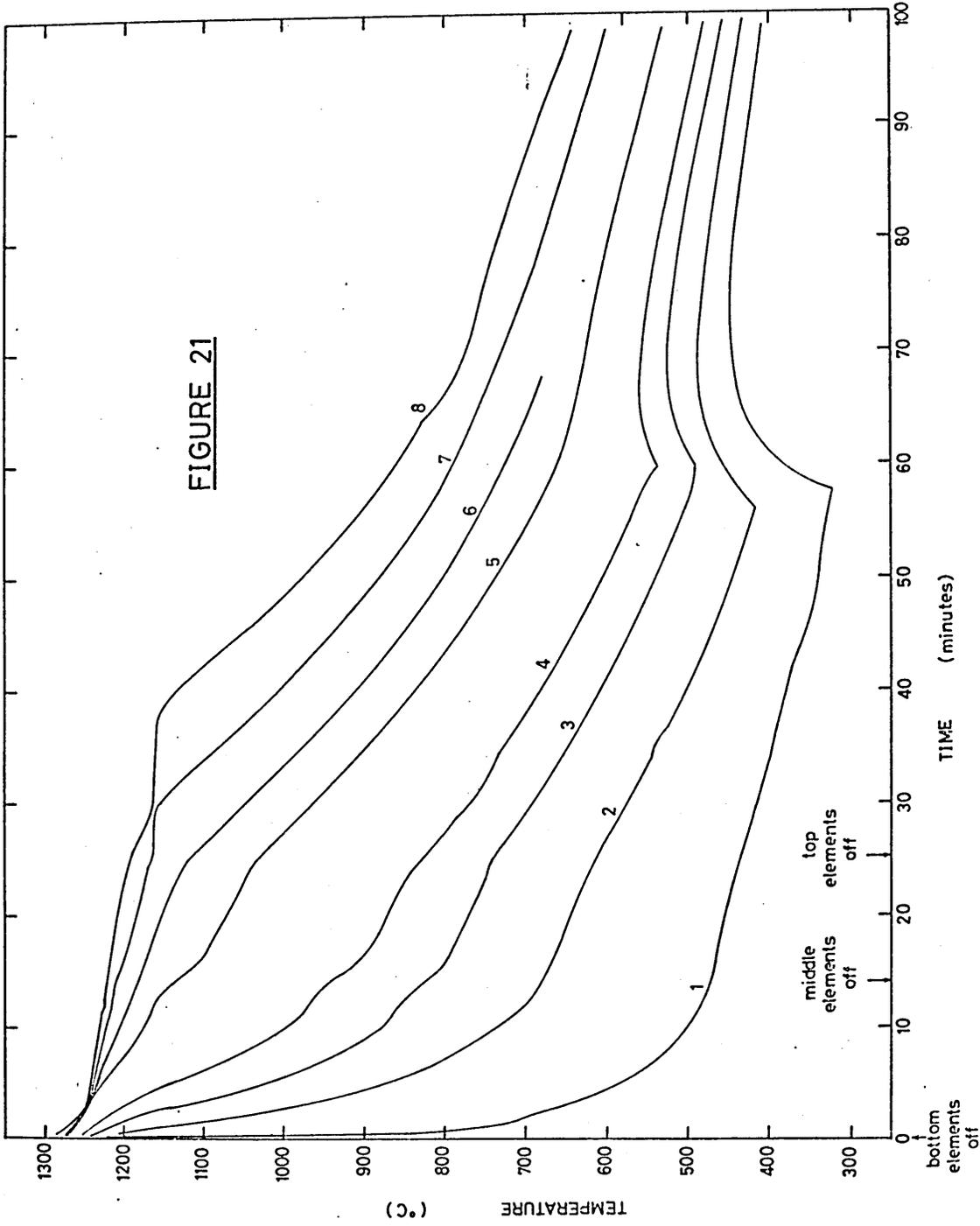
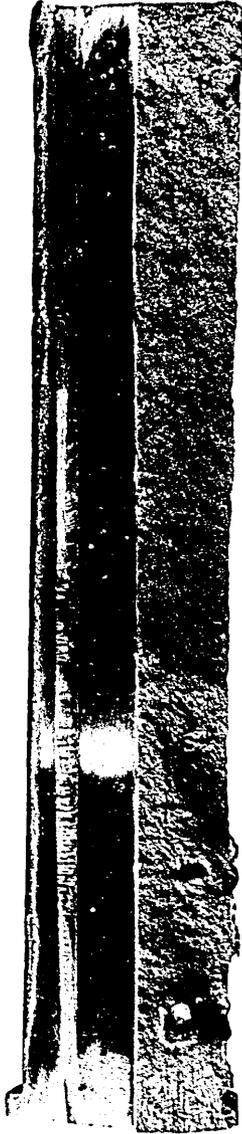


FIGURE 21









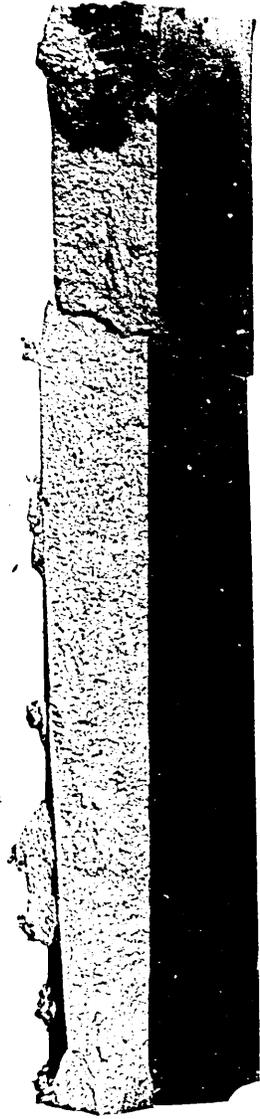




PLATE 83

C1. 127.1mm (19.05mm)
x 16

6.28°C/Min

PLATE 84

C1. 127.1mm (9.525mm)
x 63

6.28°C/Min

PLATE 85

C1. 177.8mm (19.05mm)
x 16

4.43°C/Min

PLATE 86

C1. 181mm (28.6mm)
x 16

4.35°C/Min



PLATE 79

B1. 182mm (36.6mm)
x 32

4.29°C/Min

PLATE 80

C1. 33.5mm (7mm)
x 16

32.51°C/Min

PLATE 81

C1. 63.5mm (9.525mm)
x 16

12.33°C/Min

PLATE 82

C1. 89mm (14mm)
x 63

9.79°C/Min

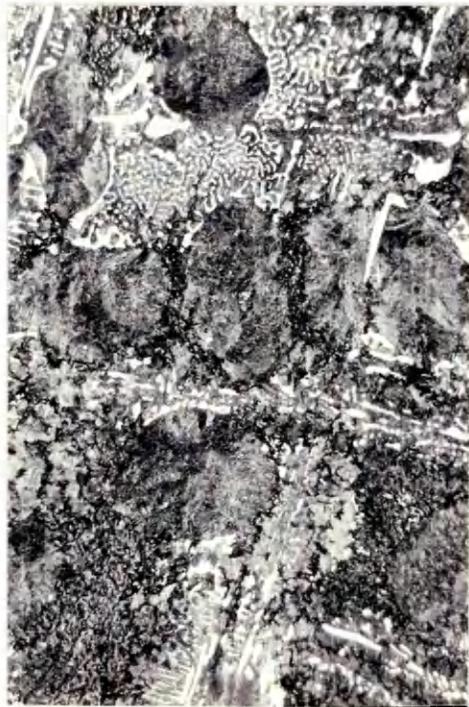
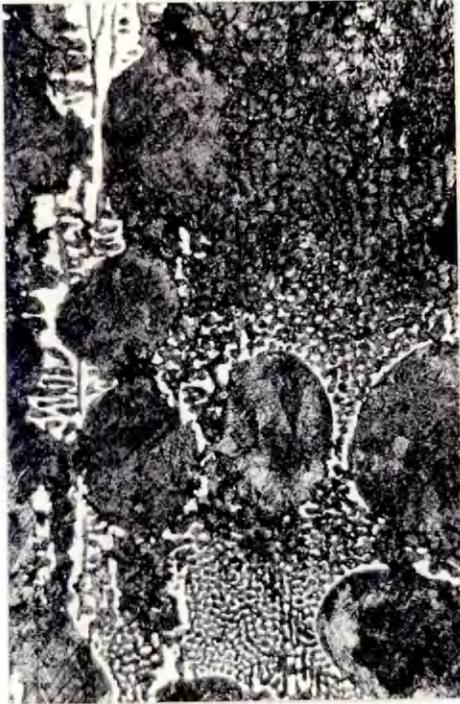


PLATE 75

B1. 89mm (26.1mm)
x 63

9.79°C/Min

PLATE 76

B1. 127.1mm (28.6mm)
x 63

6.28°C/Min

PLATE 77

B1. 127.1mm (31.1mm)
x 63

6.28°C/Min

PLATE 78

B1. 177.8mm (28.6mm)
x 63

4.43°C/Min



PLATE 71

B1. 38.1mm (29.6mm)
x 63

25.62°C/Min

PLATE 72

B1. 63.5mm (30.1mm)
x 16

12.33°C/Min

PLATE 73

B1. 64.5mm (29.6mm)
x 16

12.11°C/Min

PLATE 74

Enlargement of Plate 73
x 160

12.11°C/Min

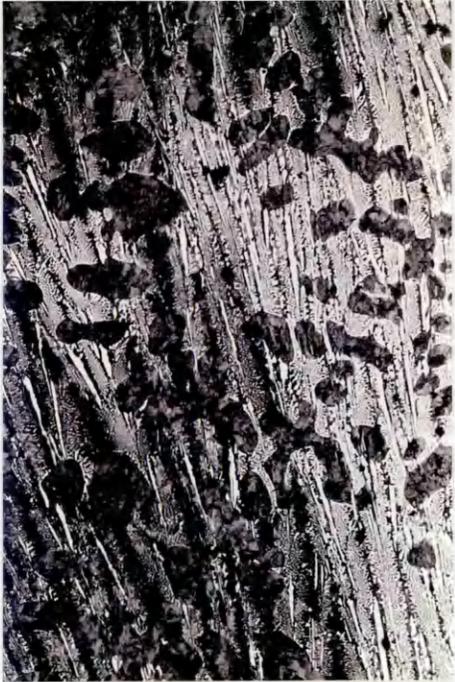


PLATE 69

A3. 177.8mm (19.05mm)
x 16

4.43°C/Min

PLATE 70

A3. 177.8mm (15mm)
x 16

4.43°C/Min

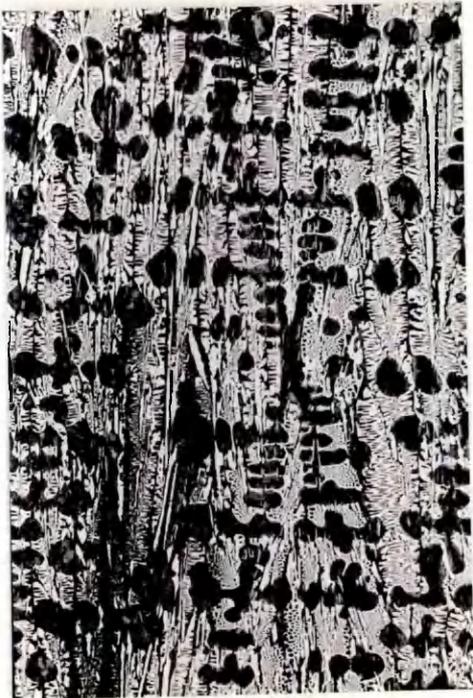
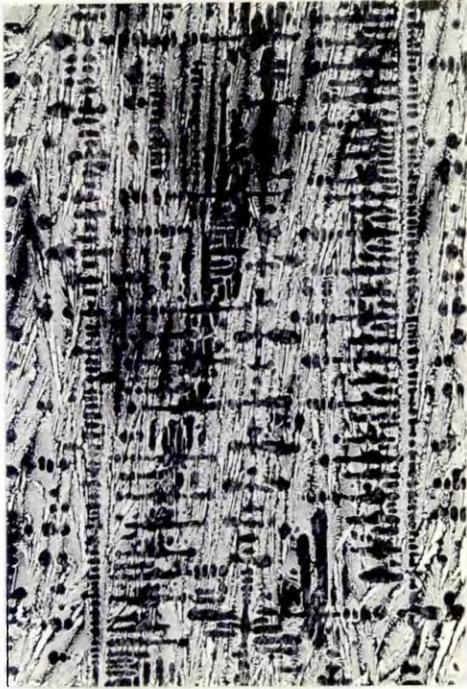
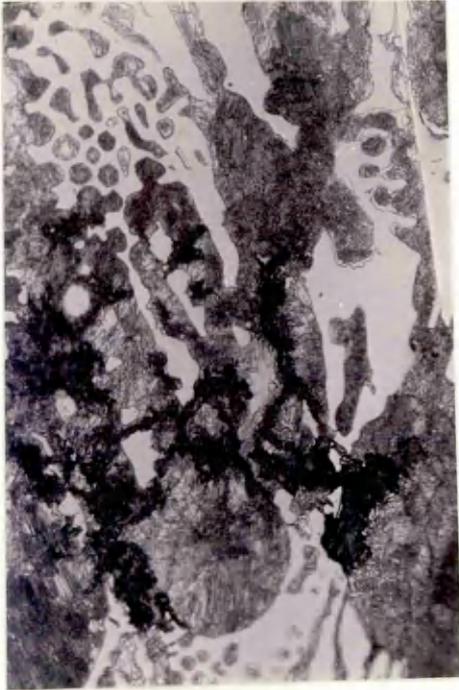


PLATE 65

A3. 38.1mm (9.525mm)
x 160

25.62°C/Min

PLATE 66

A2. 25.4mm (9.525mm)
x 16

48.10°C/Min

PLATE 67

A3. 63.5mm (19.05)
x 16

12.33°C/Min

PLATE 68

A2. 89mm (19.05mm)
x 16

9.79°C/Min



PLATE 63

A1c. 0mm (10mm L.H.S.)

x 16

635°C/Min

PLATE 64

Enlargement of Plate 63

x 63

635°C/Min

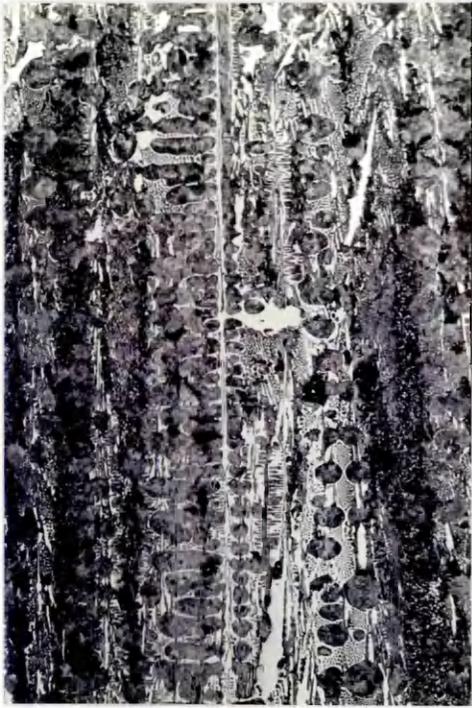


PLATE 60

A1a. 45mm (9.525mm)
x 16

21.18°C/Min

PLATE 61

A1a. 158mm (18.05mm)
x 16

5.50°C/Min

PLATE 62

A1b. 81mm (17mm)
x 16

10.42°C/Min



PLATE 59

ADDITIONAL BASE LOW NITROGEN CASTS

Cast A1a

Cast A1b

Cast A1c

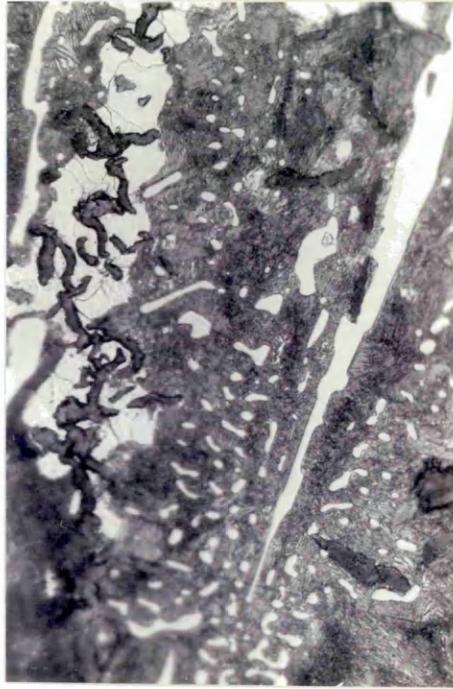


PLATE 56

A1. 185mm (19.05)
x 160

4.17°C/Min

PLATE 57

A1. 185mm (9.525mm)
x 63

4.17°C/Min

PLATE 58

A1. 185mm (10mm)
x 160

4.17°C/Min

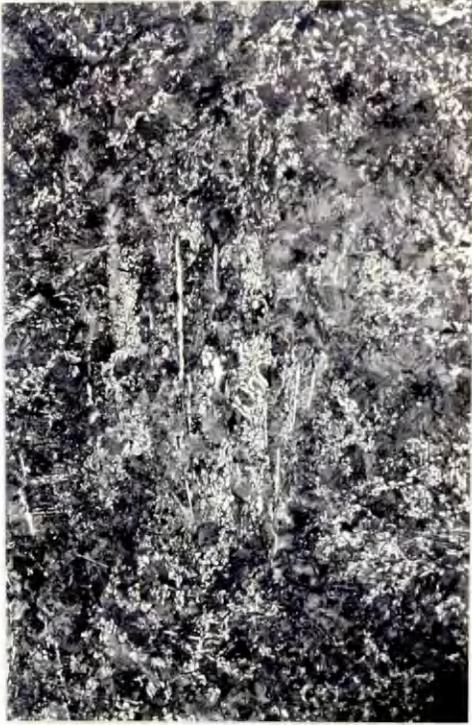


PLATE 52

A1. 89mm (19.05mm)
x 16

9.79°C/Min

PLATE 53

Enlargement of Plate 52
x 63

9.79°C/Min

PLATE 54

A1. 127.1mm (19.05mm)
x 63

6.28°C/Min

PLATE 55

A1. 177.8mm (9.525mm)
x 63

4.43°C/Min

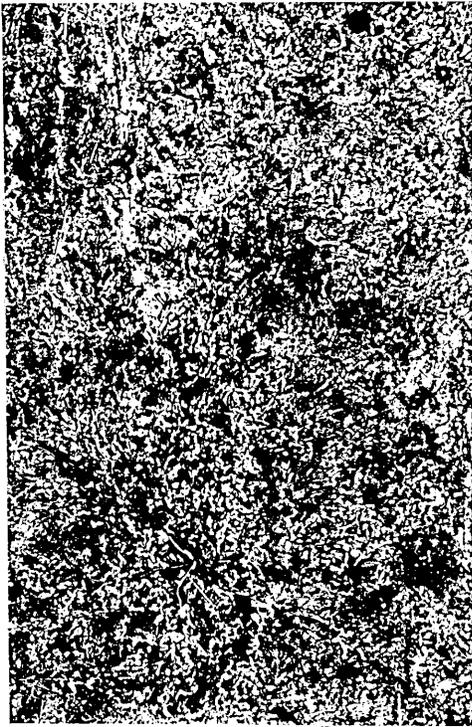


PLATE 49

A1. 89mm (9.525mm)

x 16

9.79°C/Min

PLATE 50

Enlargement of Plate 49

x 160

9.79°C/Min

PLATE 51

A1. 127.5mm (9.525mm)

x 32

6.17°C/Min



PLATE 46

A1. 63.5mm (34.1mm)

x 16

12.33°C/Min

PLATE 47

Enlargement of Plate 46

x 160

12.33°C/Min

PLATE 48

Enlargement of Plate 46

x 160

12.33°C/Min

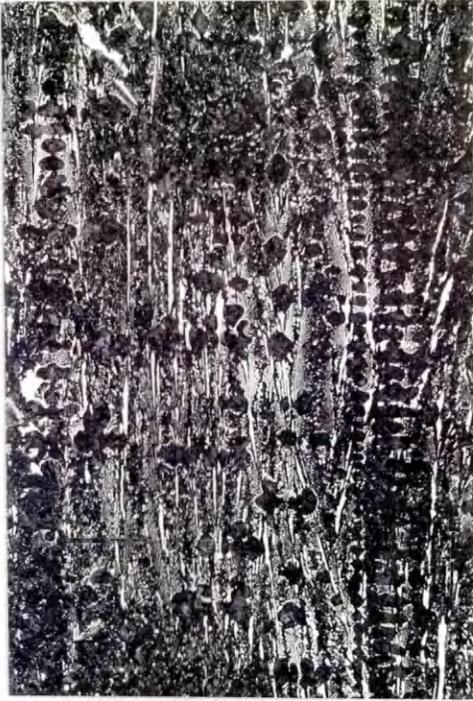


PLATE 44

A1. 38.1mm (9.525mm)

x 16

25.62°C/Min

PLATE 45

Enlargement of Plate 44

x 160

25.62°C/Min

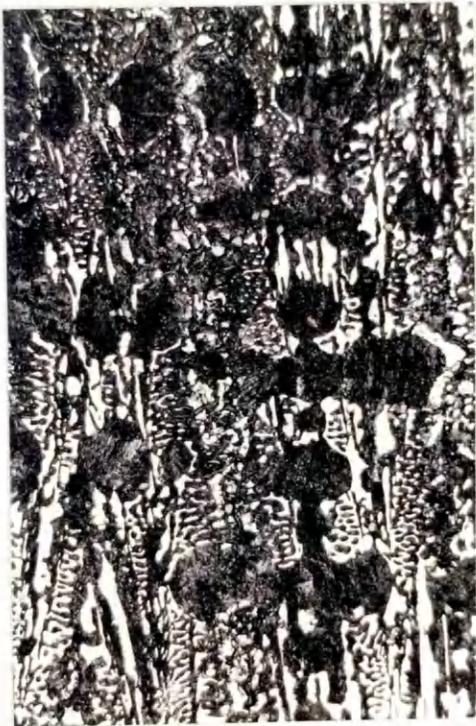


PLATE 40

A1. 25.4mm (19.01mm)
x 16

48.1°C/Min

PLATE 41

Enlargement of Plate 40
x 63

48.1°C/Min

PLATE 42

A1. 38.1mm (28.5mm)
x 63

25.62°C/Min

PLATE 43

Enlargement of Plate 42
x 160

25.62°C/Min

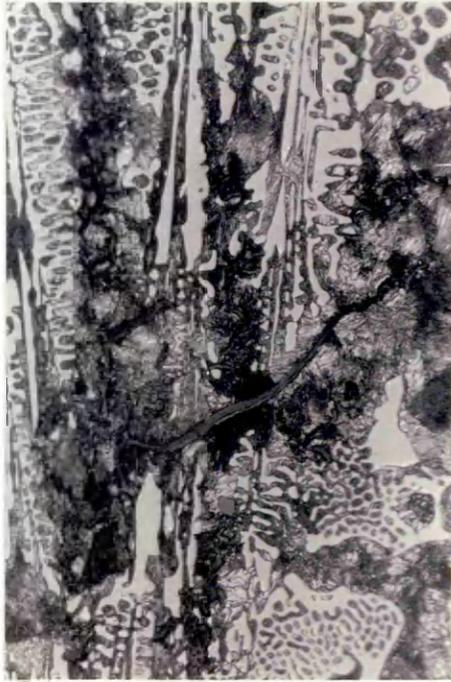
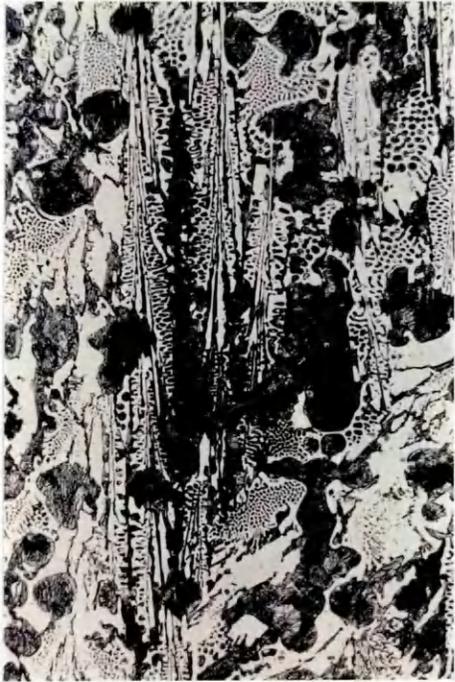
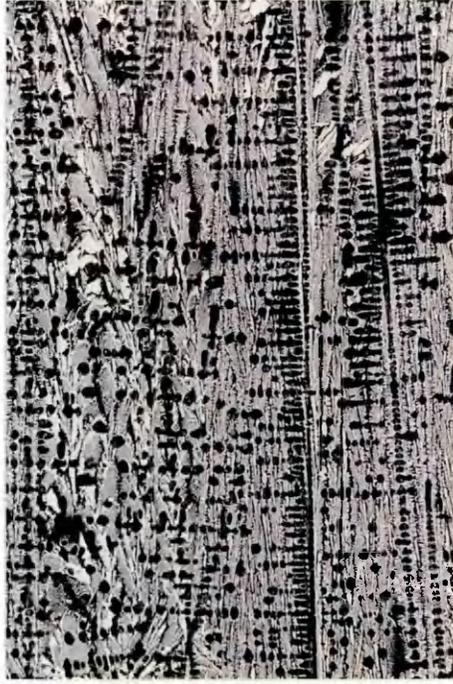
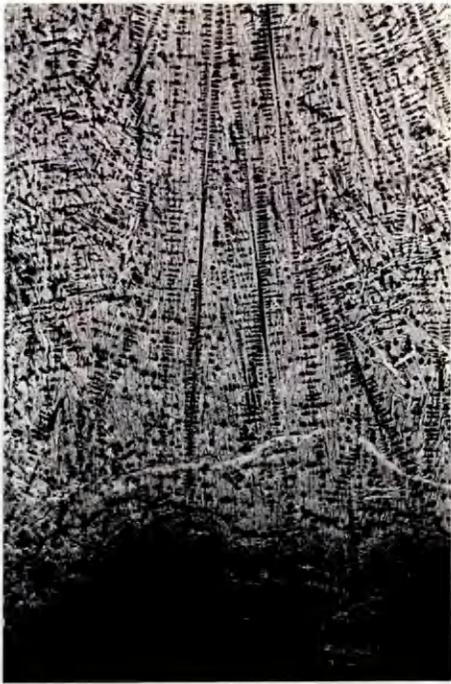


PLATE 36

A1. 0mm (19.05mm)
x 16

635°C/Min

PLATE 37

A1. 12.7mm (19.01mm)
x 16

123.97°C/Min

PLATE 38

Enlargement of Plate 37
x 63

123.97°C/Min

PLATE 39

Enlargement of Plate 37
x 160

123.97°C/Min

The details of the following microstructures, etched in 2% nital, are given as follows:-

Cast number, distance from the chill, (distance from the T/C edge) and magnification.

Cooling rate through the 'solidification arrest' - 1160°C - 1100°C .

The photographs are orientated with the chill/metal interface towards the bottom of the plates.

A1



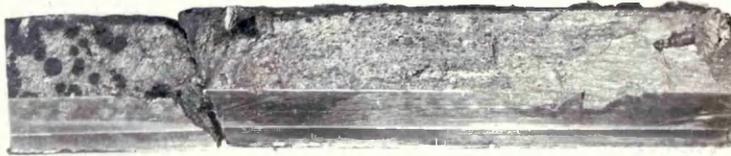
B1



C1



E1



F1



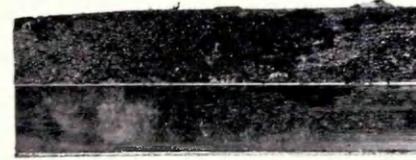
G1



A2



B2



C2



E2



F2



G2



PLATE 35

Fractured Castings for the Low Nitrogen Melt Programme

Figure 62 : The variation of overall cooling rate between 1160 and 700°C with distance from the chill-melt interface.

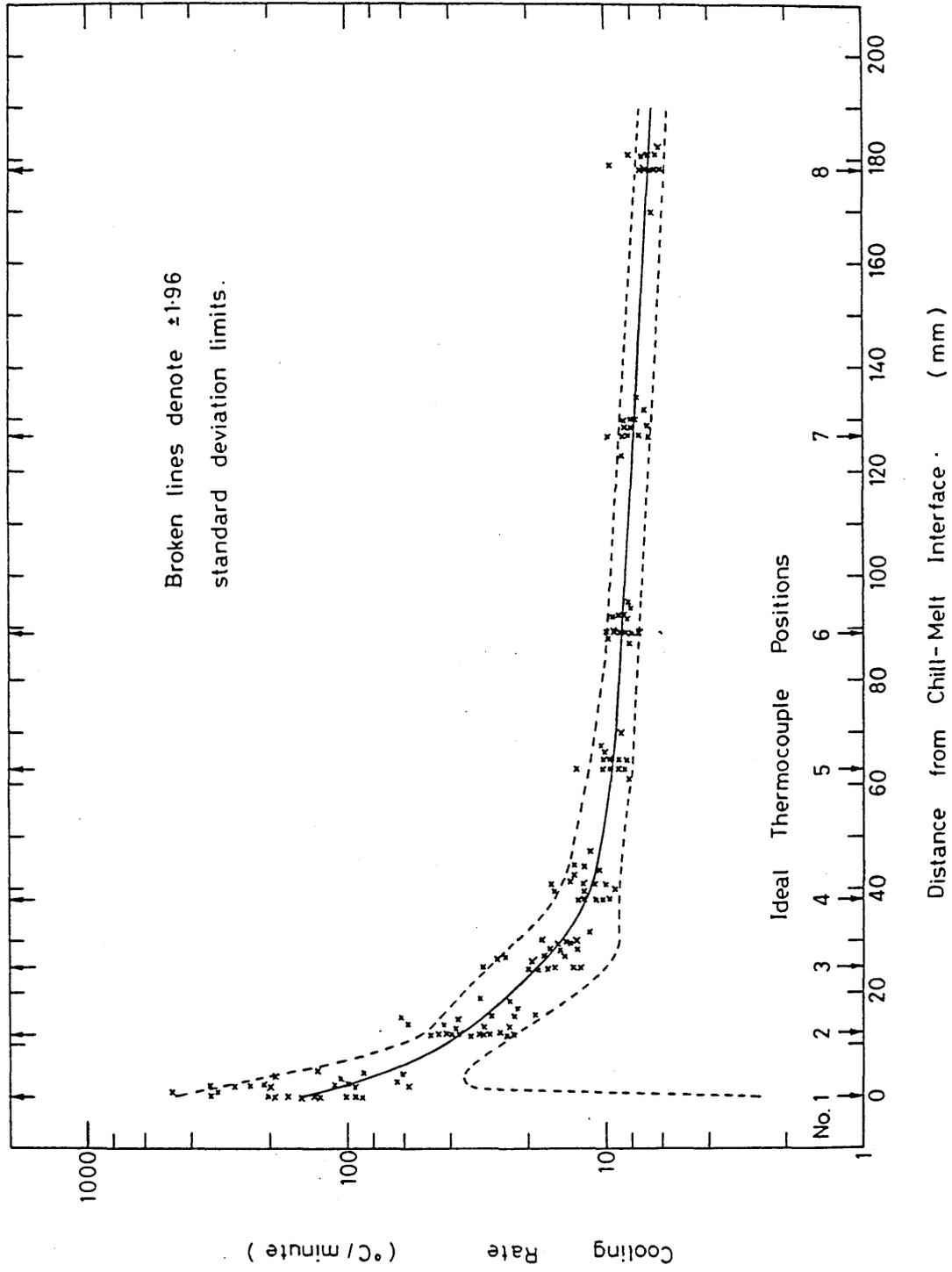
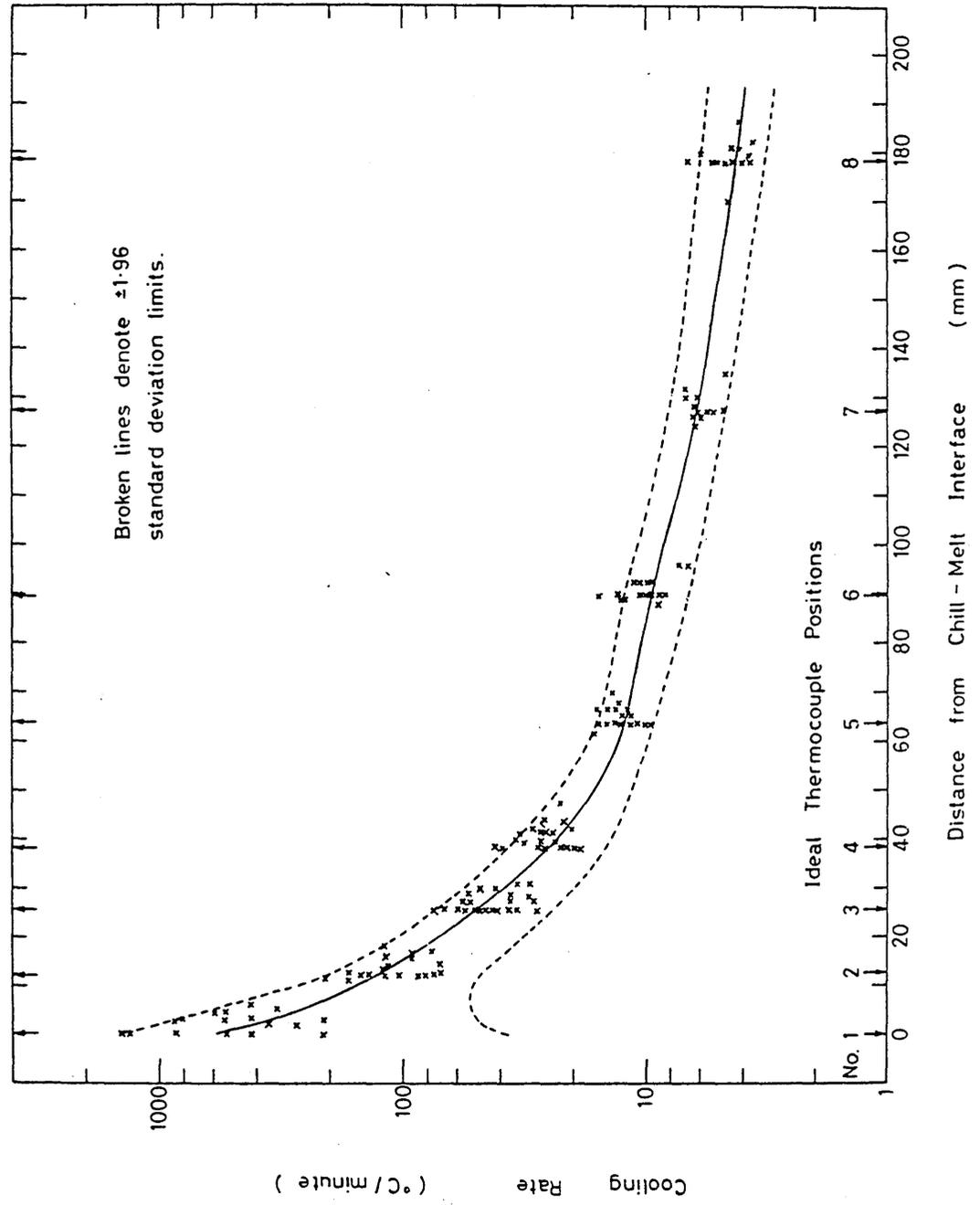


Figure 61 : The variation of overall cooling rate between 1160 and 1100 °C with distance from the chill-melt interface .



Statistical function	Thermocouple Number (1160-1100°C)								Thermocouple Number (1160-700°C)						
	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7
\bar{x}	635	123.97	48.10	25.62	12.33	9.79	6.28	4.43	156.48	35.97	18.59	11.83	9.67	8.81	7.78
v	117750	1474.75	145.07	35.71	2.28	1.92	0.58	0.34	6166.65	56.23	23.99	0.39	0.94	0.48	0.38
σ	343.15	38.4	12.04	5.98	1.51	1.39	0.76	0.59	78.53	7.50	4.90	0.63	0.97	0.69	0.61
$t_{0.966}$	672.57	75.27	23.61	11.71	2.96	2.72	1.49	1.15	153.92	14.70	9.60	1.23	1.91	1.36	1.20
$\bar{x} \pm 1.96\sigma$	1307.57	48.70	71.71	37.33	15.29	12.51	7.77	5.58	310.40	50.67	28.19	13.06	11.58	10.17	8.98
\bar{x}	635	123.97	48.10	25.62	12.33	9.79	6.28	4.43	156.48	35.97	18.59	11.83	9.67	8.81	7.78
-1.96σ	206.52	199.24	24.49	13.91	9.37	7.07	4.79	3.28	2.56	21.27	8.99	10.60	7.76	7.45	6.58
									Logarithmic Values						
$\bar{x} \pm 1.96\sigma$	3.1165	2.2994	1.8556	1.5271	1.1844	1.0973	0.8904	0.7466	2.4919	1.7048	1.4501	1.1159	1.0637	1.0073	0.9533
\bar{x}	2.8028	2.0933	1.6822	1.4086	1.0910	0.9908	0.7980	0.6464	2.1945	1.5559	1.2693	1.0730	0.9854	0.9450	0.8910
$\bar{x} \pm 1.96\sigma$	1.5748	1.6875	1.3890	1.1433	0.9717	0.8494	0.6803	0.5159	0.4085	1.3278	0.9538	1.0253	0.8899	0.8722	0.8182

Where \bar{x} is the mean of those melts whose thermocouples coincide with the aim positions.

v is the variance of the cooling rates.

σ is the standard deviation.

$t_{0.966}$ is the statistical significance limit - any results exceeding $|\bar{x} \pm 1.96\sigma|$ will be statistically significant

ACTUAL THERMOCOUPLE DISPLACEMENT (mm)

im Dist.	0	12.7	25.4	38.1	63.57	89	127.17	177.8
st/TC No.	1	2	3	4	5	6	7	8
A1	0	15.9	27.4	38.1	63.5	89	127.17	177.8
A2	0	12.7	25.4	38.1	63.5	89	127.7	177.8
A3	0	12.7	25.4	38.1	63.5	89	127.17	177.8
B1	0	12.7	25.4	38.1	63.5	89	127.17	177.8
B2	0	12.7	25.4	38.1	63.5	89	127.17	177.8
B3	0	12.7	25.4	38.1	63.5	89	127.17	177.8
C1	0	12.7	25.4	44	67	92	128.5	181.0
C2	3	15.7	27.4	40.1	63.57	89	127.17	178.0
C3	4.5	14	26.4	38.1	63.57	89	127.17	178.0
E1	0	12.7	25.4	38.1	63.57	89	127.17	178.0
E2	0	12.7	25.4	38.1	63.57	89	127.17	178.0
E3	3	12.7	25.4	38.1	63.57	89	127.1	170
F1	2.5	17.0	30.0	41.5	63.57	92.5	130.5	187
F2	3	19	30.0	41.0	70	94.0	132	178/181.5
F3	3	15.7	31.0	41.0	66	92	130.17	181
G1	1.5	14.5	29.5	44.0	63.57	92	127.17	178
G2	1.0	12.7	28.0	41.0	65.5	89	127.17	178
G3	5.0	12.7	25.4	47.6	63.5	95.5	134.5	182
A1'	2.5	-	25.4	39	-	-	127.1	179
A2'	3.5	12.7	28.4	42.5	63.5	89	127.1	178
A3'	6.5	12.7	29.0	41.0	65	-	-	178
B1'	2.0	13.7	25.4	38.1	65.57	89	127.17	178
B2'	0	12.7	25.4	38.1	63.5	89	127.17	178
B3'	0	12.7	25.4	38.1	63.5	89	127.17	178
C1'	5	16.7	30	43.5	63.5	89	127.17	178
C2'	2	14	29	41.6	64.5	87	127.17	177.8
C3'	3	14	27.5	39.1	63.5	89	123.17	177.8
D1'	4	16	32	39.6	61	89	129.1	178/181.5
D3'	4.5	19.7	31	38.1	63.57	95	127.1	178
F1'	0	12.7	25.4	38.1	63.5	89	127.1	178
F2'	0	16.0	27.4	42.6	67	89	128	178
F3'	3	15.7	25.4	41.1	68	92	130.2	181

ADDITIONAL CASTS

Ala	-	17	30	45	70	87	125	-
Alb	0	12.7	25.4	38.1	63.5	81	135	185.5
Alc	-	-	-	-	-	-	-	-
E1a	0	12.7	25.4	38.1	63.7	89	127.1	177.5
Cl a	NO GRAPH →							
F2a	0	12.7	25.4	38.1	63.7	89	127.17	178
Ala'	7	20	32.5	46	63.5	89	133.5	-
B3a'	3	12.7	25.4	38.1	63.5	89	127.17	178
C2a'	NO GRAPH →							

THE COOLING RATES ($^{\circ}\text{C}/\text{MIN}$) FOR THE $1160^{\circ} - 700^{\circ}\text{C}$ TEMPERATURE RANGE

Cast	Thermocouple Number							
	1	2	3	4	5	6	7	8
	85.87	23.50	14.57	11.50	9.61	8.52	8.09	7.34
	128.80	32.20	15.33	11.38	9.25	8.47	7.76	7.11
	153.33	45.35	13.33	12.20	10.06	9.47	7.89	7.08
	201.25	46.00	29.54	10.81	8.77	7.84	7.49	6.48
	357.78	42.37	16.43	11.97	9.88	8.59	7.74	6.57
	94.71	38.80	16.60	12.48	9.50	8.56	7.97	6.56
	189.41	41.28	20.38	13.59	10.66	9.58	8.61	7.19
	357.78	61.92	25.76	15.86	-	10.13	8.16	7.24
	184.00	57.50	18.94	11.80	8.80	8.13	7.37	6.63
	169.47	24.03	12.15	-	9.31	8.90	8.52	7.12
	-	-	20.25	11.42	9.94	8.87	7.80	7.08
	233.33	35.00	16.43	12.39	9.31	8.75	7.56	6.52
	189.76	32.20	14.04	13.86	9.64	8.77	7.76	6.69
	64.4	24.77	14.90	-	8.94	7.93	7.12	6.34
	111.04	28.75	14.98	12.15	9.85	8.99	8.01	6.78
	322.00	42.93	16.51	12.11	10.39	8.66	7.69	6.52
	460.0	26.83	13.31	10.59	8.92	8.50	7.39	6.55
	61.92	25.56	13.53	11.22	-	8.26	7.29	6.22
1'	115.00	34.26	20.40	13.70	11.22	10.46	9.97	9.70
1'	109.15	27.29	14.77	9.25	8.75	8.13	6.97	6.22
3'	134.17	48.79	15.56	11.46	9.33	8.70	8.05	7.40
1'	94.71	38.33	19.88	12.88	10.46	9.17	8.01	6.91
2'	94.71	38.33	19.88	12.88	10.46	9.17	8.01	6.91
3'	115.83	38.80	16.86	11.14	9.31	8.82	7.82	6.44
1'	178.89	22.68	14.98	10.88	9.17	8.59	7.51	6.61
2'	57.00	24.39	14.84	10.66	8.82	8.17	7.35	7.35
3'	268.33	32.53	17.22	12.06	13.14	9.82	9.12	7.42
1'	-	18.72	12.11	10.06	8.13	7.52	6.84	6.63
3'	89.44	30.67	16.68	11.38	8.97	8.07	6.93	6.11
1'	89.44	30.67	16.68	11.38	8.97	8.07	6.93	6.11
2'	137.02	37.44	20.77	13.55	10.35	9.33	8.15	6.75
3'	191.67	60.67	29.82	16.60	11.03	9.79	8.52	8.26

ADDITIONAL CASTS

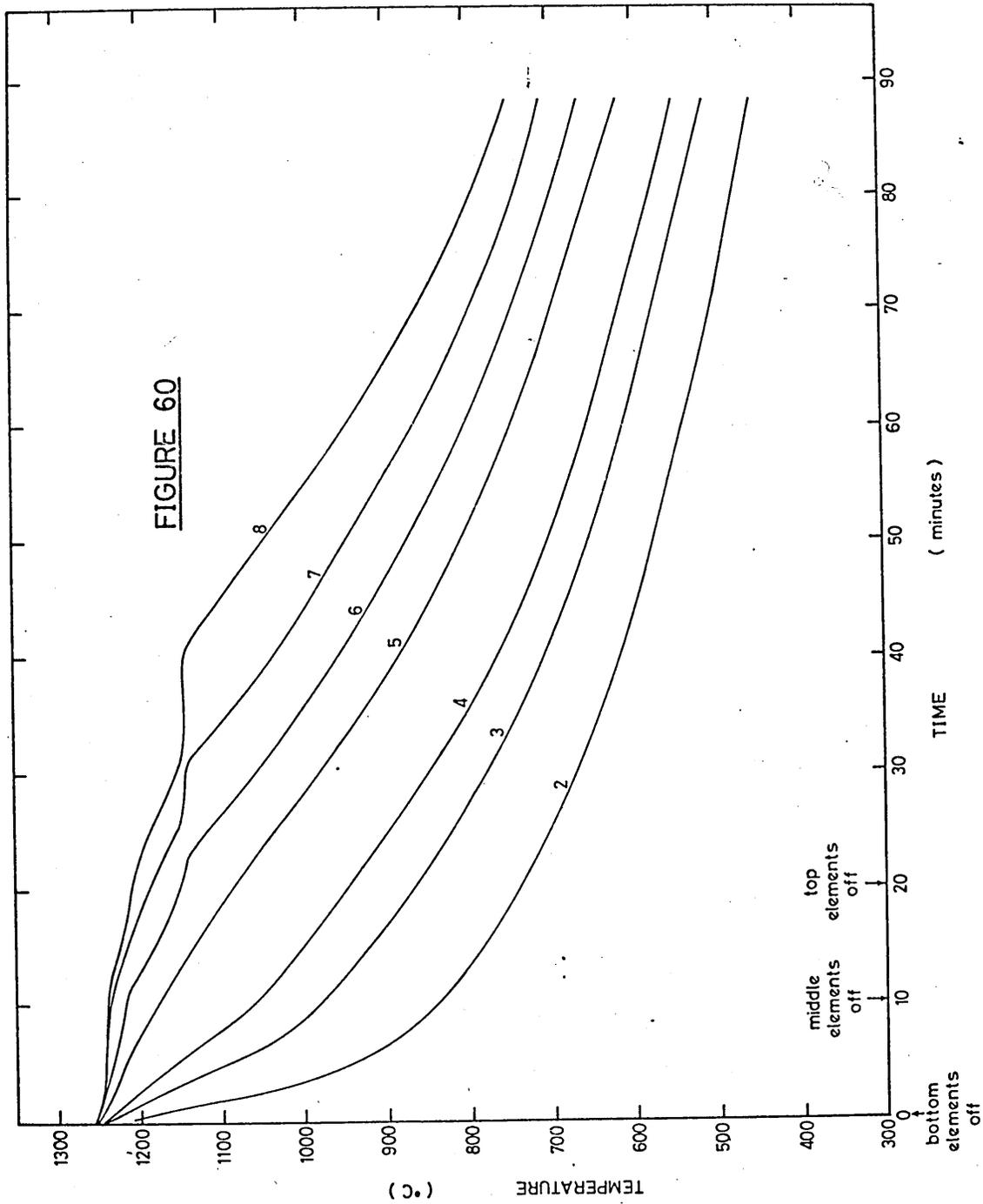
1a	-	-	-	-	-	-	-	-
1b	-	47.35	16.26	10.59	8.50	8.52	7.82	6.97
1c	-	42.93	24.39	17.22	14.12	12.83	11.03	10.09
3a	NO GRAPH							
1a	78.54	26.18	17.50	11.03	8.99	8.19	8.24	6.44
2a	189.41	67.08	20.13	13.76	10.13	9.12	8.05	6.91
1a'	73.8	20.13	12.93	9.79	9.61	8.90	8.05	7.52
3a'	-	42.93	20.00	11.71	9.50	8.50	7.42	6.64
2a'	NO GRAPH							

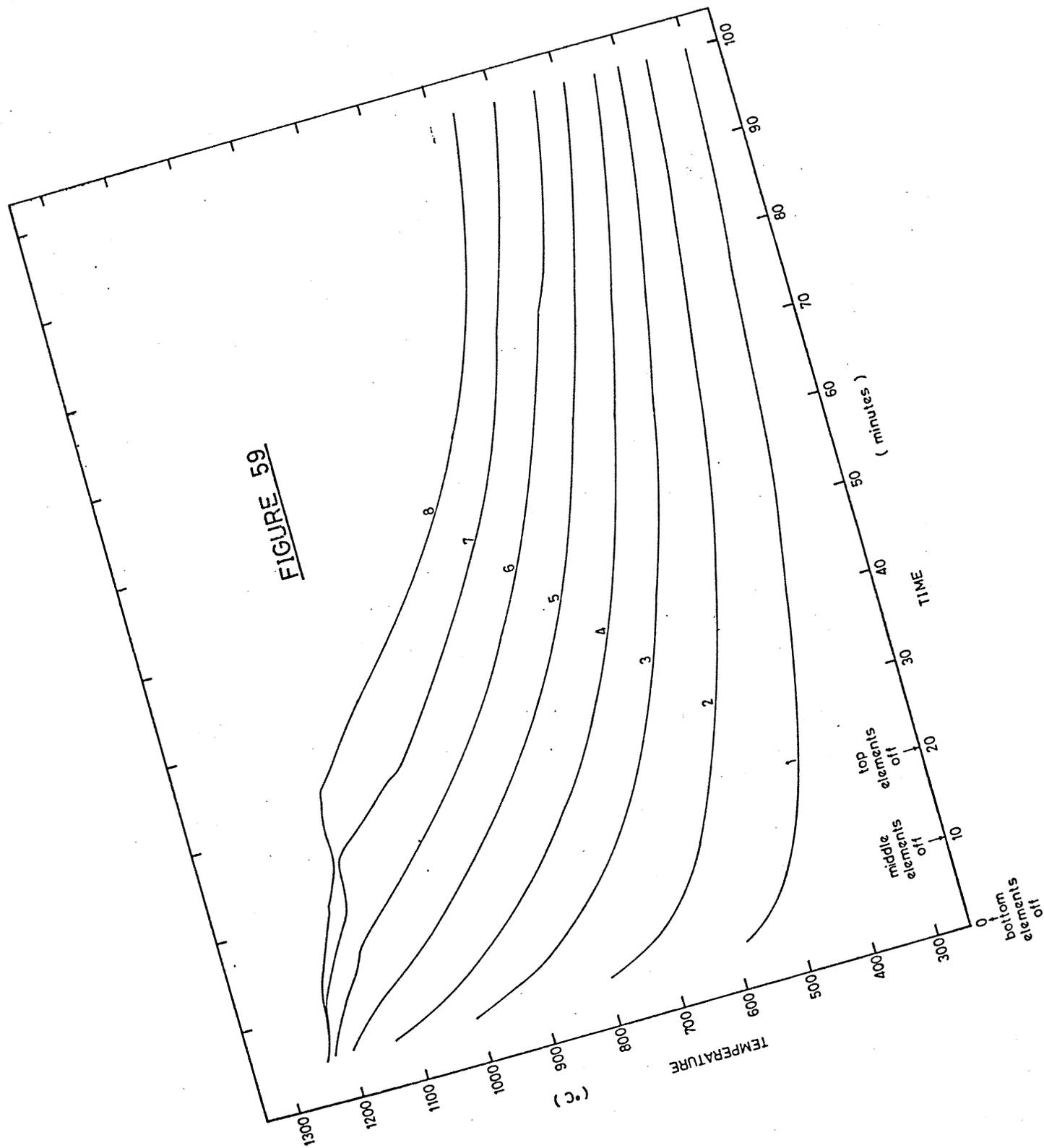
THE COOLING RATE (°C/min) FOR THE 1160-1100°C TEMPERATURE RANGE

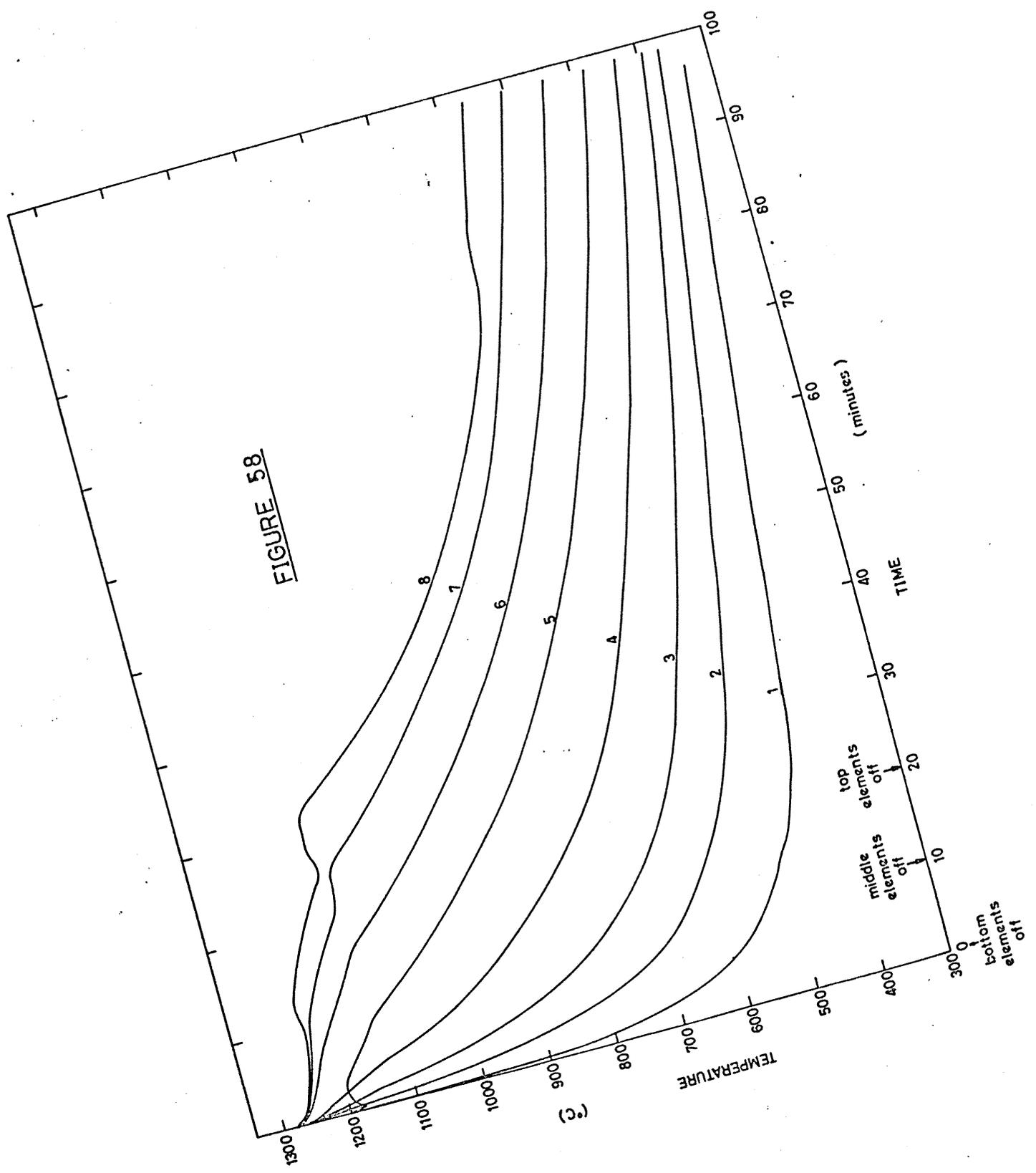
st.	Thermocouple Number							
	1	2	3	4	5	6	7	8
1	≈420	93.33	30	22.95	12.17	10.5	5.75	4.19
	840	105.0	38.18	22.22	12.8	8.57	5.86	3.96
3	-	168.0	46.67	23.6	15.7	-	5.92	5.25
1	-	-	≈60	26.25	11.67	8.94	6.32	4.77
2	1400	120.0	38.18	27.1	14.48	9.66	6.56	4.31
3	420	105	35	30	13.13	9.13	9.33	4.33
1	525	76.36	49.41	28	15.85	10.5	6.89	4.40
2	840	140	54.62	35	-	10.5	6.0	4.0
3	600	168	70	28.97	13.77	12.73	6.18	6.67
1	≈420	150	44.68	-	10.24	8.62	6.30	4.97
2	-	-	60	40	13.77	9.13	6.51	4.57
3	210	140	56	30	10.63	10.63	6.22	4.67
1	≈525	93.3	42	30	12.54	9.77	6.27	4.18
2	420	120	-	28	13.55	10.5	6.36	4.52
3	420	60	30	28	12.35	9.55	7.0	4.2
1	-	120	36.52	27.1	14.0	9.77	6.46	4.33
2	-	210	52.50	24.71	10.37	8.94	5.81	4.23
3	323	89.36	28.97	27.70	-	7.57	4.86	3.65
1'	840	84	56	24.71	12.35	7.18	5.68	3.89
2'	525	140	36.52	21	12.35	13.13	6.56	3.98
3'	≈420	168	31.11	26.25	11.67	8.57	6.18	4.31
1'	280	120	42	19.09	12.35	10.00	6.56	4.77
2'	-	-	-	-	-	-	-	-
3'	420	87.5	42.00	16.80	12.73	9.23	6.41	4.00
1'	-	76.36	49.41	22.70	11.35	-	-	4.33
2'	350	70	52.50	25.45	12.73	9.13	6.09	3.75
3'	-	-	52.50	28.97	9.55	8.66	6.56	4.35
1'	-	-	-	33.6	16.80	10.77	6.18	4.24
3'	-	70	33.60	20.49	11.35	7.18	5.75	3.75
1'	420	76.36	-	-	-	10.37	5.32	4.24
2'	420	120	-	28.00	13.55	10.50	6.36	4.52
3'	840	140	76.36	35.00	13.13	11.35	7.00	5.53

ADDITIONAL CASTS

1a	-	-	-	-	-	-	-	-
1b	-	175	56	26.25	8.7	10.19	6.77	4.52
1c	300	100	44.21	15.11	17.14	9.27	5.32	-
1a	420	84	70.0	76.25	13.13	8.84	10.91	4.04
2a	-	≈280	52.5	32.31	14.0	10.0	6.18	4.26
3a	-	NO GRAPH	-	-	-	-	-	-
a'	420	76.36	40.0	16.15	11.20	8.24	5.68	4.16
a'	-	168	70.0	24.0	16.8	10.24	6.27	7.64
a'	-	NO GRAPH	-	-	-	-	-	-







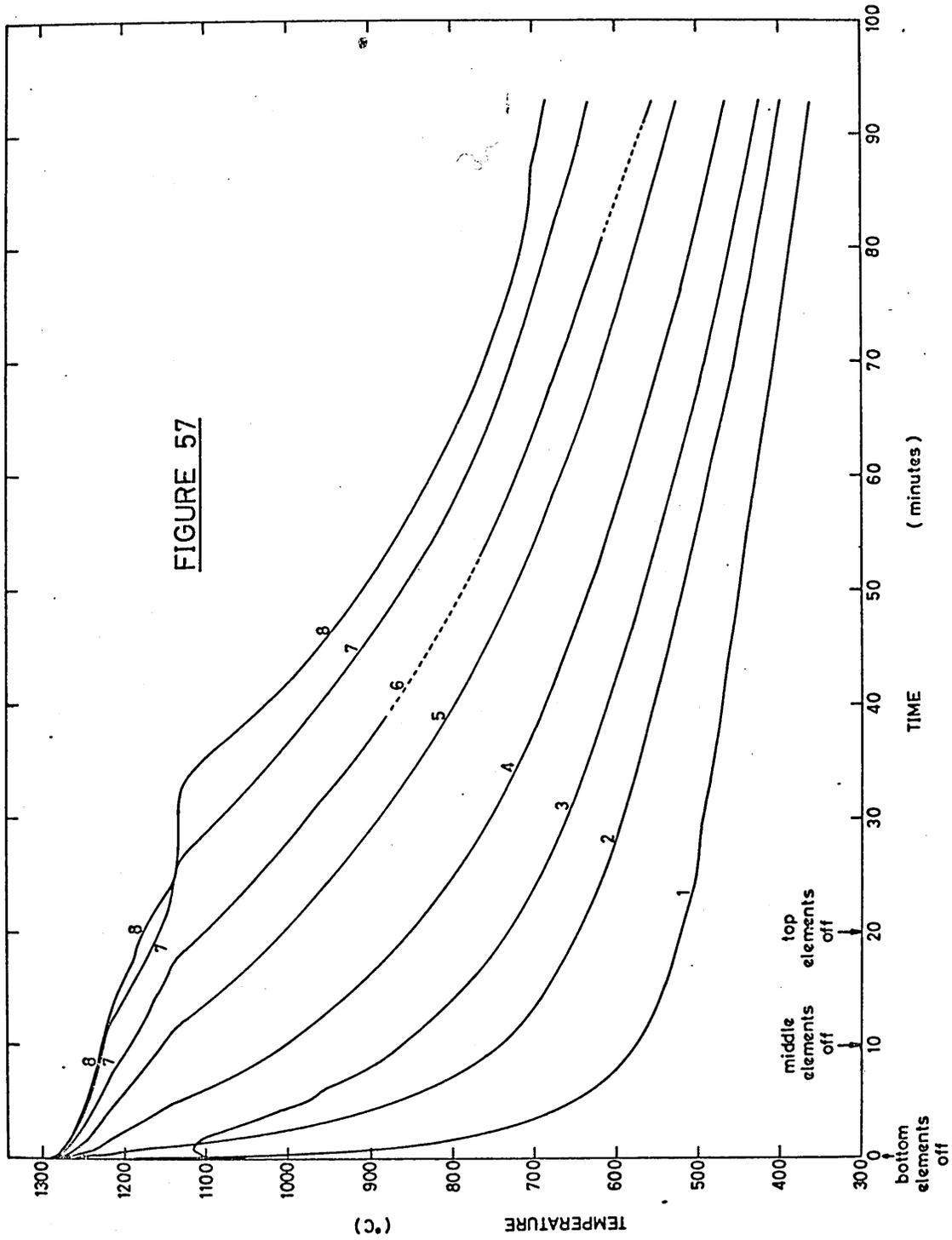
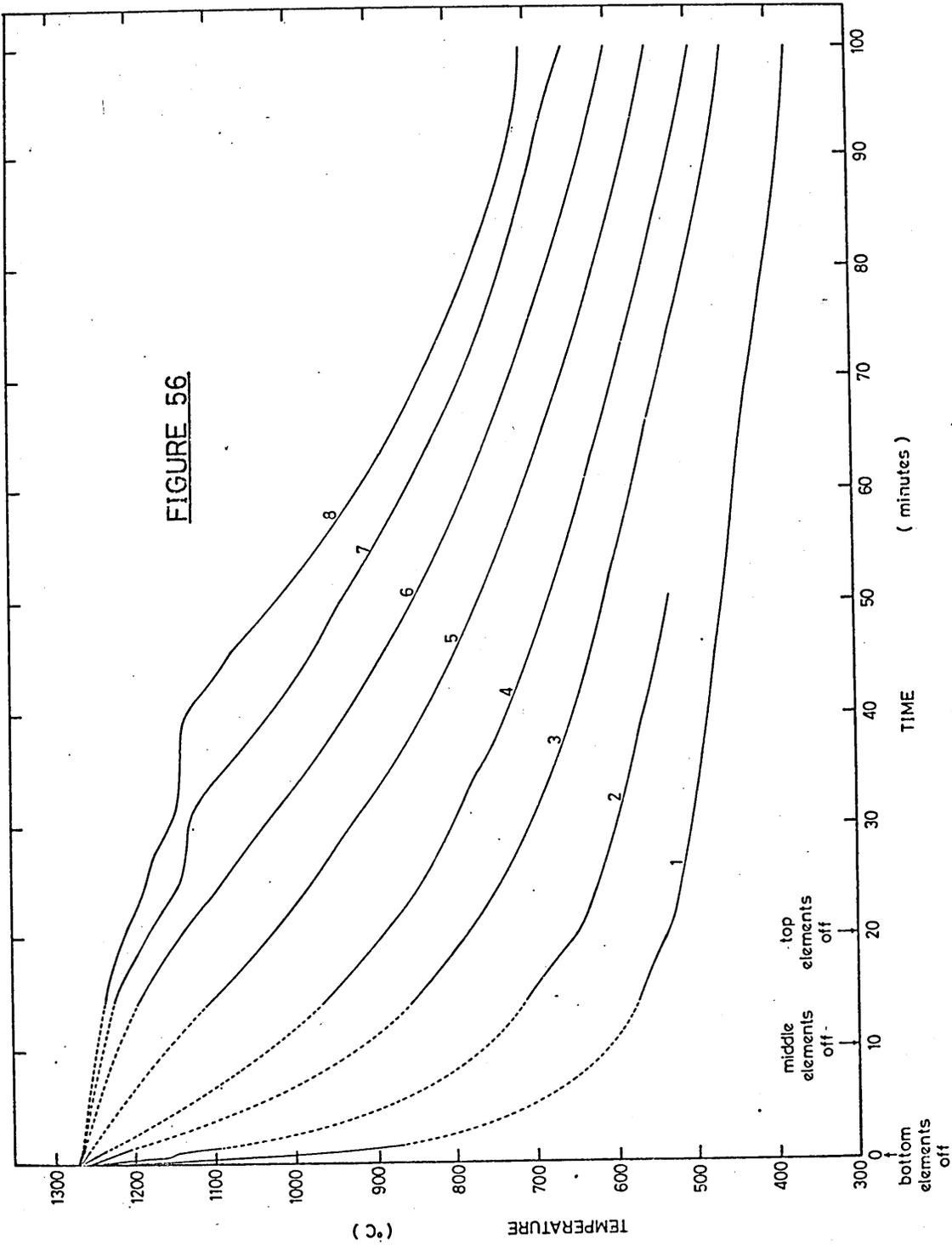
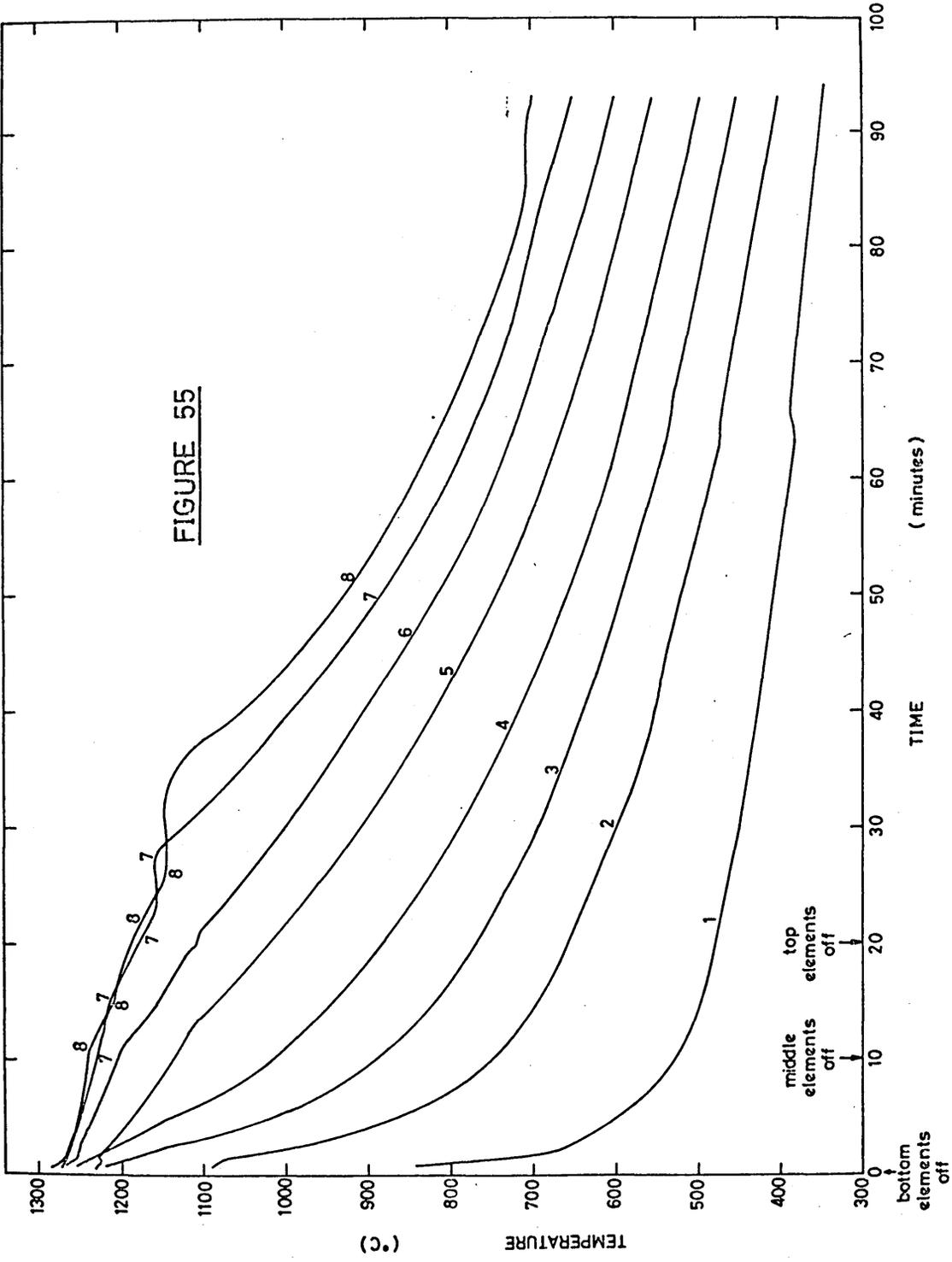
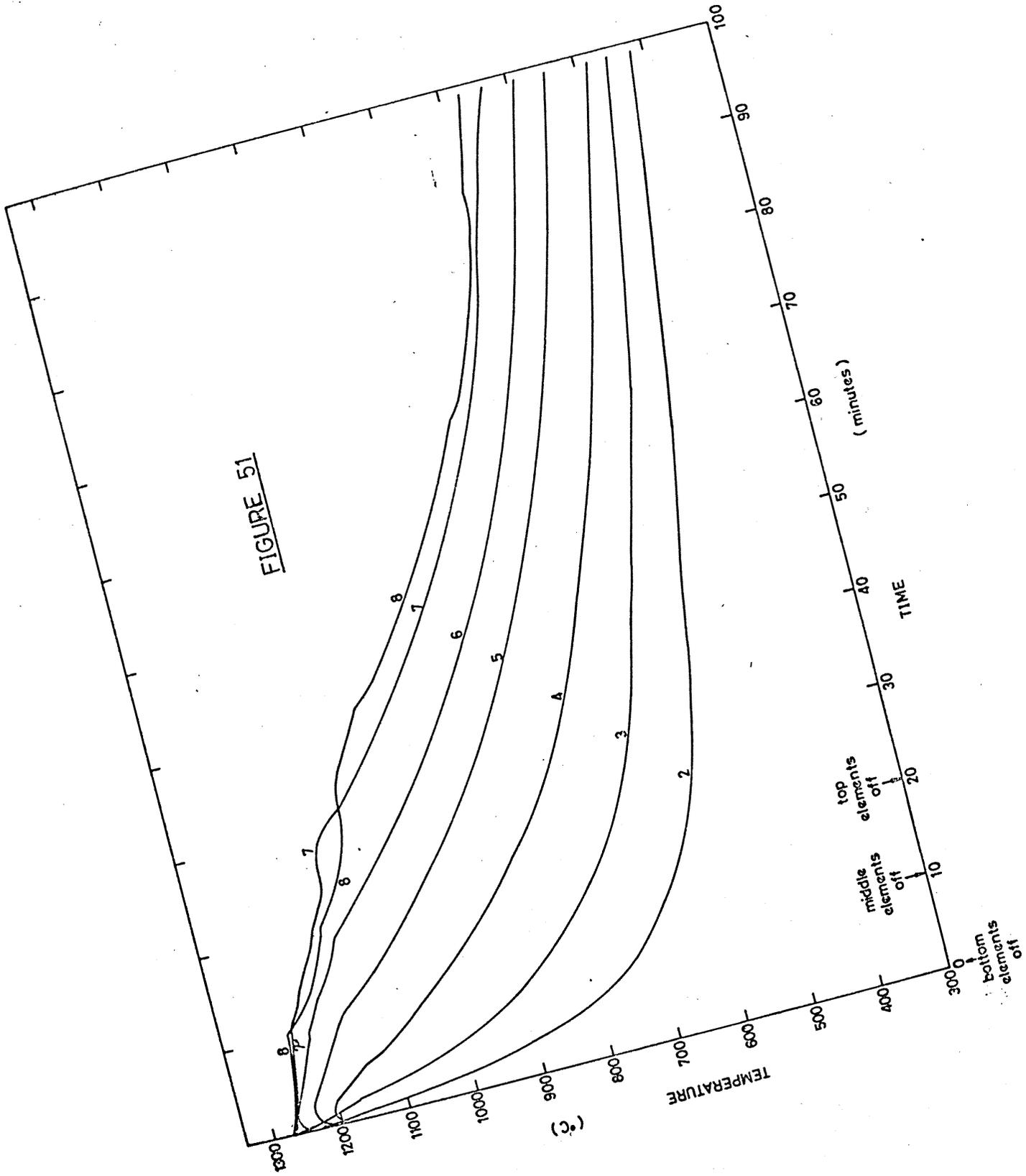
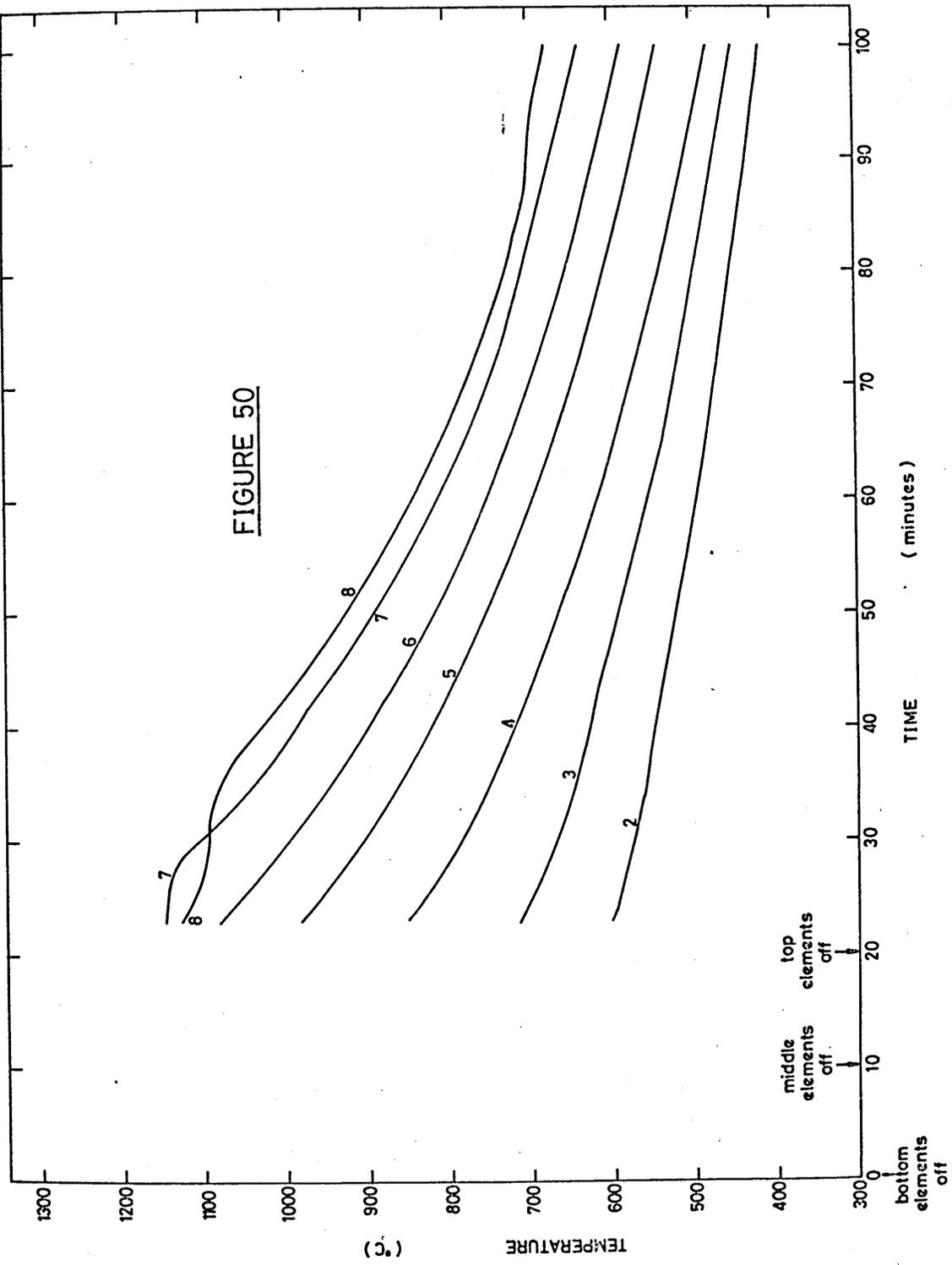


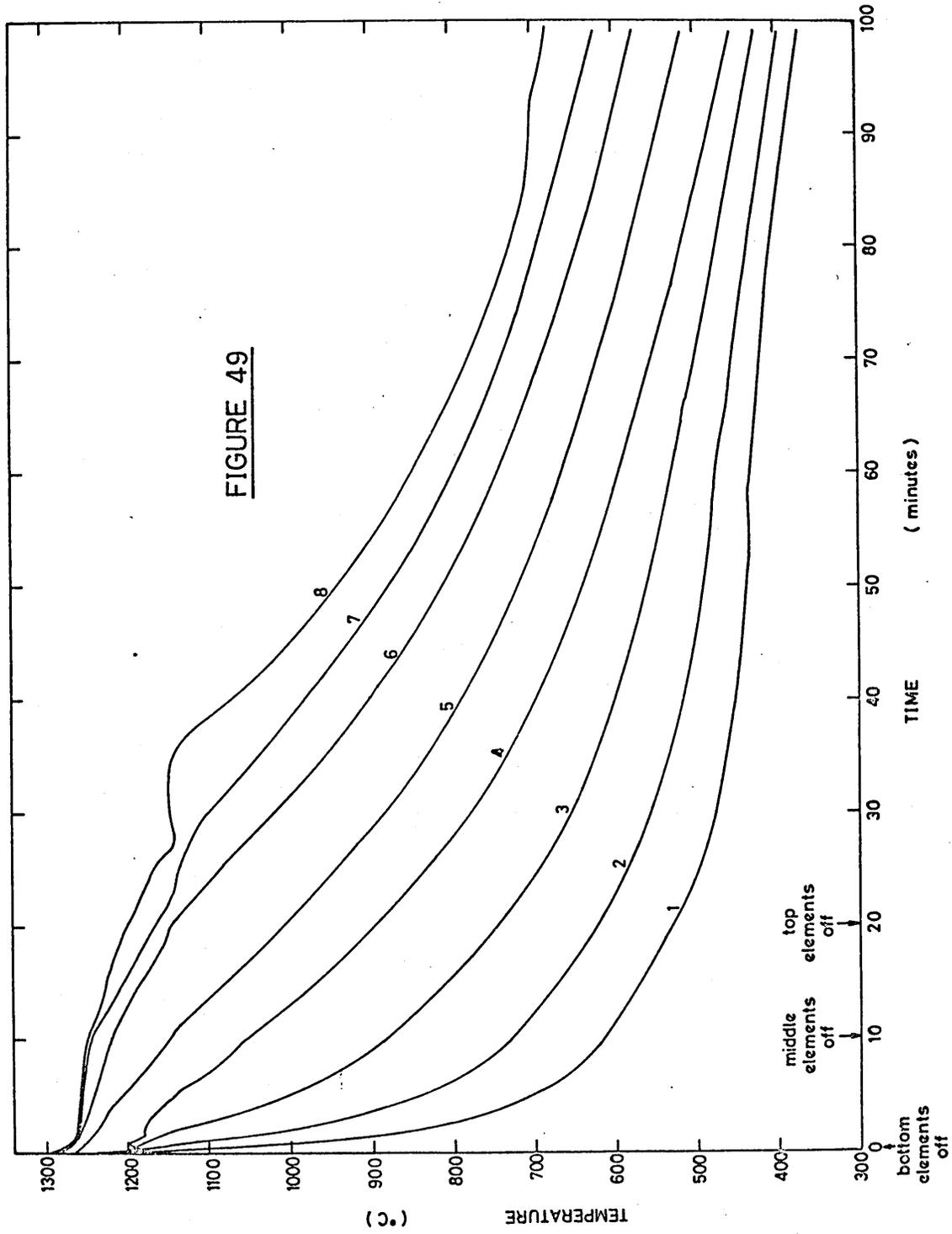
FIGURE 56

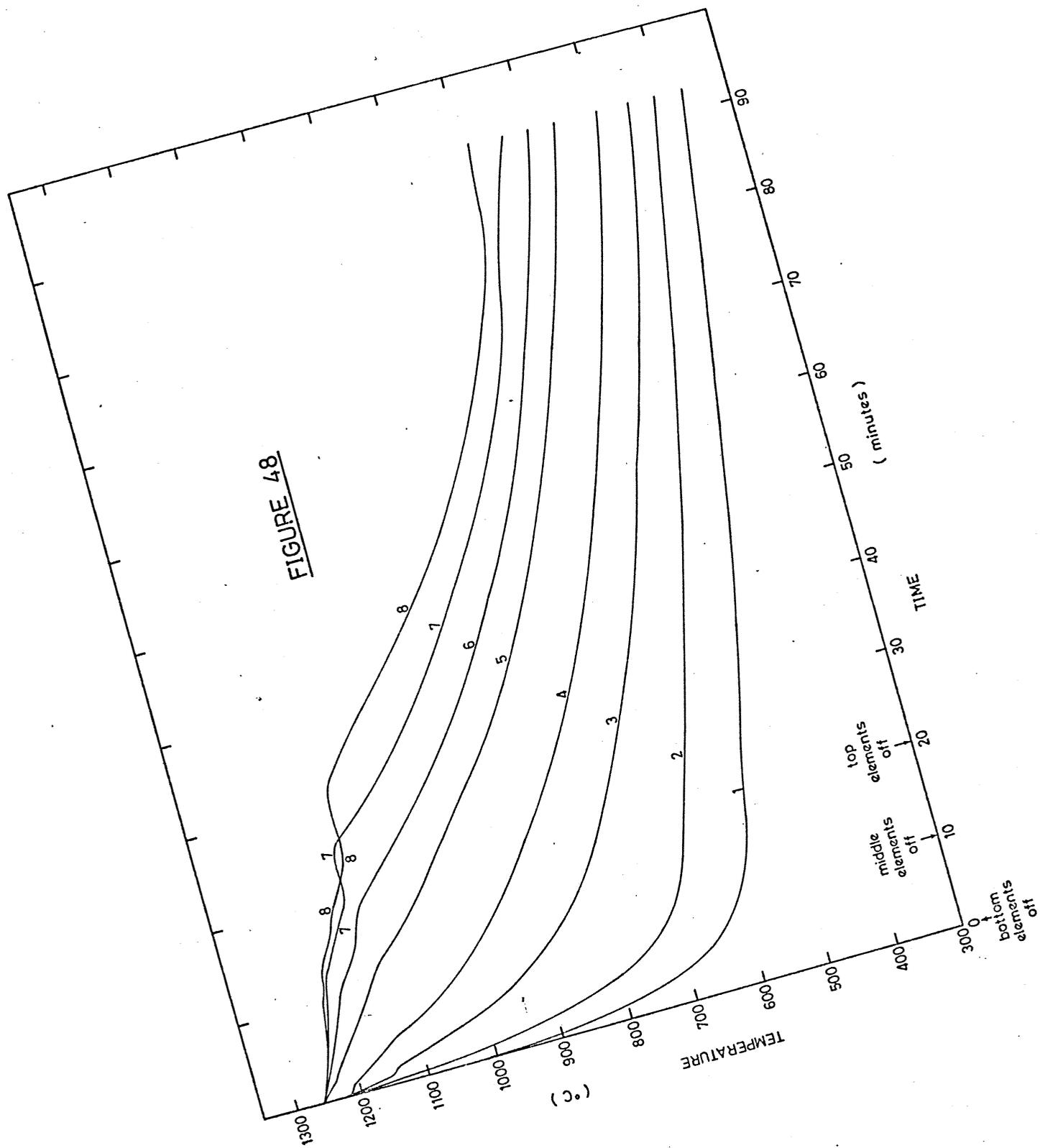


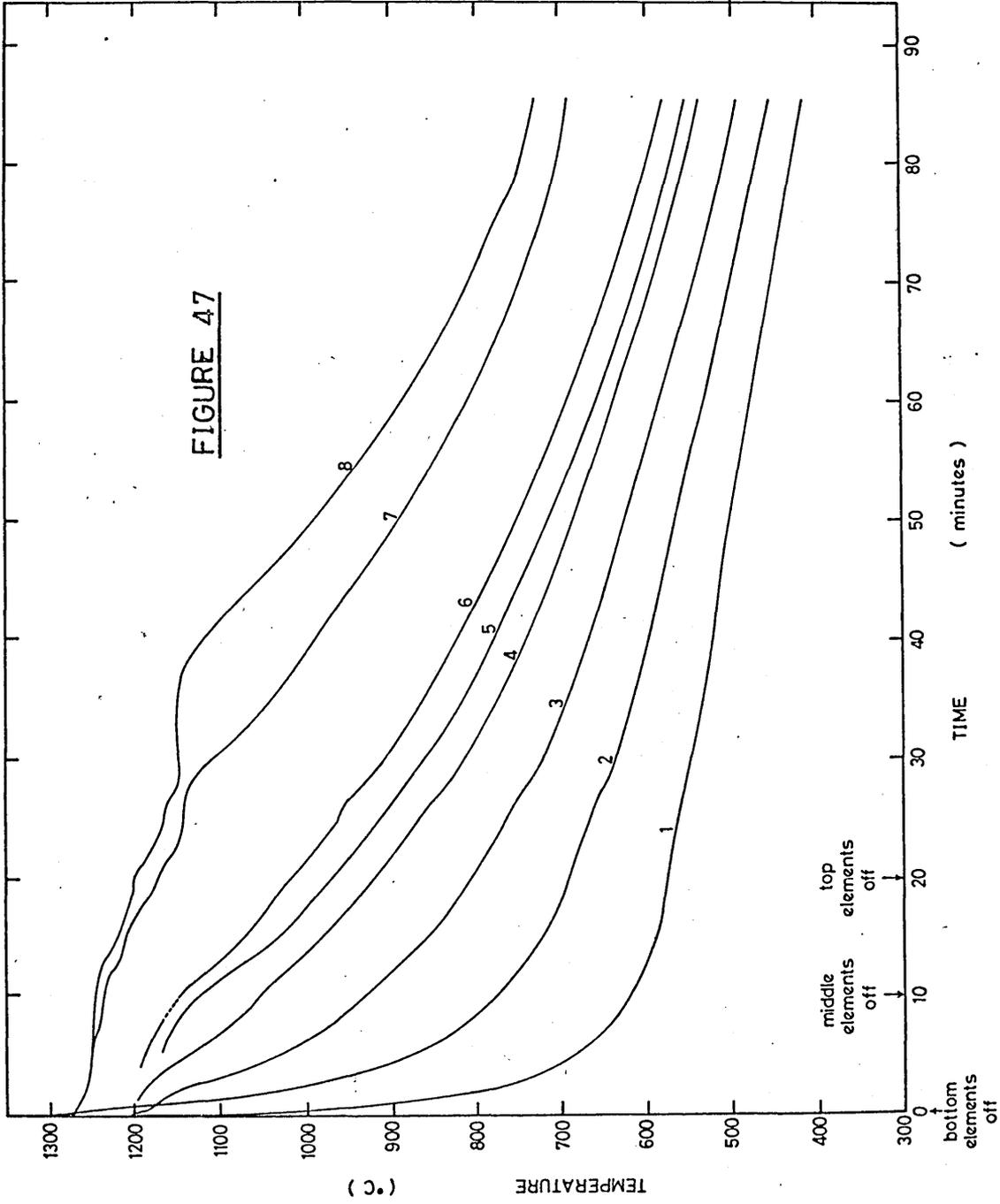


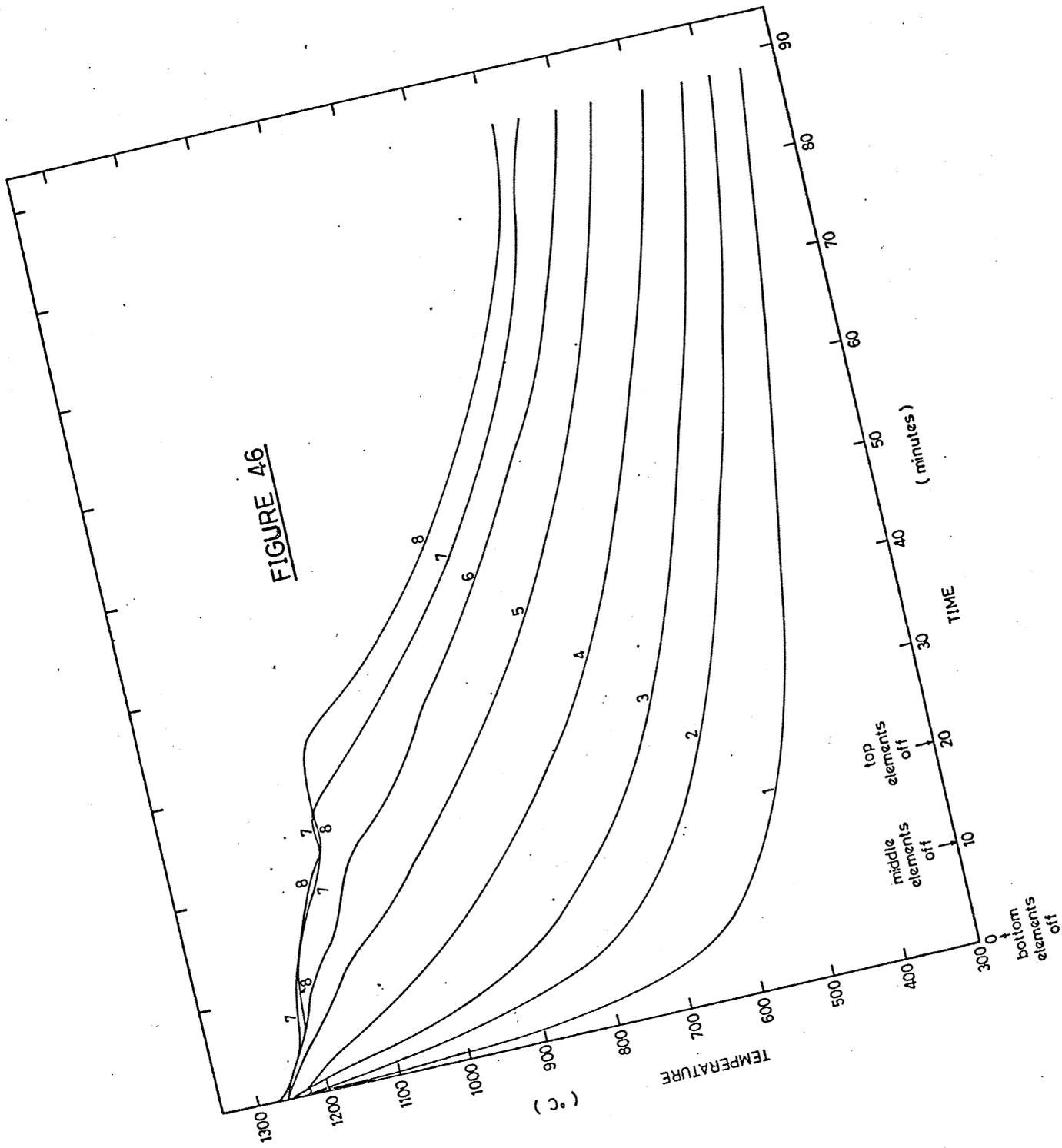


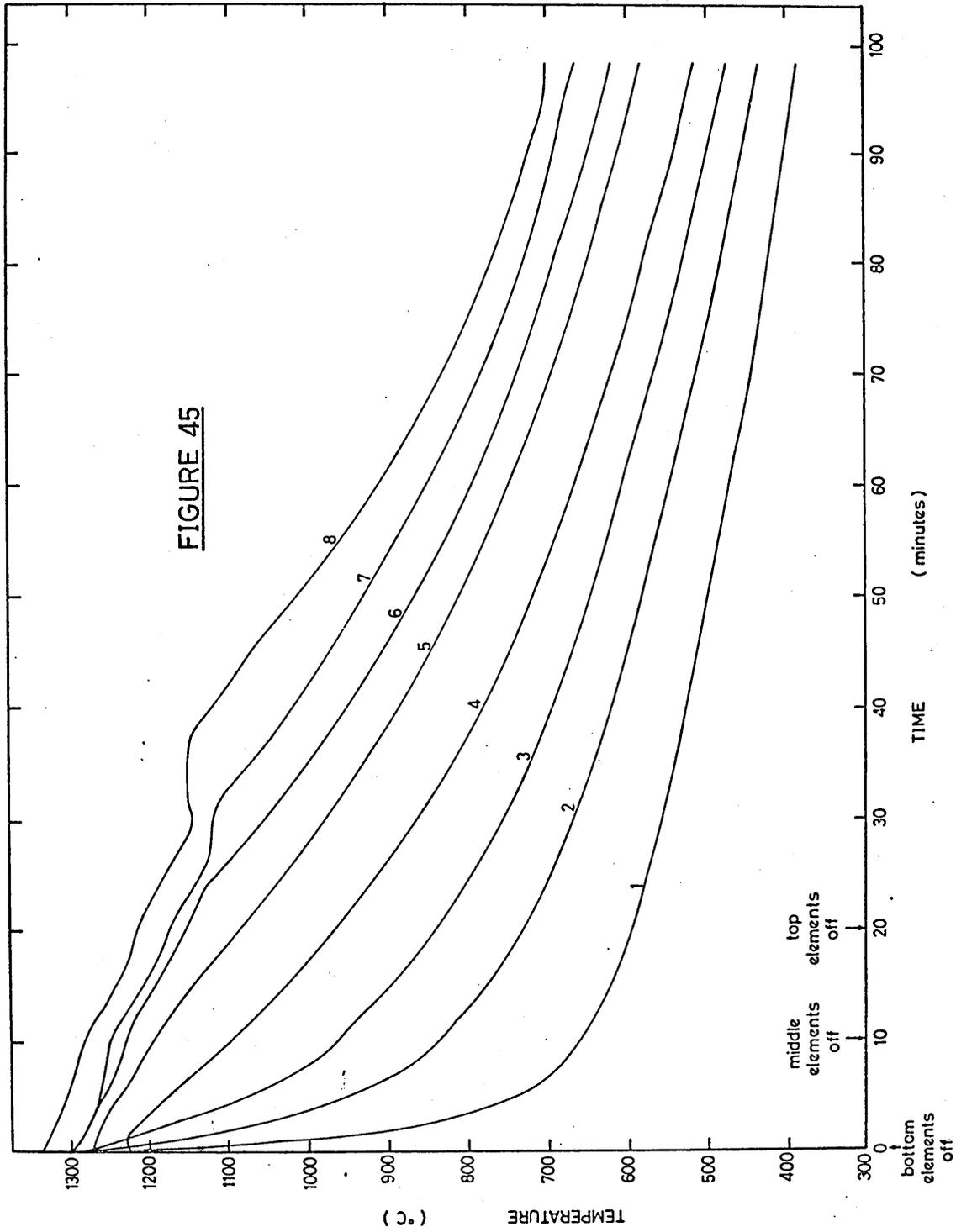


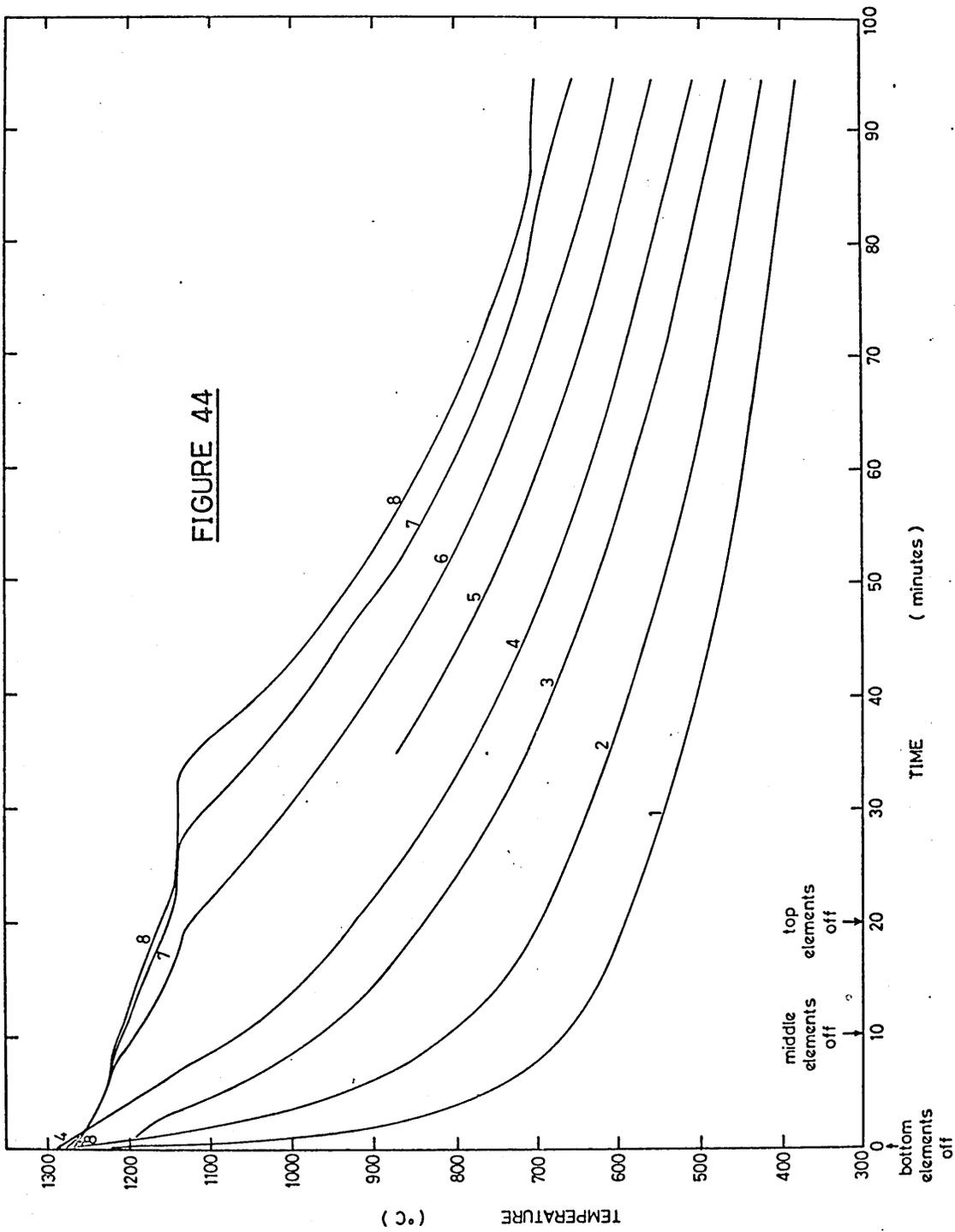


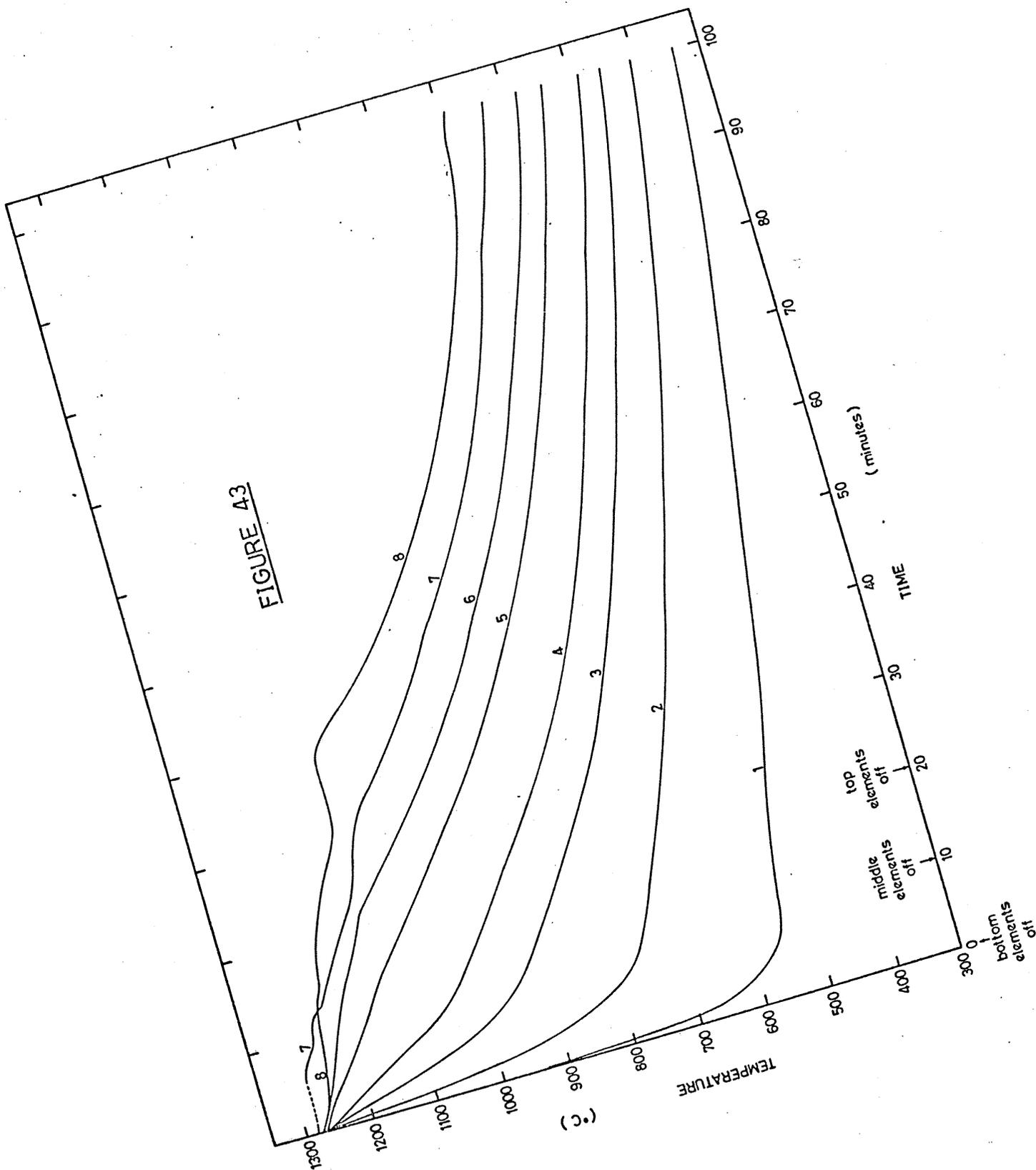


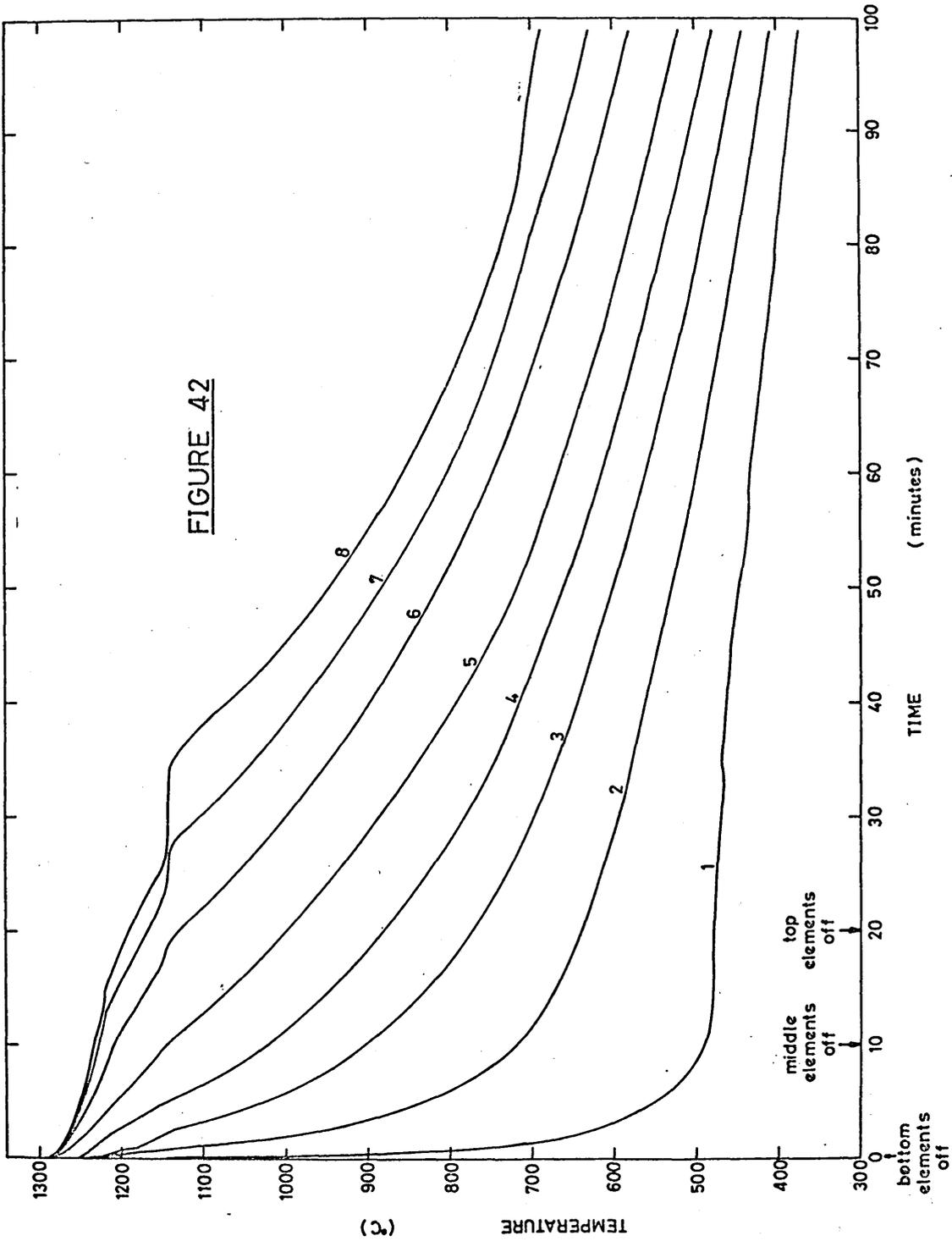












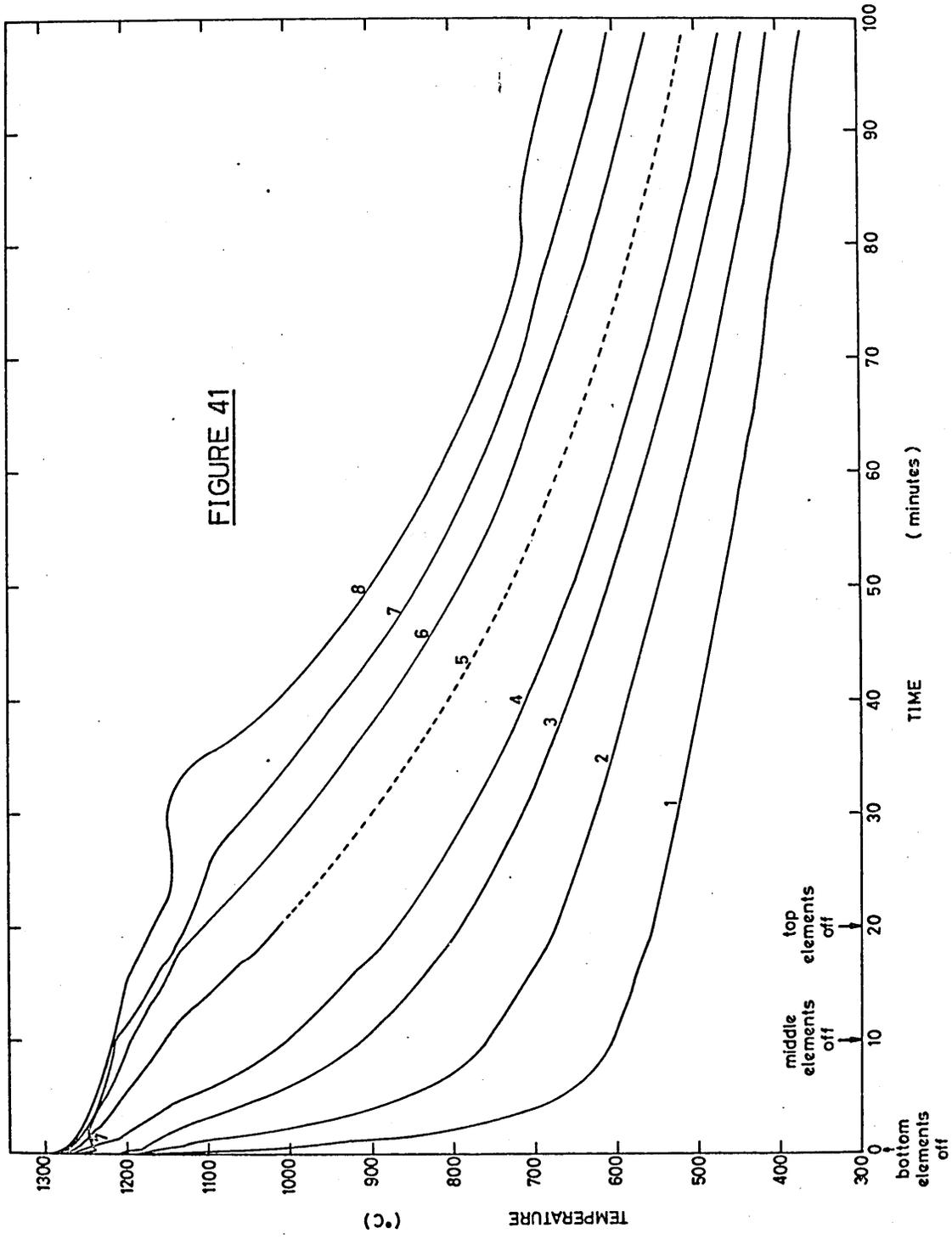


FIGURE 41

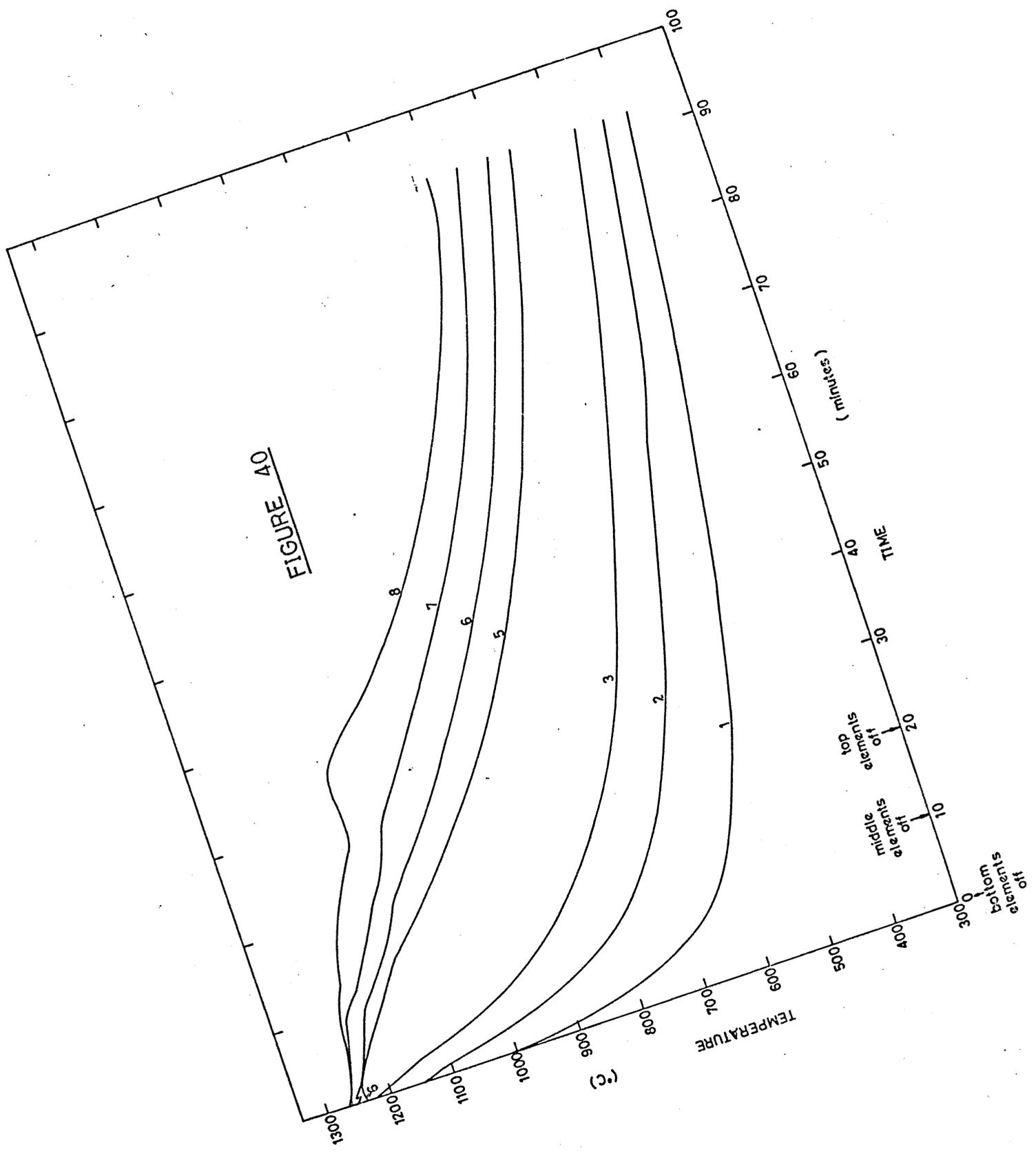
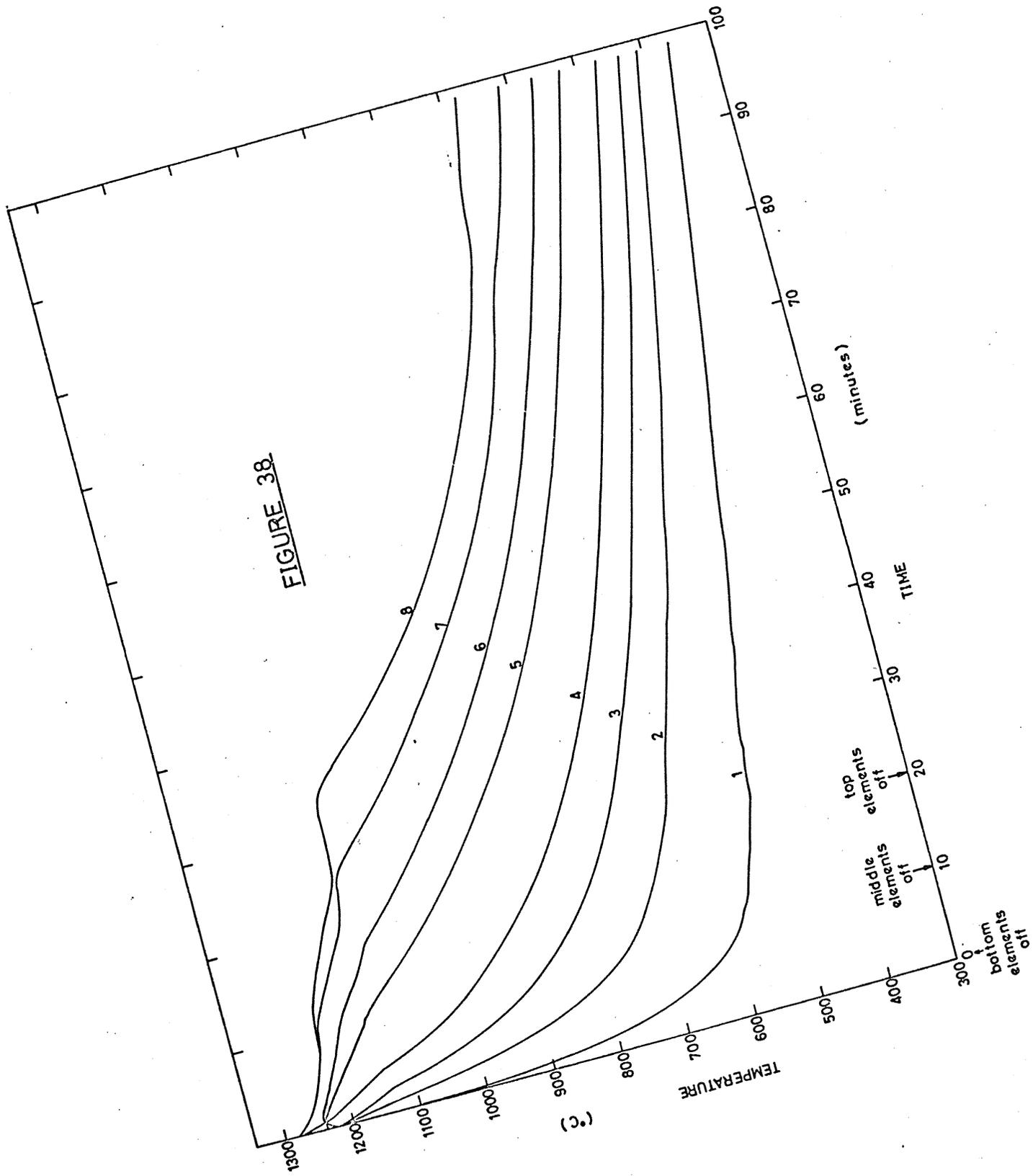
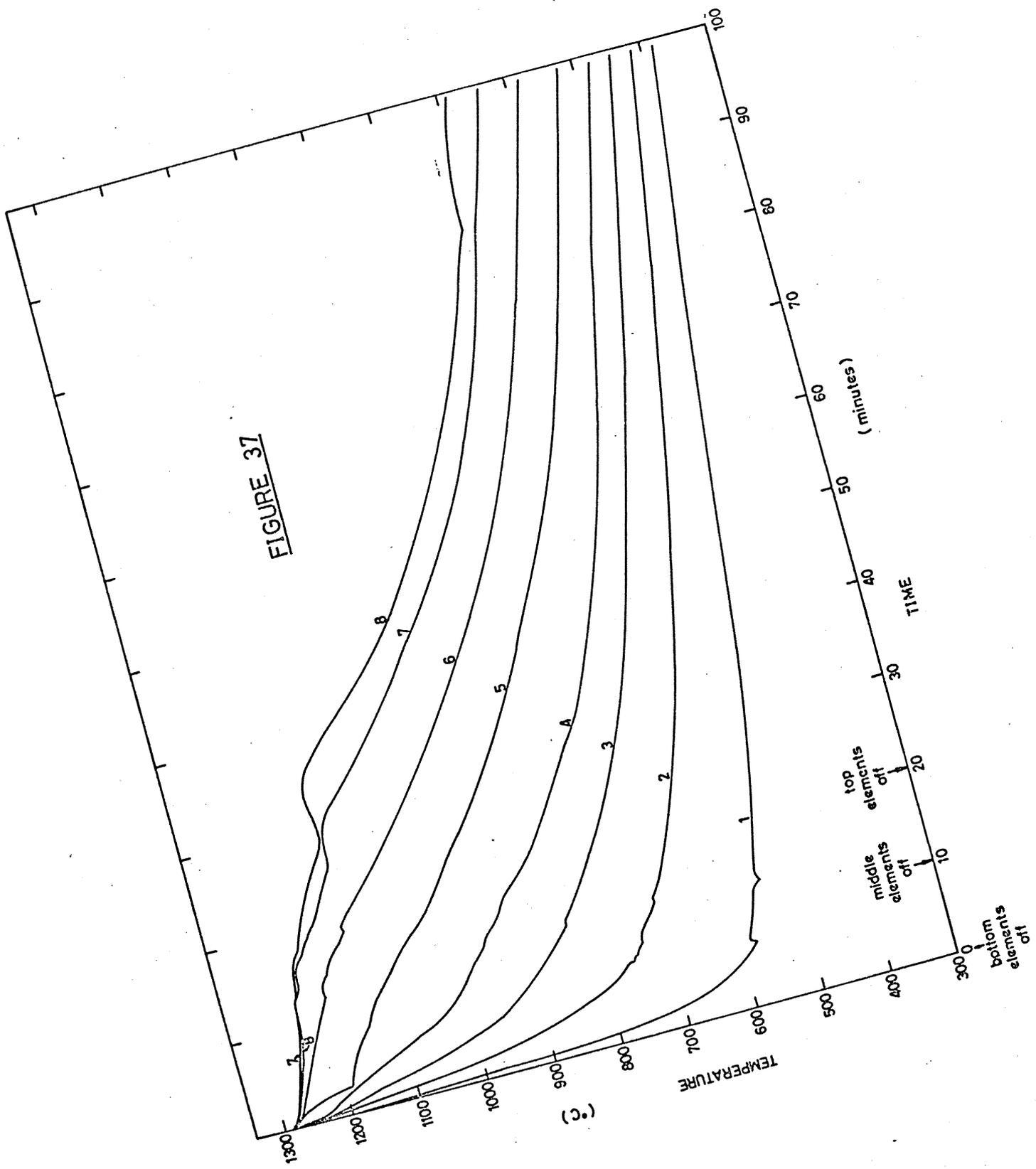
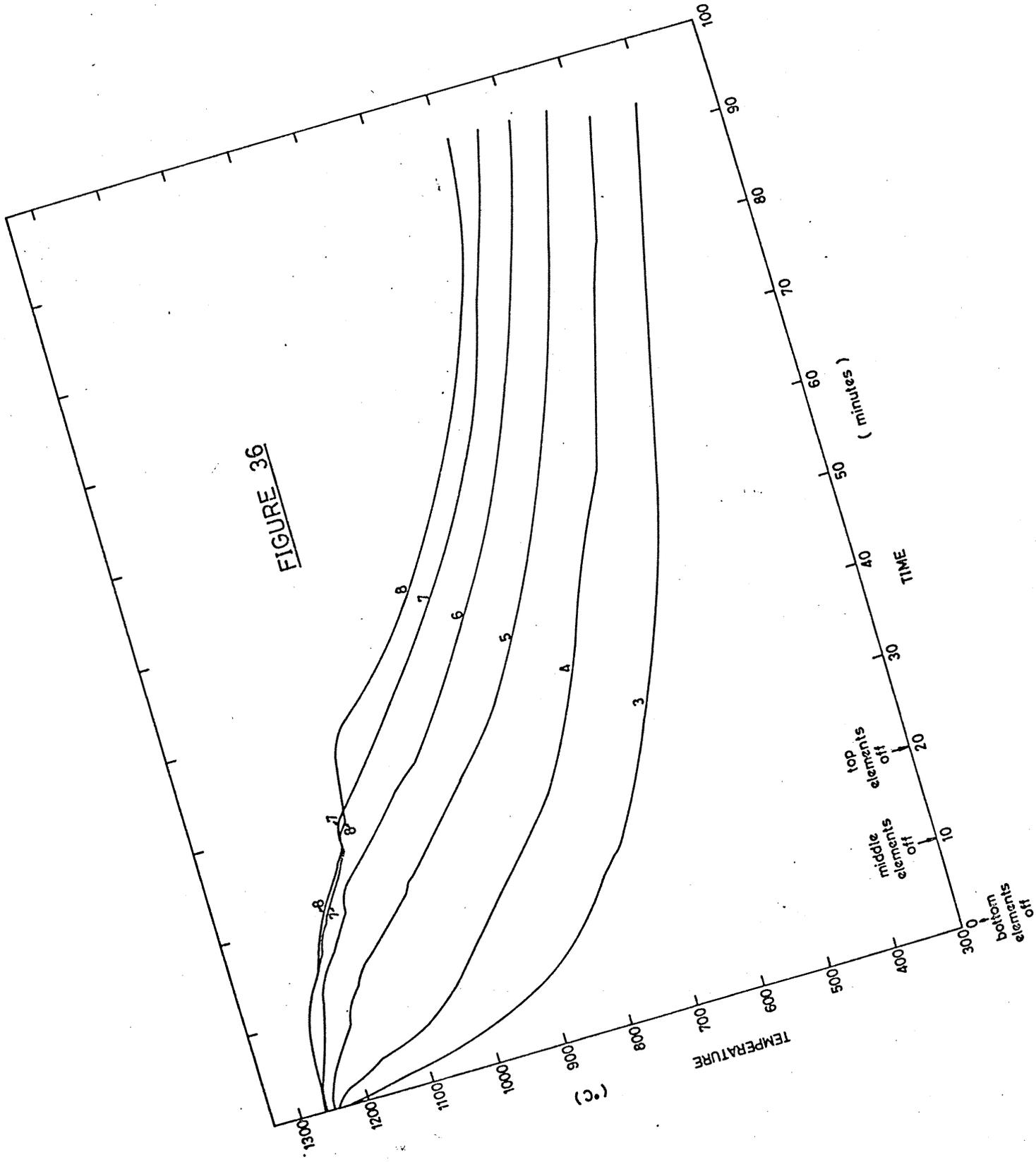
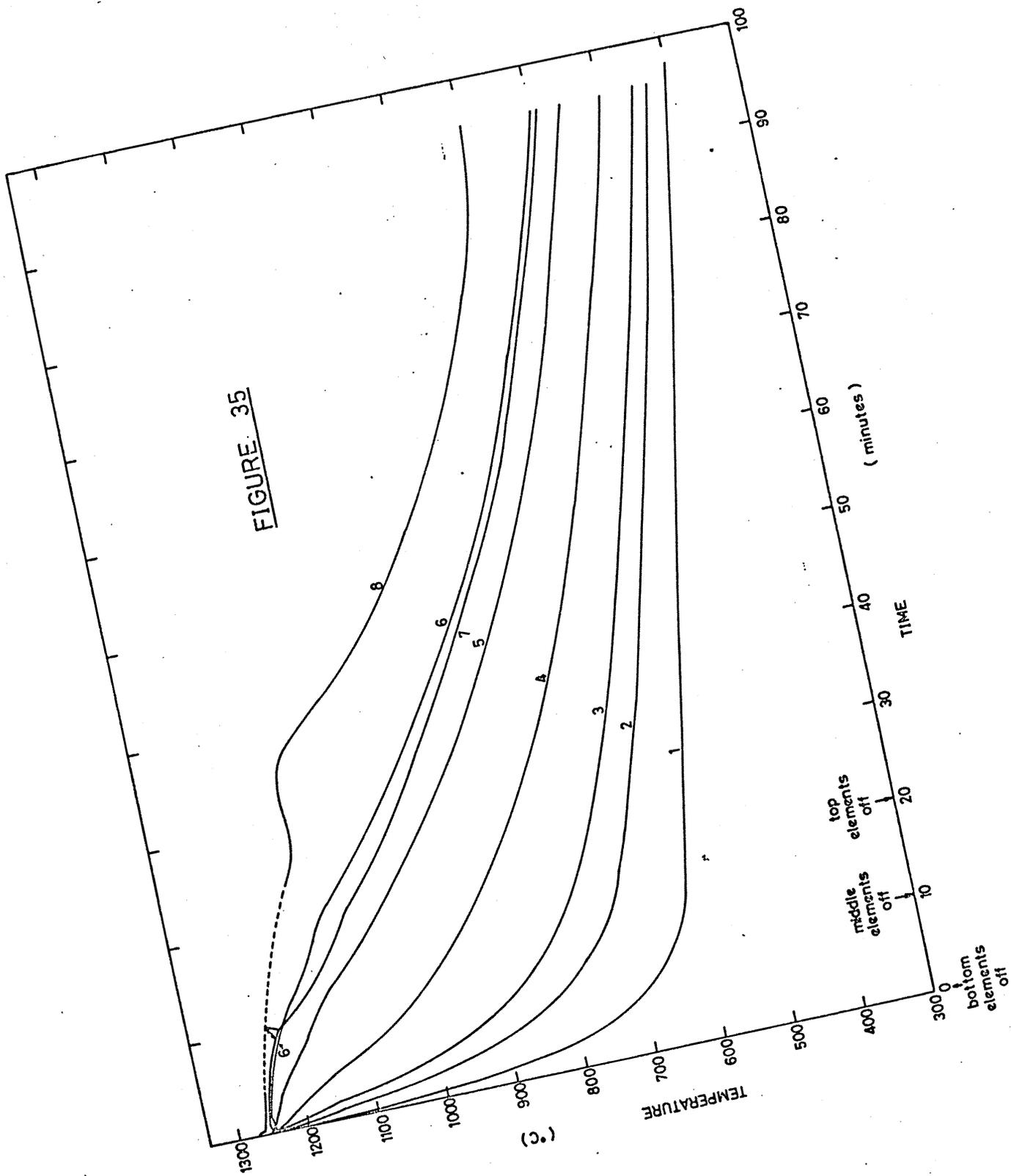


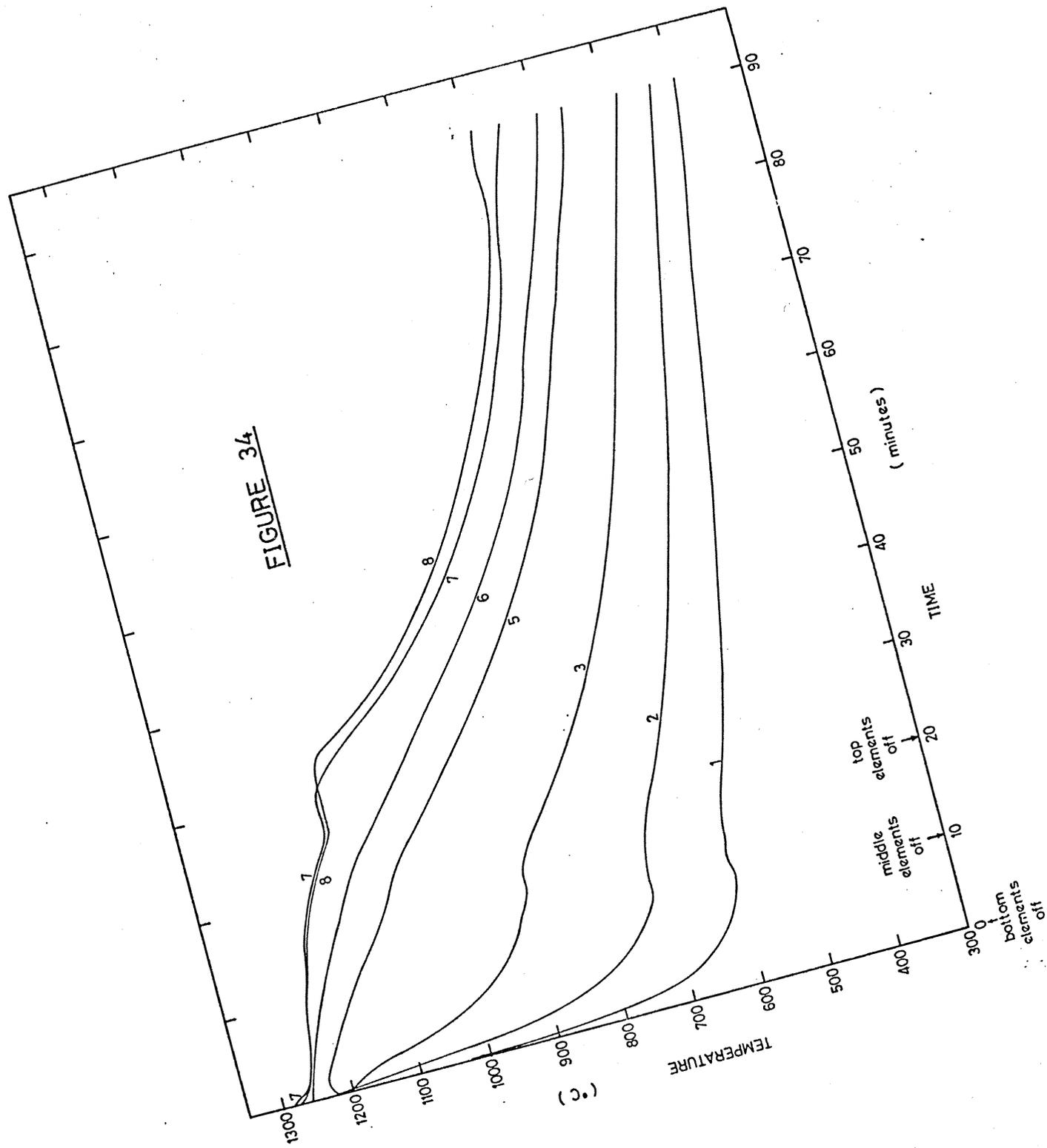
FIGURE 40

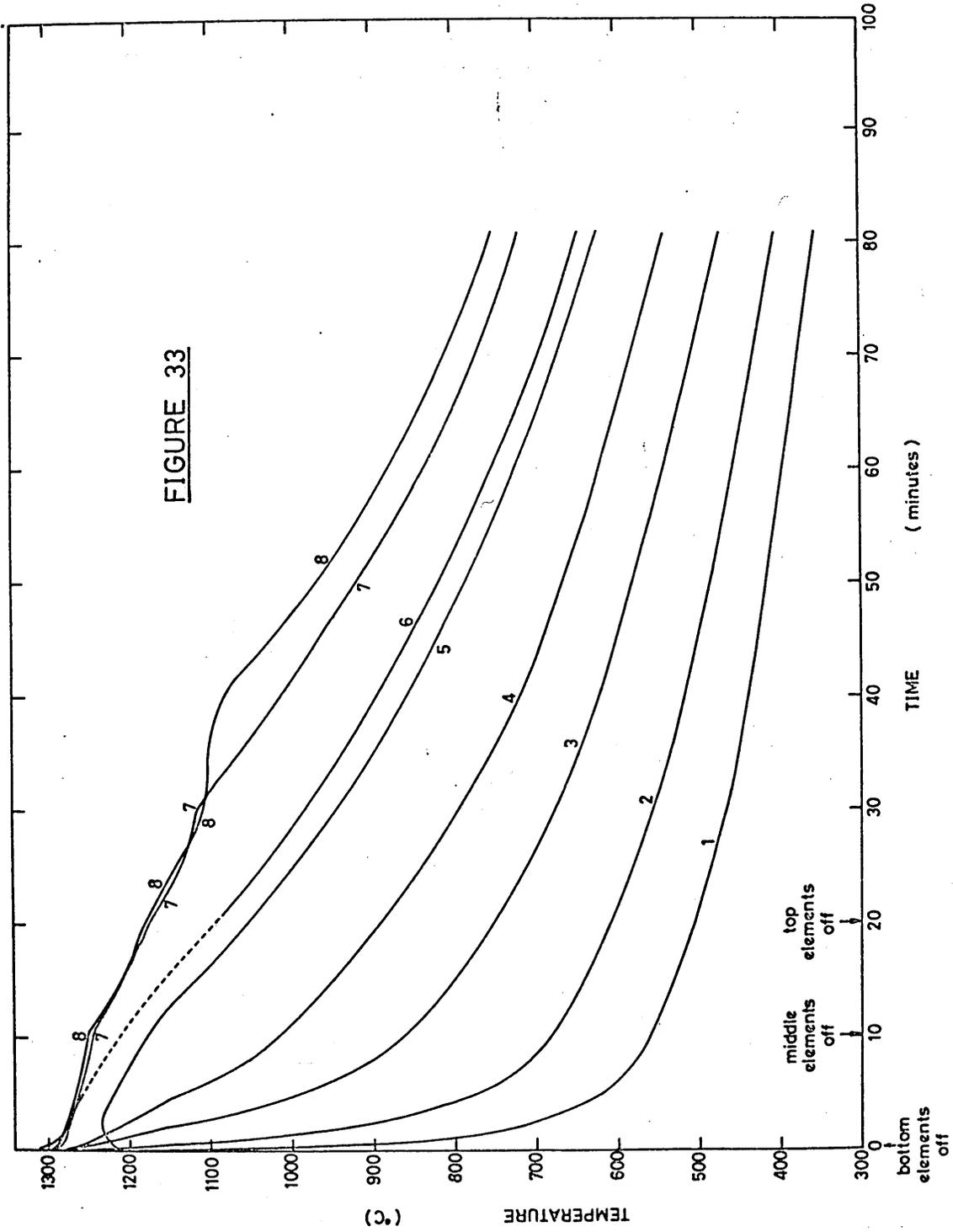


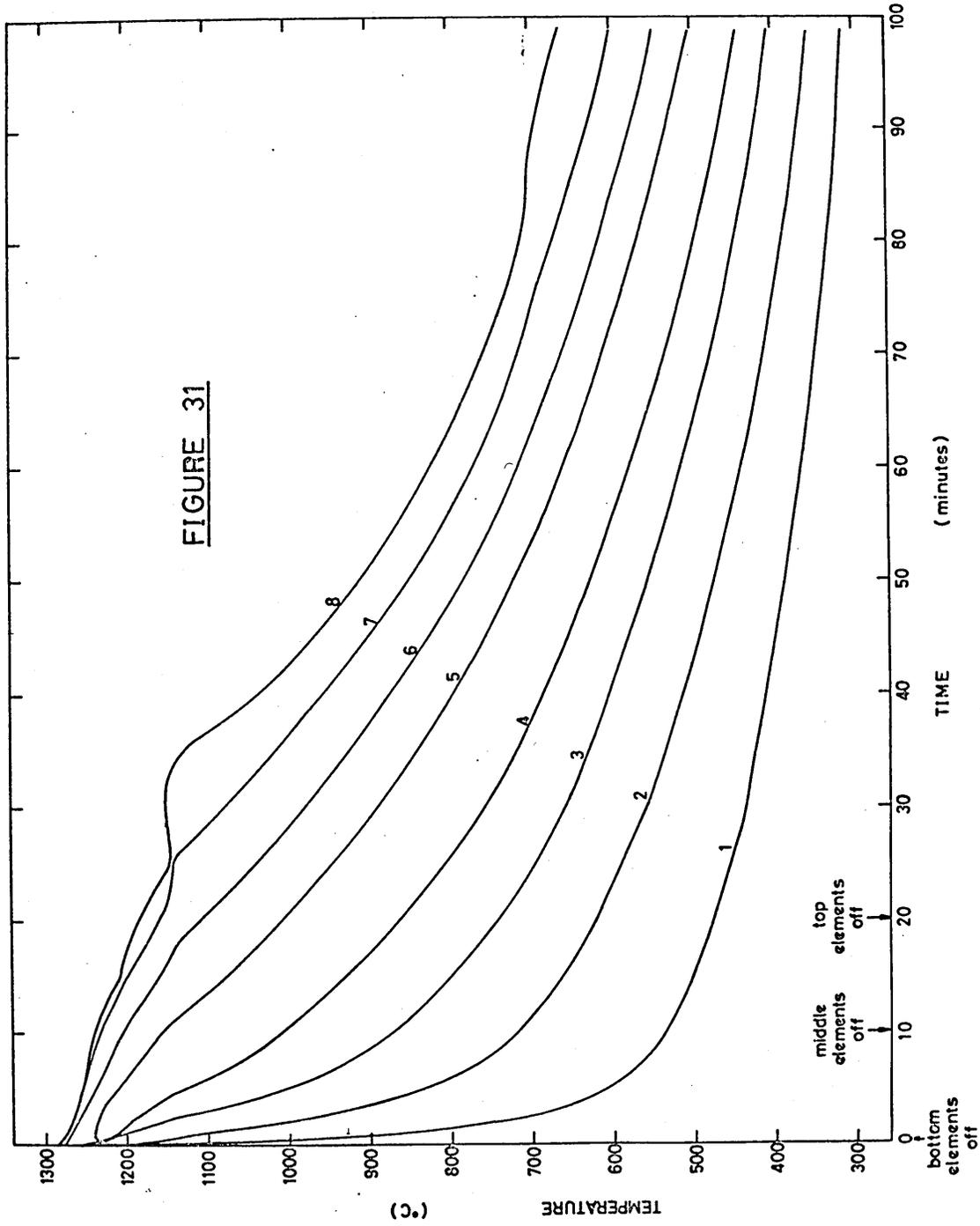


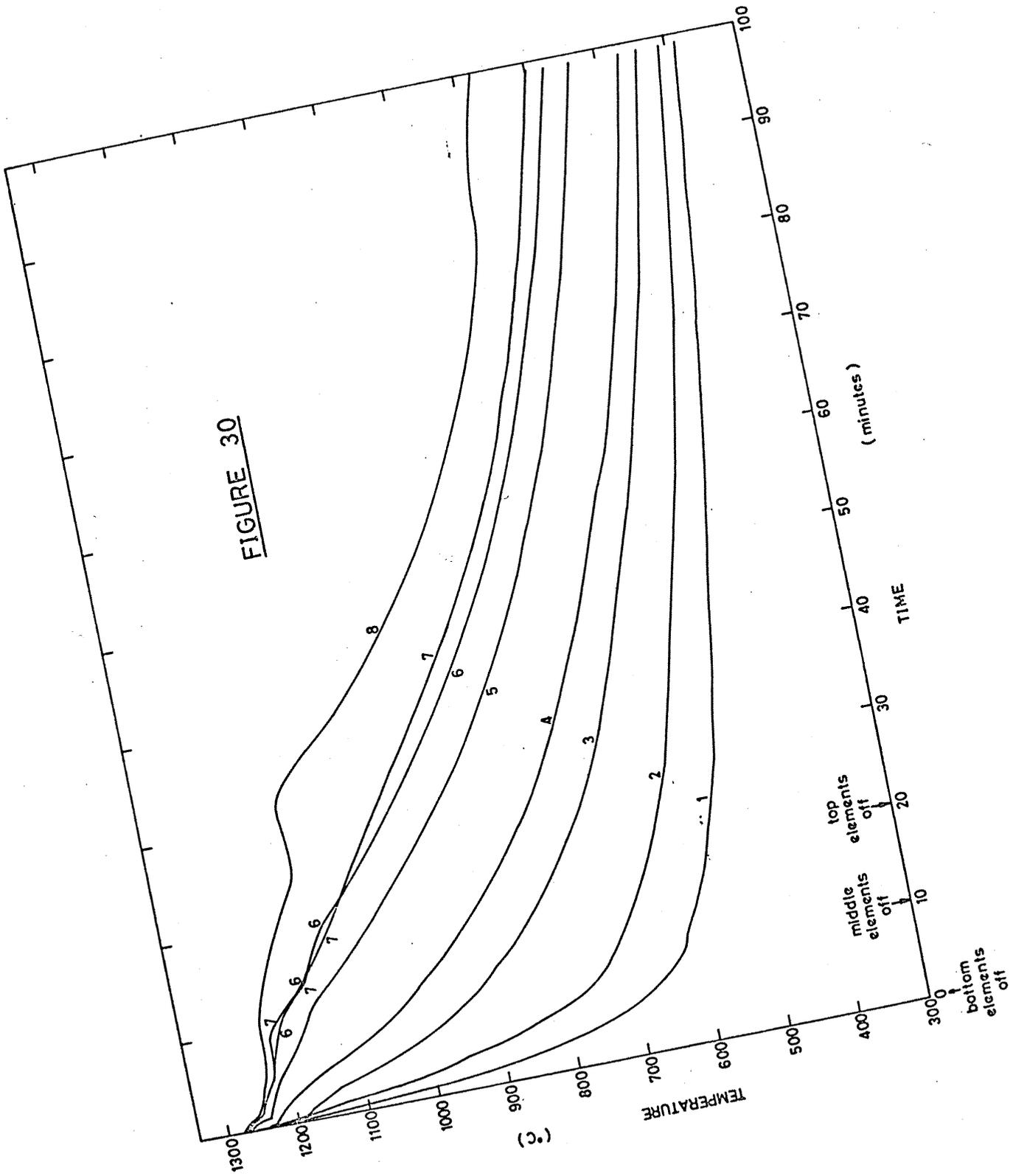


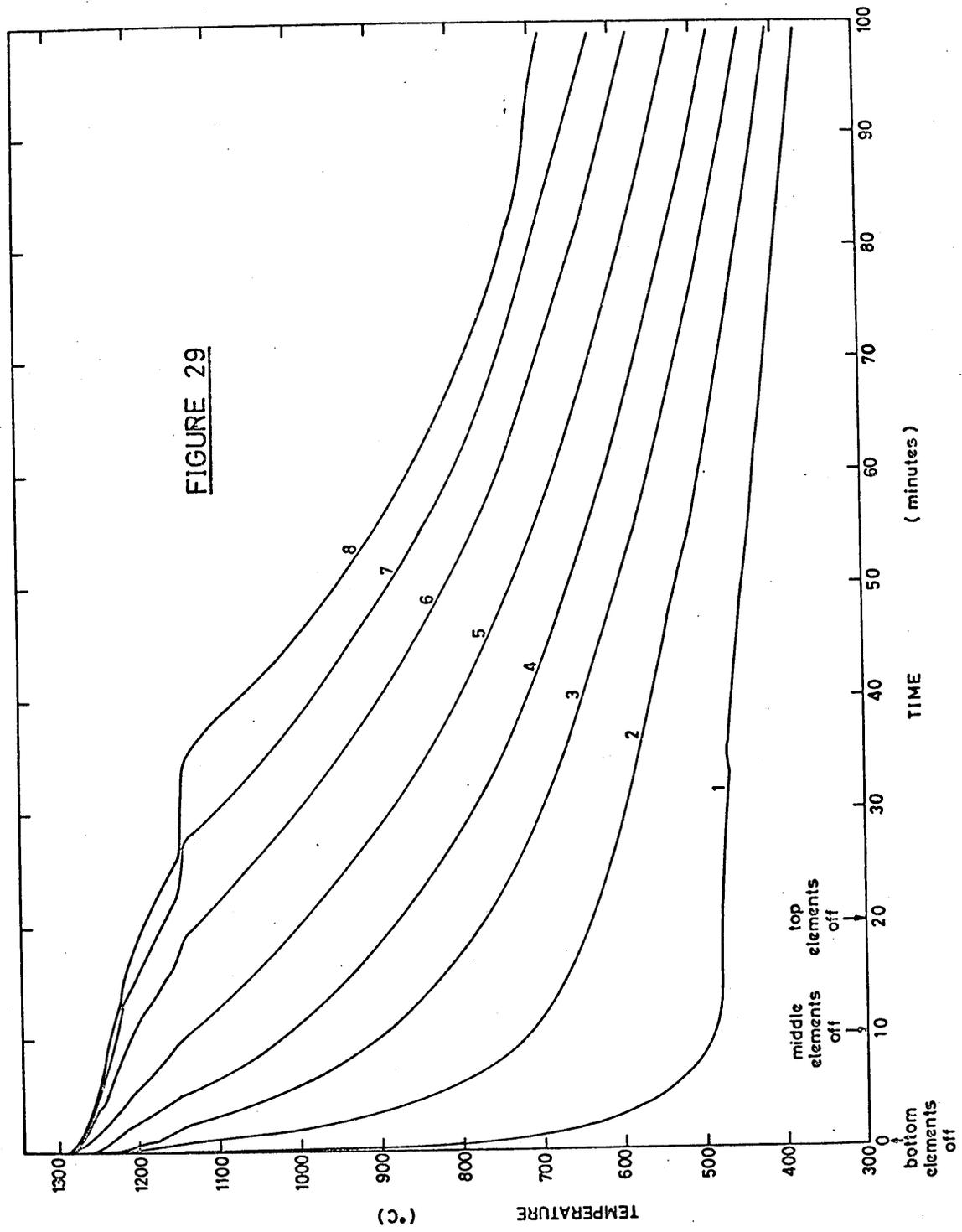


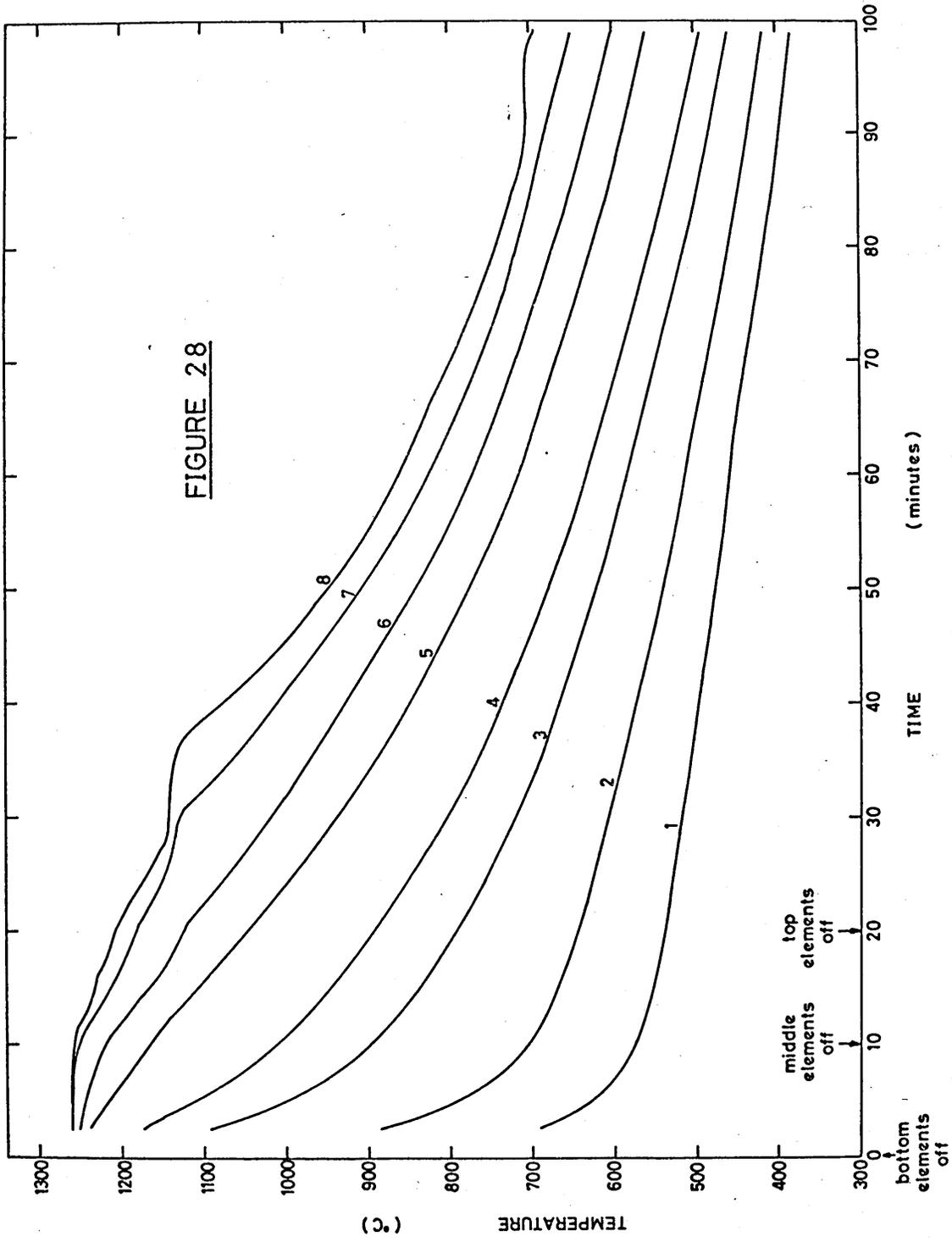


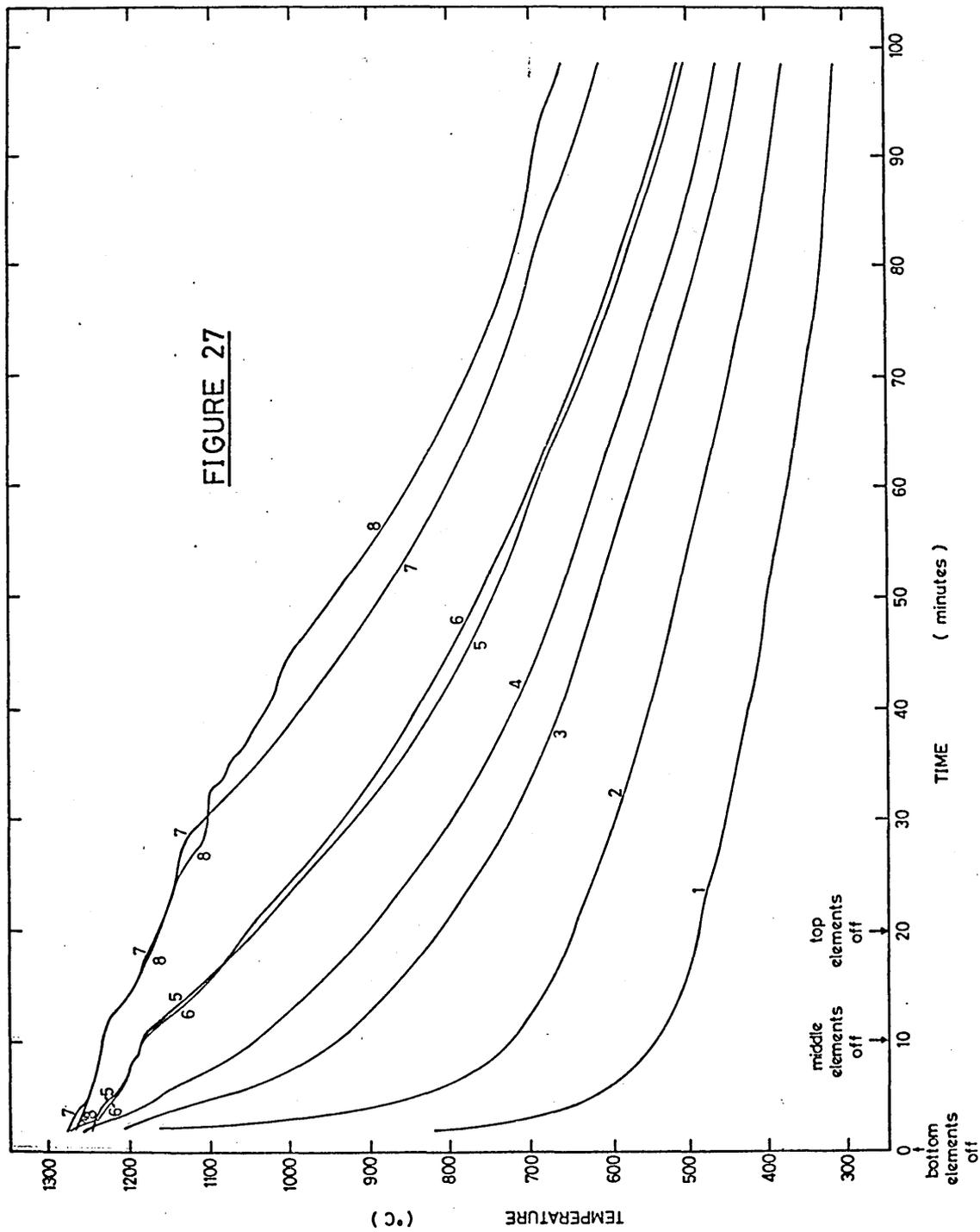


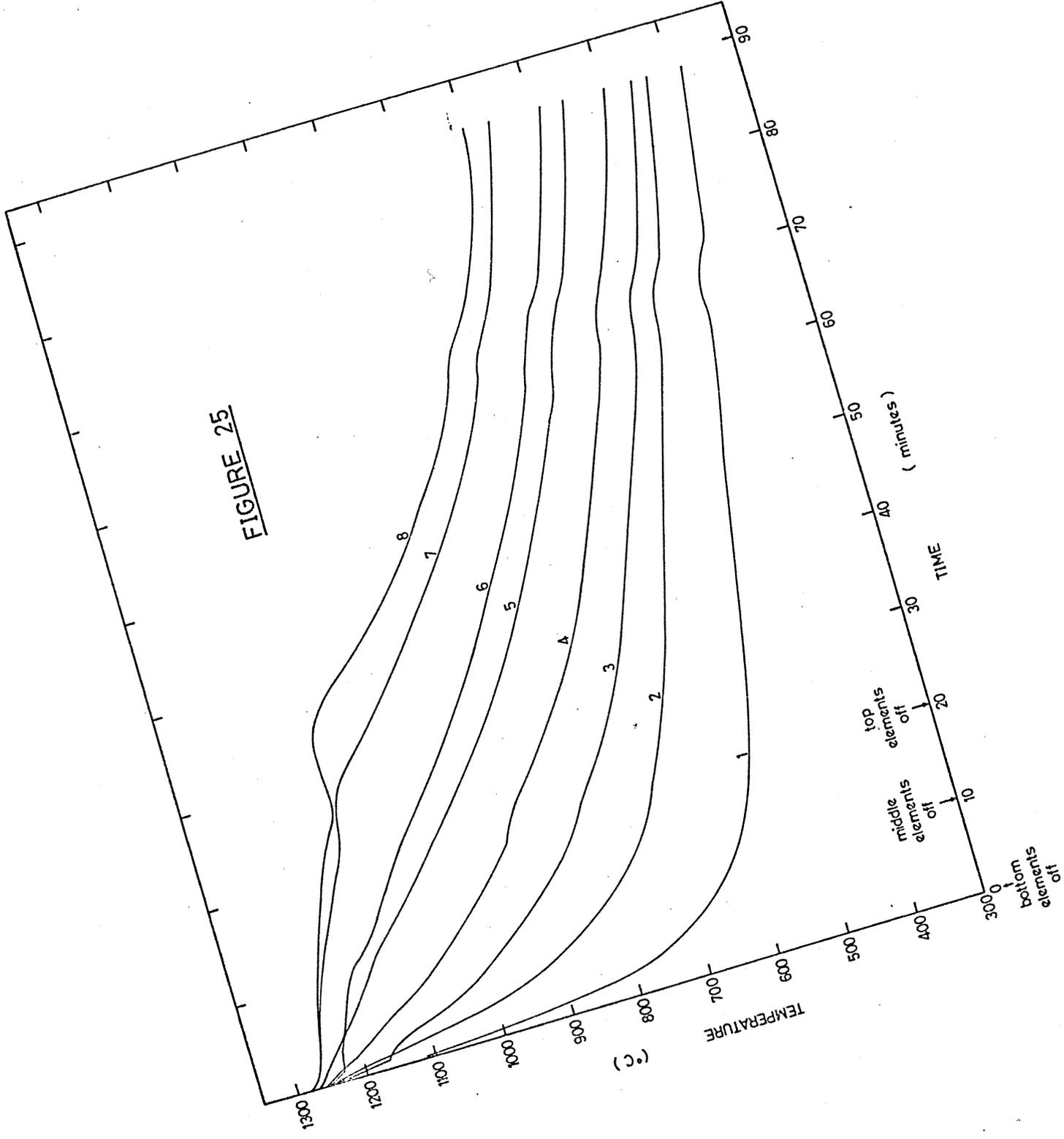












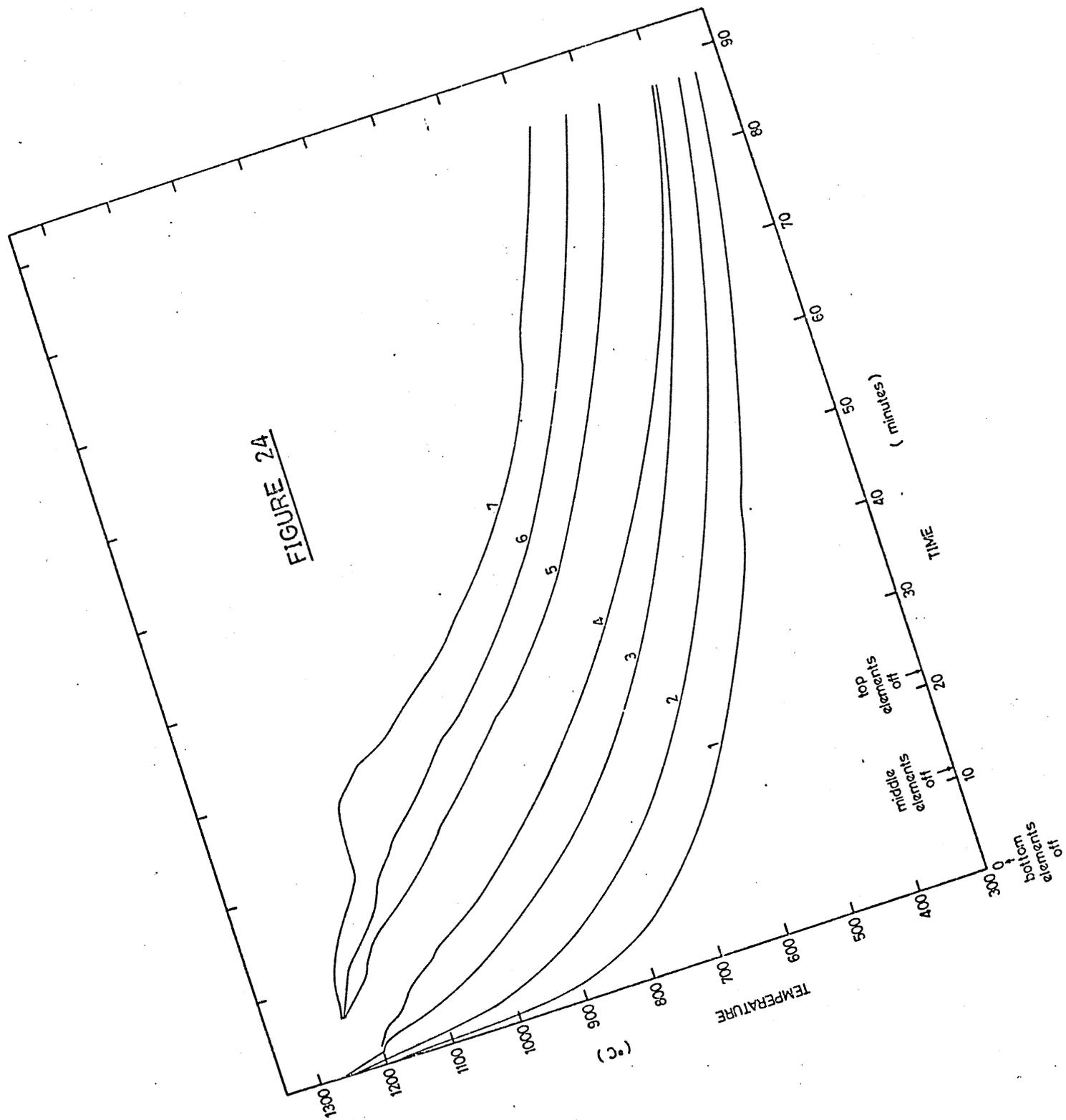


FIGURE 23

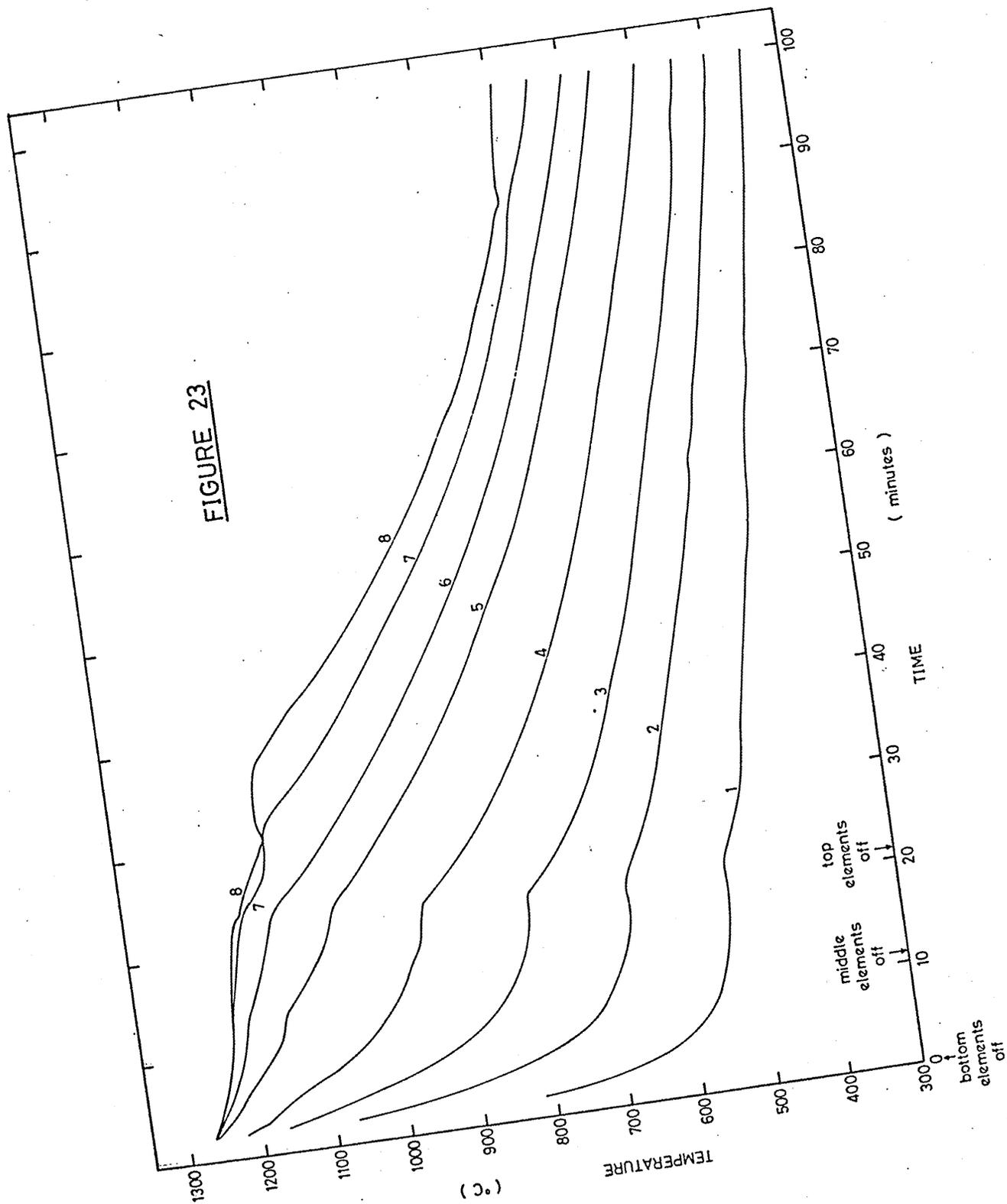
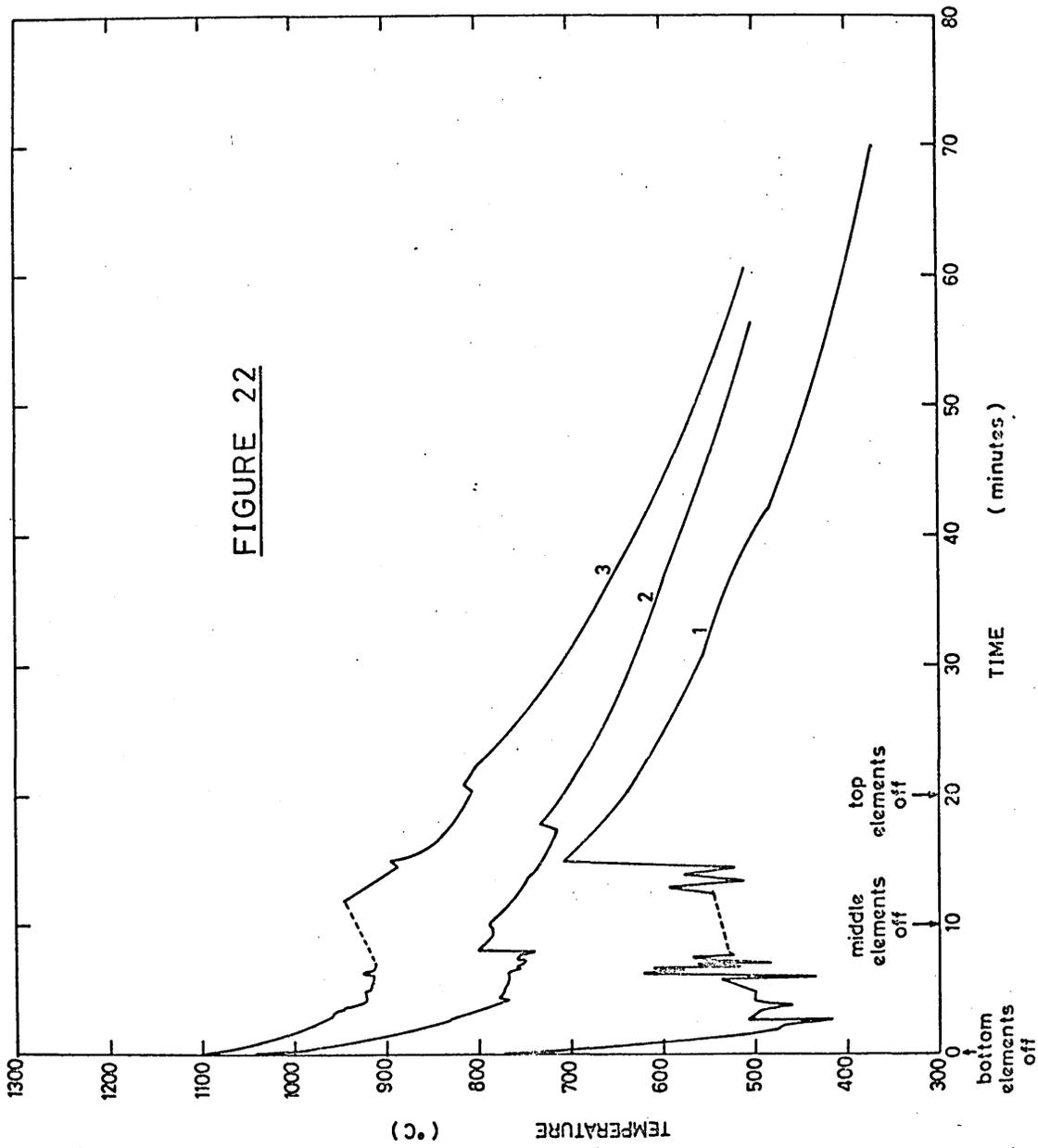


FIGURE 22



COOLING CURVES FOR THE GREY

IRON MELT PROGRAMME (FIGURES 22-60)

The following cooling curves have been obtained from the grey iron melt programme castings and are correlated as follows:-

LOW NITROGEN CASTINGS

Figure No.	Cast No.
22	Ala
23	Alb
24	Alc
25	A1
26	A2
27	A3
28	B1
29	B2
30	B3
31	C1
32	C2
33	C3
34	E1a
35	E1
36	E2
37	E3
38	F1
39	F2a
40	F2
41	F3
42	G1
43	G2
44	G3

HIGH NITROGEN CASTINGS

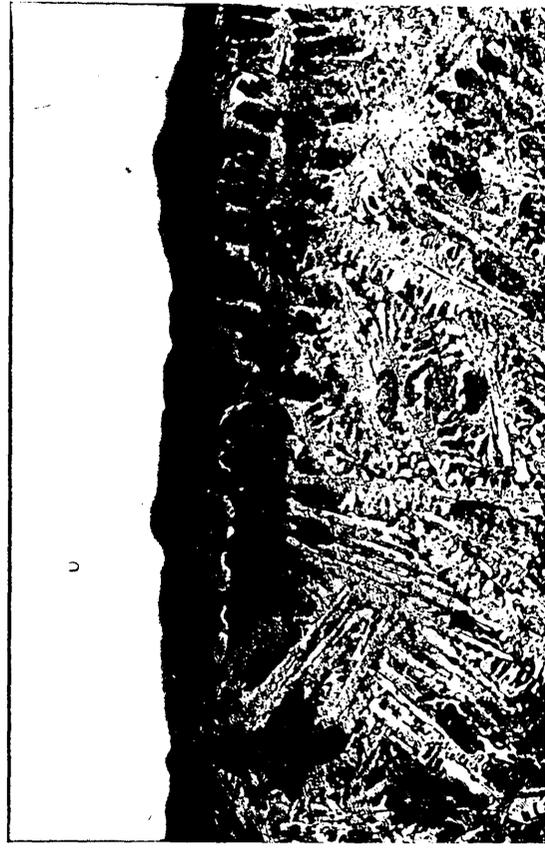
Figure No.	Cast No.
45	Ala'
46	A1'
47	A2'
48	A3'
49	B1'
50	B2'
51	B3a'
52	B3'
53	C1'
54	C2'
55	C3'
56	F1'
57	F2'
58	F3'
59	D1'
60	D3'

Table 15 - Continued

Cast	Elements											Cooling Curve Figure	Fracture Plate No.
	C	Si	Ti	N	P	Si	Mn	Cr	B	Al			
	TABLE 15b HIGH NITROGEN MELTS												
A1a'	3.80	0.02	-	.0112	0.02	0.95	0.83	0.07	0.004	<0.001	45	159	
A1'	3.80	0.03	-	0.012	0.02	1.04	0.86	0.05	0.005	<0.001	46	139	
A2'	3.80	0.05	-	0.0118	0.02	1.00	0.89	0.05	0.005	<0.001	47	139	
A3'	3.80	0.09	-	0.010	0.02	0.92	0.82	0.06	0.005	<0.001	48	139	
B1'	3.80	0.18	0.093	0.0084	.015	0.87	0.87	0.07	0.005	0.001	49	139	
B2'	3.70	0.06	0.091	0.0091	0.01	0.95	0.85	.035	0.003	0.001	50	139	
B3a'	3.70	0.11	0.094	0.015	0.02	0.90	0.86	0.04	0.005	0.001	51	-	
B3'	3.65	.115	0.090	0.009	0.02	0.84	0.80	0.06	0.005	0.002	52	139	
C1'	3.60	0.02	0.120	0.009	0.02	0.85	0.74	0.05	0.005	<0.002	53	139	
C2'	3.70	0.05	0.112	0.010	0.02	0.84	0.78	0.05	0.005	0.002	54	139	
C2a'	3.57	0.06	0.130	0.010	0.02	0.79	0.825	0.05	0.005	0.002	-	-	
C3'	3.60	0.10	0.130	0.009	0.02	0.83	0.80	0.06	0.005	0.002	55	139	
D1'	3.60	0.26	0.180	0.008	0.018	0.78	0.82	0.06	0.005	0.001	59	139	
D3'	3.68	0.15	0.210	0.009	0.016	0.89	0.80	0.05	0.004	0.004	60	139	
F1'	3.60	.021	0.410	0.009	0.01	0.80	0.74	0.05	0.003	0.001	56	139	
F2'	3.64	0.06	0.380	0.0091	0.02	0.78	0.80	0.03	0.003	0.002	57	139	
F3'	3.65	0.10	0.380	0.0091	0.02	0.75	0.79	0.07	0.001	0.002	58	139	

Table 15 - Cast Compositions for the Grey Iron Melt Programme

Cast	Elements											Cooling Curve Figure	Fracture Plate No.
	C	S	Ti	N	P	Si	Mn	Cr	B	Al			
	TABLE 15a LOW NITROGEN MELTS												
Ala	3.42	0.02	-	0.005	0.02	0.97	0.86	0.11	0.003	0.001	0.001	22	59
Alb	3.55	0.02	-	0.0048	0.02	1.17	0.84	0.08	0.003	<0.001	<0.001	23	59
Alc	4.02	0.02	-	0.0056	0.02	1.16	0.87	0.08	0.003	<0.001	<0.001	24	59
A1	3.90	0.02	-	0.0064	0.02	1.01	0.80	0.09	0.005	<0.001	<0.001	25	35
A2	3.80	0.045	-	0.0057	.026	1.05	0.82	0.08	0.004	<0.001	<0.001	26	35
A3	3.80	0.104	-	0.006	0.02	0.95	0.80	0.08	0.003	<0.001	<0.001	27	35
B1	3.65	0.03	0.091	0.0047	0.02	0.94	0.85	0.06	0.002	0.002	0.002	28	35
B2	3.75	0.06	0.091	0.004	0.02	0.955	0.92	0.05	0.005	0.001	0.001	29	35
B3	3.65	0.10	.0915	0.0051	0.02	0.91	0.85	0.06	0.005	0.001	0.001	30	35
C1	3.75	0.015	0.143	0.0044	0.02	1.00	0.80	0.04	0.003	0.002	0.002	31	35
C2	3.80	0.068	0.137	0.0049	0.02	1.04	0.80	0.04	0.003	0.002	0.002	32	35
C3	3.80	0.110	0.137	0.0046	0.02	0.95	0.80	0.04	0.002	0.001	0.001	33	35
E1a	3.80	0.02	0.293	0.0038	0.02	1.01	.825	0.08	0.004	0.002	0.002	34	133
E1	3.65	0.022	0.330	0.005	0.02	0.80	0.76	0.05	0.005	0.001	0.001	35	35
E2	3.60	0.045	0.316	0.005	.019	0.80	0.70	0.05	0.003	0.001	0.001	36	35
E3	3.70	0.098	0.316	0.004	.018	0.87	0.80	0.05	0.003	0.002	0.002	37	35
E3a	3.52	0.120	0.340	0.004	0.02	0.90	0.80	0.05	0.003	0.002	0.002	-	134
F1	3.60	0.024	0.390	0.0041	0.01	0.90	0.81	0.04	0.002	0.007	0.007	38	35
F2a	3.75	0.050	0.390	0.0046	0.02	0.97	0.76	0.05	0.002	0.002	0.002	39	136
F2	3.60	0.050	0.390	0.0045	0.01	0.94	0.80	0.04	0.004	0.002	0.002	40	35
F3	3.70	0.100	0.377	0.0047	0.02	0.99	0.77	0.04	0.002	0.002	0.002	41	35
G1	3.80	0.017	0.490	0.004	0.02	0.90	0.85	0.06	0.003	0.004	0.004	42	35
G2	3.80	0.060	0.408	0.003	0.02	1.20	0.78	0.08	0.004	0.001	0.001	43	35
G3	3.80	0.100	0.435	0.003	0.02	1.02	.805	0.08	0.004	0.001	0.001	44	35



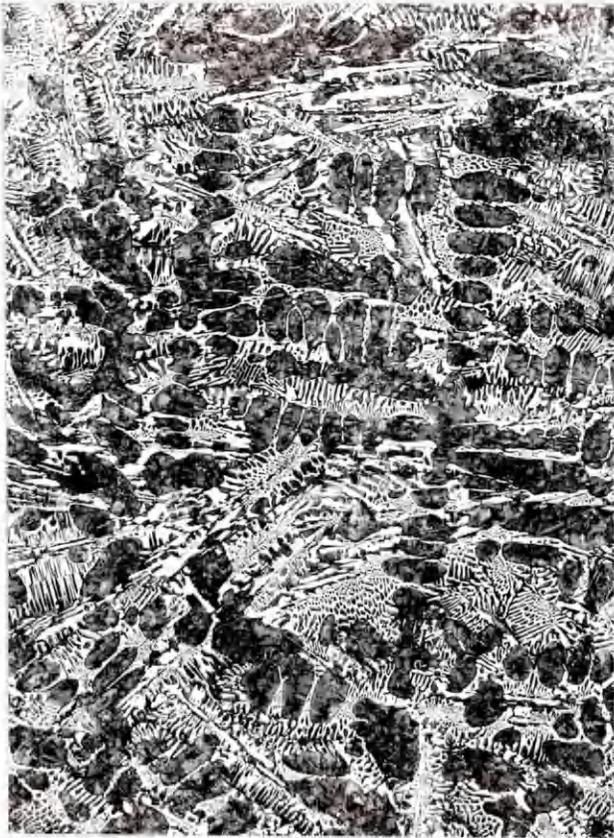
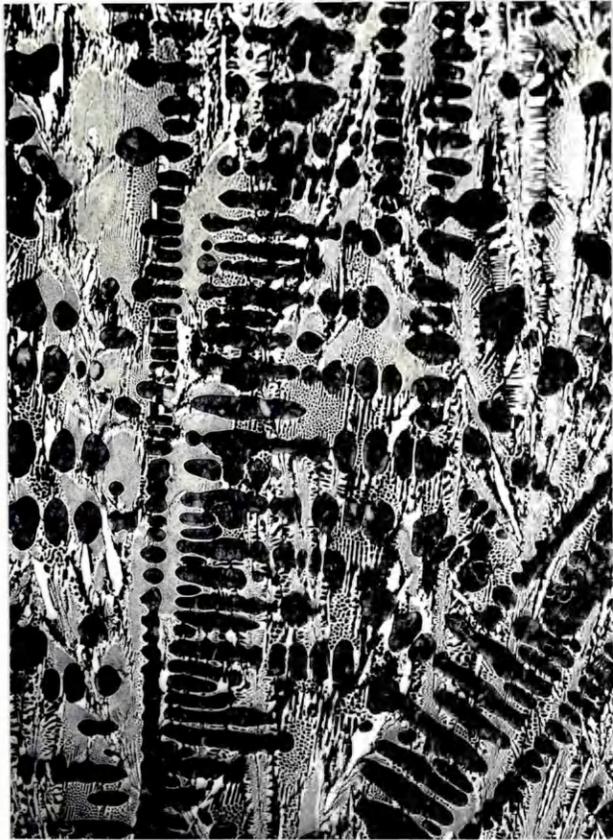


PLATE 32

Melt 17, 101.6mm (9.525mm) x40

PLATE 33

Melt 17, 177.8mm (9.525mm) x 40

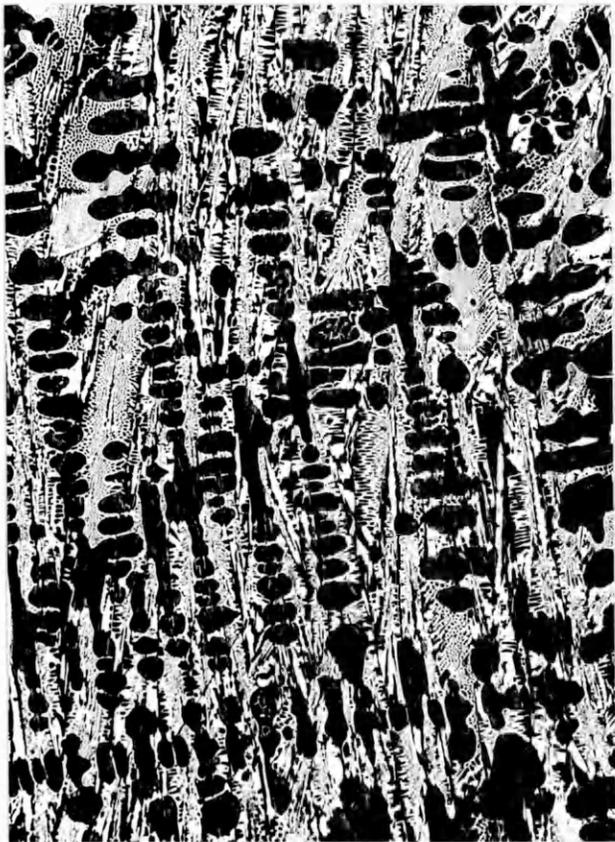


PLATE 30

Melt 17, 35mm (9.525mm)
X 50

PLATE 31

Melt 17, 63.5mm (9.525mm)
X 50

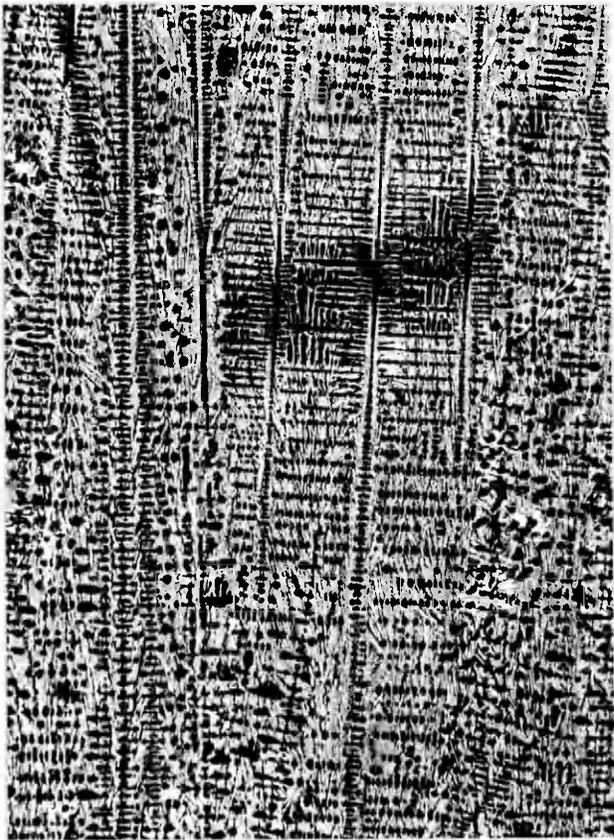
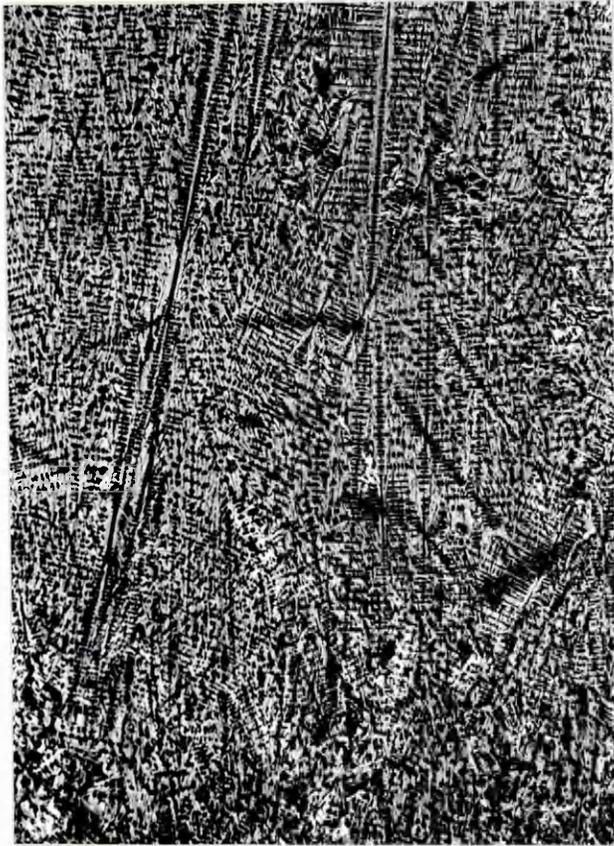


PLATE 28

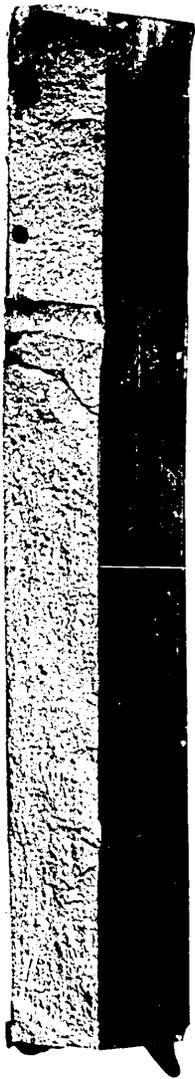
Melt 17, Omm (9.525mm)

X 50

PLATE 29

Melt 17, 1Omm (9.525mm)

X 50



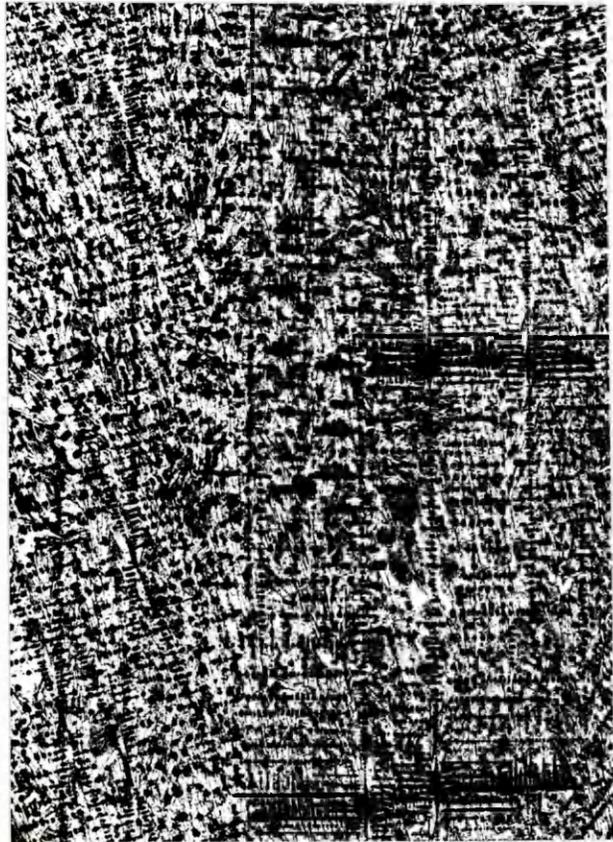
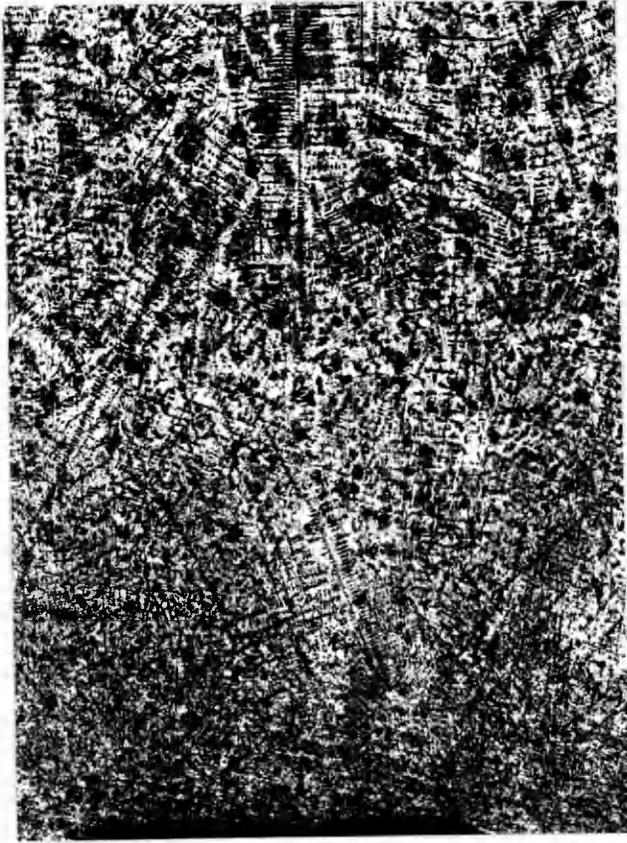


PLATE 25

Melt 16, Omm (9.525mm)

X 50

PLATE 26

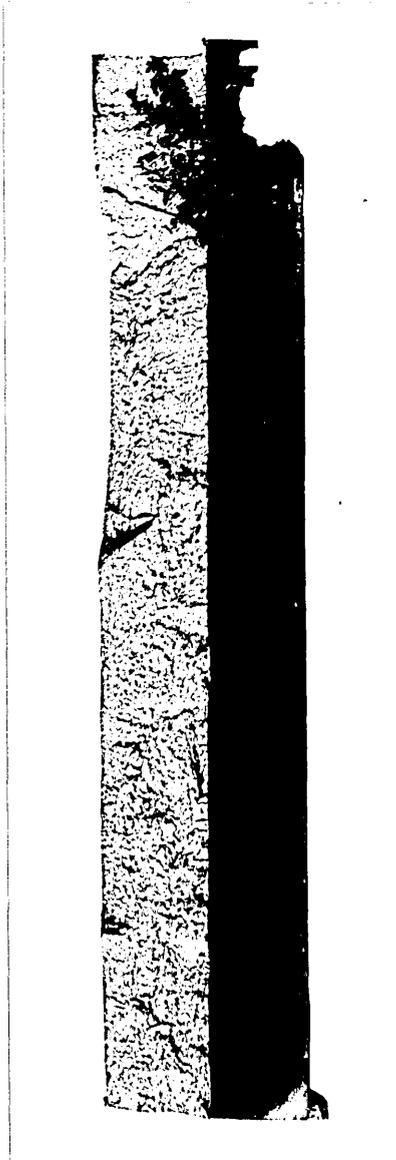
Melt 16, 12.7mm (9.525mm)

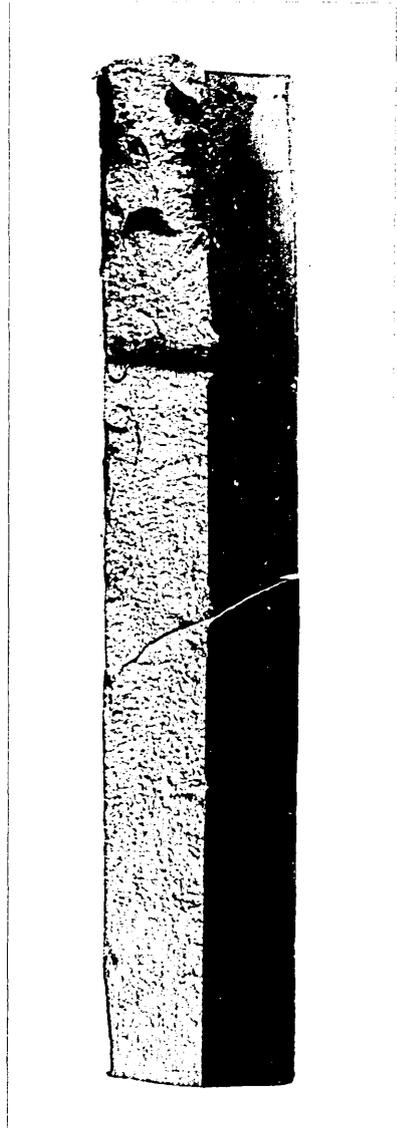
X 50

The details of the following microstructures, etched in 2% nital, are given as follows:-

Cast number, distance from the chill, (distance from the T/C edge) and magnification.

The photographs are orientated with the chill/metal interface towards the bottom of the plates.





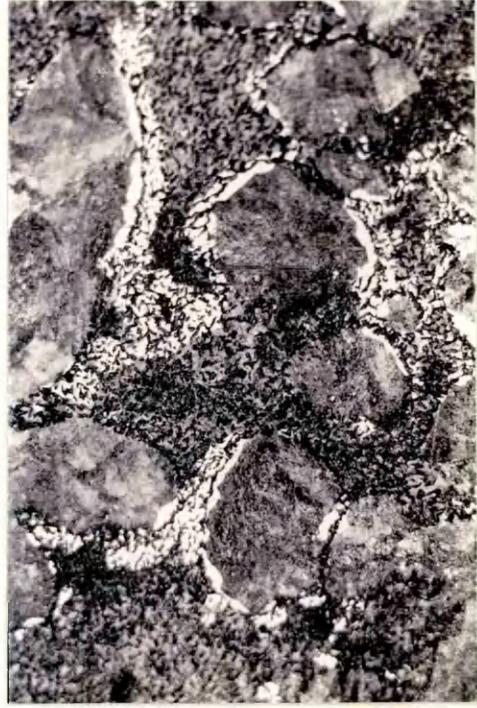


PLATE 87

C1. 185mm (32.1mm)

x 63

4.17°C/Min

PLATE 88

C1. 181mm (20.5mm)

x 16

4.35°C/Min

PLATE 89

C1. 181mm (20.5mm)

x 63

4.35°C/Min

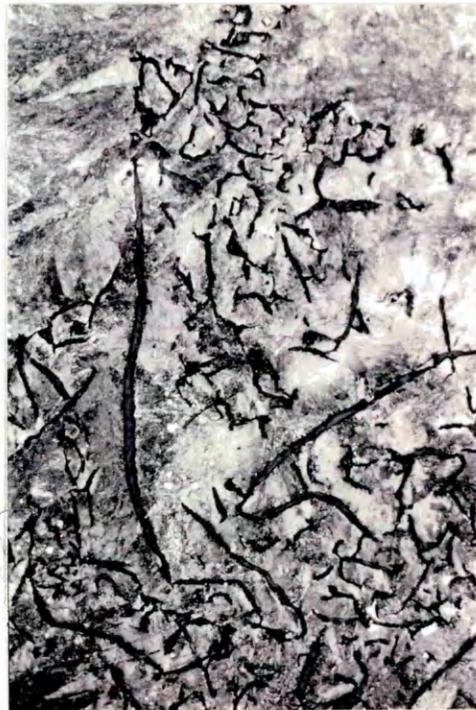
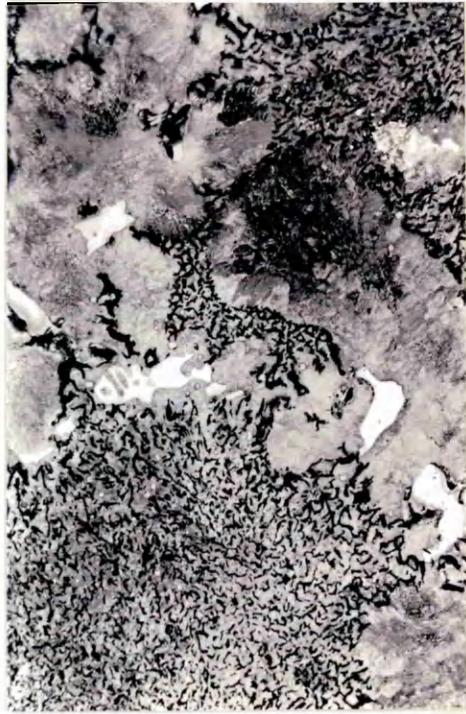


PLATE 90

G1. 0mm (28.6mm)
x 16

635°C/Min

PLATE 91

G1. 44mm (28.6mm)
x 16

21.88°C/Min

PLATE 92

F1. 63.5mm (32.1mm)
x 16

12.33°C/Min

PLATE 93

G1. 118mm (25.1mm)
x 16

6.89°C/Min



PLATE 94

E1. 89mm (34.1mm)
x 63

9.79°C/Min

PLATE 95

F1. 89mm (30.1mm)
x 16

9.79°C/Min

PLATE 96

Enlargement of Plate 95
x 63

9.79°C/Min



PLATE 97

G1. 89mm (19.05mm)
x 16

9.79°C/Min

PLATE 98

E1. 127.1mm (21.1mm)
x 16

6.28°C/Min

PLATE 99

Enlargement of Plate 98
x 63

6.28°C/Min

PLATE 100

Enlargement of Plate 98
x 160

6.28°C/Min



PLATE 101

F1. 127.1mm (35.1mm)
x 16

6.28°C/Min

PLATE 102

G1. 136mm (25.6mm)
x 16

5.82°C/Min

PLATE 103

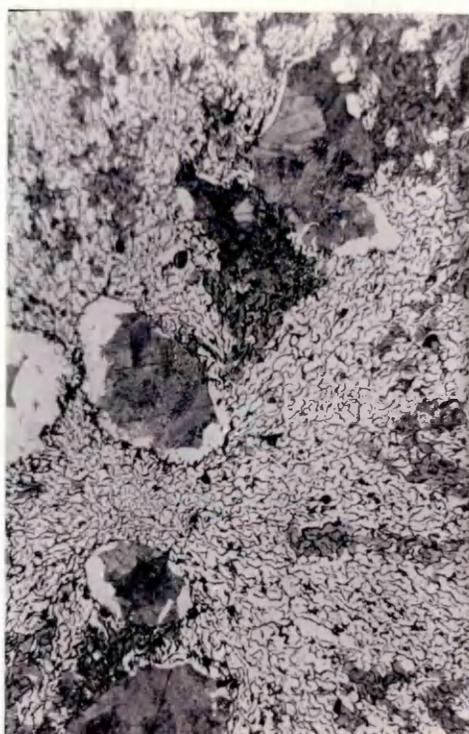
F1. 177.8mm (24.6mm)
x 16

4.43°C/Min

PLATE 104

Enlargement of Plate 103
x 160

4.43°C/Min



MICROSTRUCTURAL CRITERIA FOR THE LOW NITROGEN GREY IRON CASTINGS

Sulphur Levels	Cast Groups					
	A	B	C	E	F	G
1	12.7	12.7	26	38.1	38.1	38.1
2	12.7	25.4	25.4	38.1	38.1	25.4
3	27.4	38.1	26.4	30.4	12.7	28.7

Table 20(a) Streamer Graphite Start (mm)

Sulphur Levels	Cast Groups					
	A	B	C	E	F	G
1	25.4	38.1	33.5	44	63.5	75
2	25.4	49.1	38.1	73	58	38.1
3	63.5	63.5	38.1	63.5	50	47.6

Table 20(b) 'Grey' Start (mm)

Sulphur Levels	Cast Groups					
	A	B	C	E	F	G
1	63.5	64.5	89	127.1	127.1	136
2	63.5	76.1	63.7	141	116	127.1
3	73.5	107.1	90.5	127.1	127.1	127.1

Table 20(c) Graphitic Cell Start (mm)

Sulphur Level	Cast Groups					
	A	B	C	E	F	G
1	A	D	A/D	D	D	D
2	A	A/D	A/D	D	D/Deg.	D/Deg.
3	A/D	A/Dpred	A/D	D	Dpred/A/Deg.	D/Deg.

Table 20(d) Type of Graphite at 177.8mm

pred.=predominantly

deg.=degenerate

PLATE 105

B2. 63.5mm (28.6mm)
x 16

12.33°C/Min

PLATE 106

B2. 112mm (28.6mm)
x 160

7.38°C/Min

PLATE 107

B2. 127.1mm (28.6mm)
x 63

6.28°C/Min

PLATE 108

B2. 127.1mm (33.1mm)
x 32

6.28°C/Min

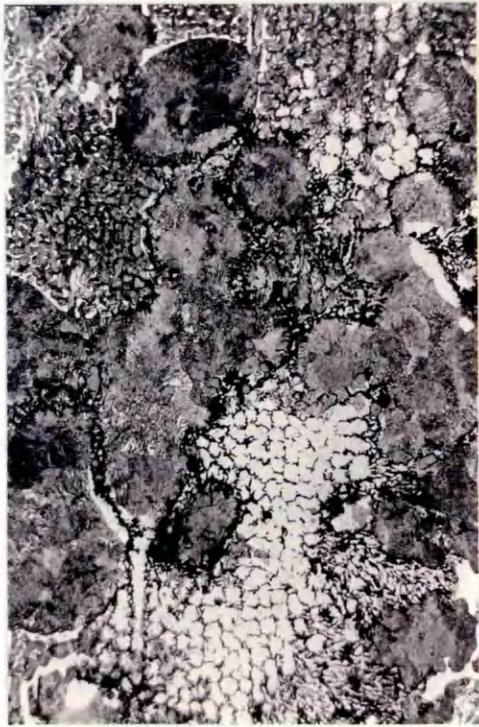
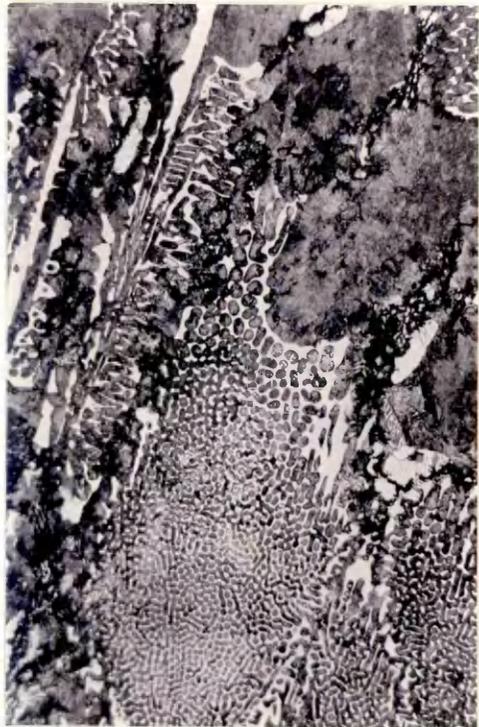


PLATE 109

B2. 178mm (19.05mm)
x 63

4.40°C/Min

PLATE 110

B3. 153.6mm (34.1mm)
x 160

5.25°C/Min

PLATE 111

B3. 184mm (30.10mm)
x 16

4.25°C/Min

PLATE 112

B3. 178mm (31.1mm)
x 16

4.40°C/Min



PLATE 113

C2. 45.1mm (28.6mm)
x 16

21.18°C/Min

PLATE 114

C2. 145mm (27.1mm)
x 16

5.52°C/Min

PLATE 115

C2. 187mm (19.05mm)
x 63

4.15°C/Min

PLATE 116

Enlargement of Plate 115
x 160

4.15°C/Min

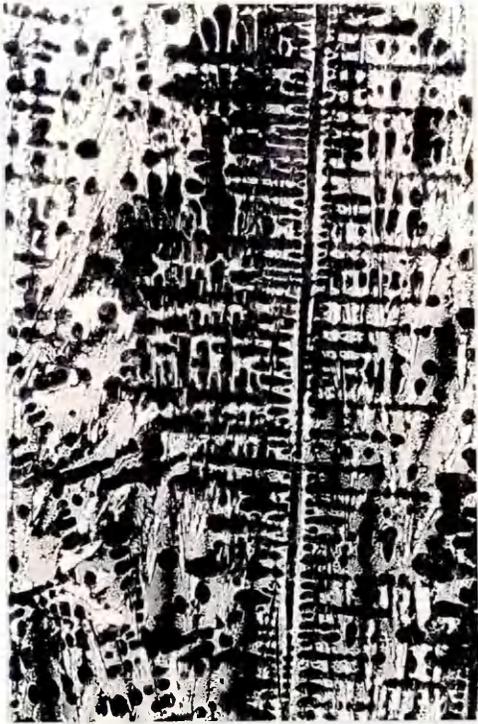


PLATE 117

C3. 38.1mm (22.1mm)
x 16

25.62°C/Min

PLATE 118

Enlargement of Plate 117
x 63

25.62°C/Min

PLATE 119

C3. 164mm (33.1mm)
x 16

4.84°C/Min

PLATE 120

E2. 42.5mm (5mm)
x 160

22.91°C/Min

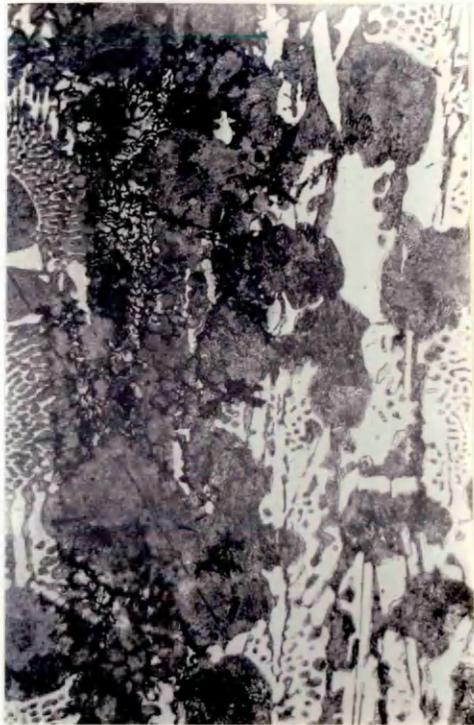


PLATE 121

E3. 63.5 mm (35.1mm)
x 160

12.33°C/Min

PLATE 122

E3. 127.1mm (19.05mm)
x 160

6.28°C/Min

PLATE 123

F2. 70mm (9.525mm)
x 16

11.56°C/Min

PLATE 124

F2. 181.5mm (26.1mm)
x 63

4.32°C/Min



PLATE 125

F3. 66mm (9.525mm)
x 16

12.02°C/Min

PLATE 126

F3. 63.7mm (19.05mm)
x 63

12.30°C/Min

PLATE 127

F3. 127.1mm (9.525mm)
x 32

6.28°C/Min

PLATE 128

F3. 177.8mm (11mm)
x 16

4.43°C/Min

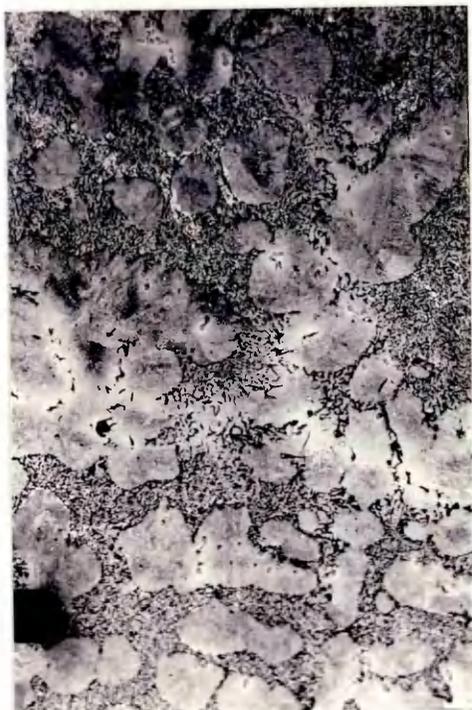


PLATE 129

G2. 65.5mm (22.6mm)

x 16

11.97°C/Min

PLATE 130

Enlargement of Plate 129

x 63

11.97°C/Min

PLATE 131

G2. 127.1mm (22.1mm)

x 63

6.28°C/Min

PLATE 132

G2. 177.8mm (15.0mm)

x 160

4.43°C/Min





ADDITIONAL LOW NITROGEN CASTS

PLATE 134

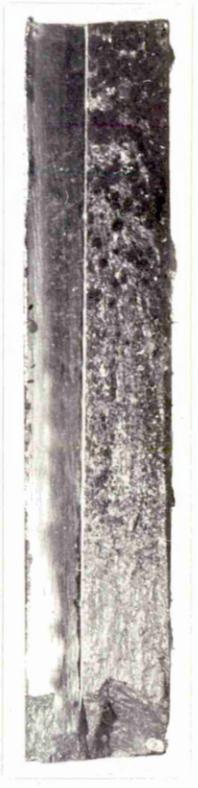
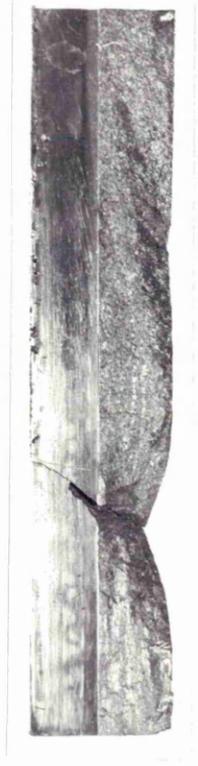
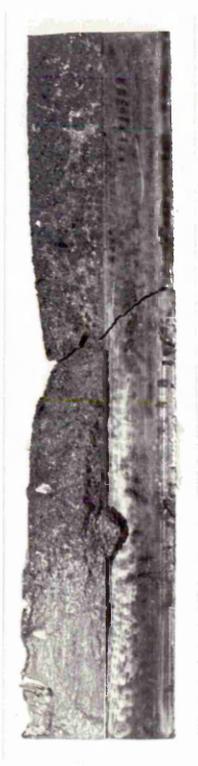
Cast E1a

PLATE 135

Cast E3a

PLATE 136

Cast F2a



MICROSTRUCTURAL CRITERIA FOR THE ADDITIONAL CASTINGS

Criteria	Cast Groups					
	Ala	Alb	Alc	E1a	E3a	F2a
Streamer Start (mm)	17	>12.7 <25.4	-	12.7	63.5	25.4
'Grey' Start (mm)	54	20	-	63.5	178	52.1
Cell Start (mm)	70	50	0	127.1	-	100
Graphite at 177.8mm	A & D	A & Dpred	Large A	D & Deg.	D & Deg. round T/C	D

Table 21a Low Nitrogen Melts

Criteria	Cast Groups		
	E1a'	B3a'	C2a'
(a) Streamer Start (mm)	25.4	25.4	12.7
(b) 'Grey' Start (mm)	38.1	63.5	38.1
(c) Cell Start (mm)	127.1	127.5	127.1
(d) Graphite at 177.8mm	A & Small amount D	A & D	Fine A & D & Deg.

Table 21b High Nitrogen Melts

PLATE 137

E3a 177.8mm (6mm)
x 160

4.43°C/Min

PLATE 138

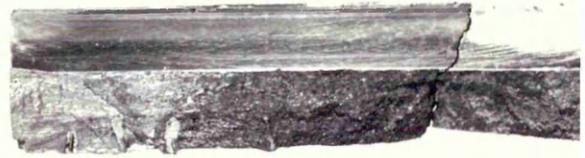
F2a 64.8mm (9.525mm)
x 63

12.08°C/Min



PLATE 139

FRACTURED CASTINGS FOR THE HIGH NITROGEN MELT PROGRAMME



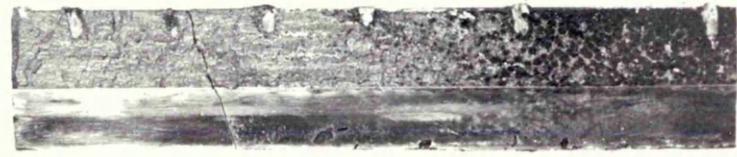
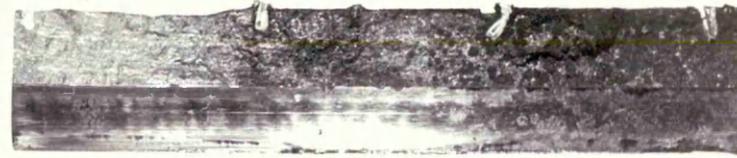
A3'

B3'

C3'

D3'

F3'



MICROSTRUCTURAL CRITERIA FOR THE HIGH NITROGEN GREY IRON CASTINGS

Sulphur Level	Cast Groups				
	A'	B'	C'	D'	F'
1	25.4	38.1	16.7	16.0	38.1
2	25.4	25.4	12.7	-	38.1
3	29.0	15.5	21.5	25.4	28.4

Table 22a Streamer Graphite Start (mm)

Sulphur Level	Cast Groups				
	A'	B'	C'	D'	F'
1	41.1	89	38.1	39.6	-
2	42.5	38.1	38.1	-	-
3	63.5	38.1	38.1	57	130.2

Table 22b 'Grey' Start (mm)

Sulphur Level	Cast Groups				
	A'	B'	C'	D'	F'
1	89	105	63.7	89	127.1
2	89	63.5	63.5	-	106
3	127.1	89.0	92	89	130.2

Table 22c Graphitic Cell Start (mm)

Sulphur Level	Cast Groups				
	A'	B'	C'	D'	F'
1	A	Feathery D & Deg.	Deg. & A	A & Some D & Deg.	Deg.
2	A	> A & D	> A & Bit D	-	Deg. D
3	A & Deg. & Broad	A/D/ Deg./ Mesh	> D and A	A and Broad D	Deg.

Table 22d Graphite Type at 177.8 (mm)

PLATE 140

A1' 89mm (28.1mm)

x 32

9.79°C/Min

PLATE 141

Enlargement of Plate 140

x 160

9.79°C/Min

PLATE 142

A1' 187mm (31.6mm)

x 160

4.15°C/Min



PLATE 143

A1^o 179mm (34.1mm)

x 160

(Enlargement of Plate 144)

4.37^oC/Min

PLATE 144

A1^o 179mm (34.1mm)

x 16

4.37^oC/Min

PLATE 145

A1^o 179mm (9.525mm)

x 32

4.37^oC/Min



PLATE 146

A1^o 179mm (19.05mm)
x 63

4.37^oC/Min

PLATE 146A

Enlargement of Plate 146
x 160

4.37^oC/Min

PLATE 147

A2^o 63.5mm (9.525mm)
x 63

12.33^oC/Min

PLATE 148

A2^o 127.1mm (19.05mm)
x 160

6.28^oC/Min

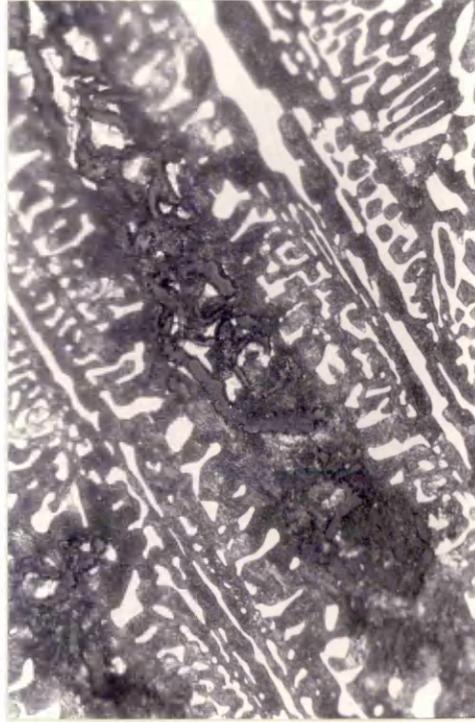
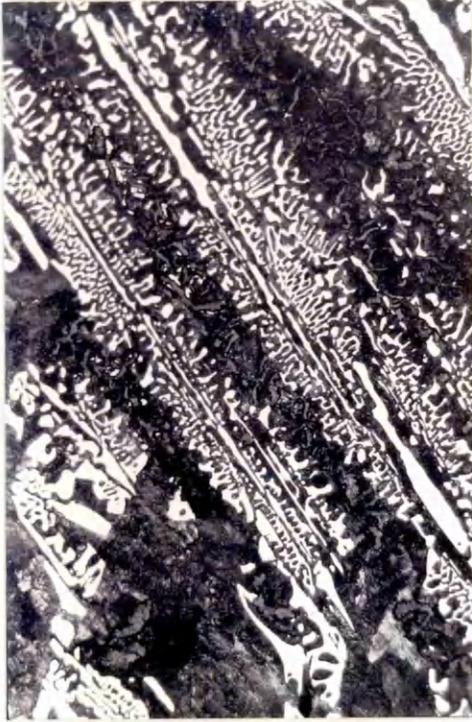


PLATE 149

A2^o 177.8mm (19.05mm)
x 63

4.43^oC/Min

PLATE 150

A2^o 182mm (22.6mm)
x 160

4.29^oC/Min

PLATE 151

A2^o 177.8mm (9.525mm)
x 160

4.43^oC/Min

PLATE 152

A3^o 63.5mm (9.525mm)
x 160

12.33^oC/Min

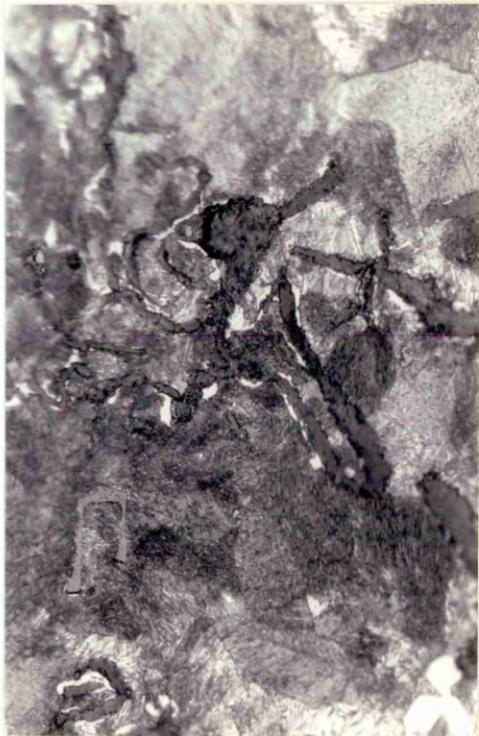


PLATE 153

A3' 177.8mm (35.1mm)
x 160

4.43°C/Min

PLATE 154

A3' 181mm (28.6mm)
x 63

4.35°C/Min



PLATE 155

THE FRACTURED CASTING OF CAST A1a^o



PLATE 156

A1a' 38.1mm (5mm)
x 160

25.62°C/Min

PLATE 157

B1' 89mm (16mm)
x 16

9.79°C/Min

PLATE 158

B1' 89mm (16mm)
x 160

9.79°C/Min

PLATE 159

B1' 127.1mm (28.6mm)
x 63

6.28°C/Min

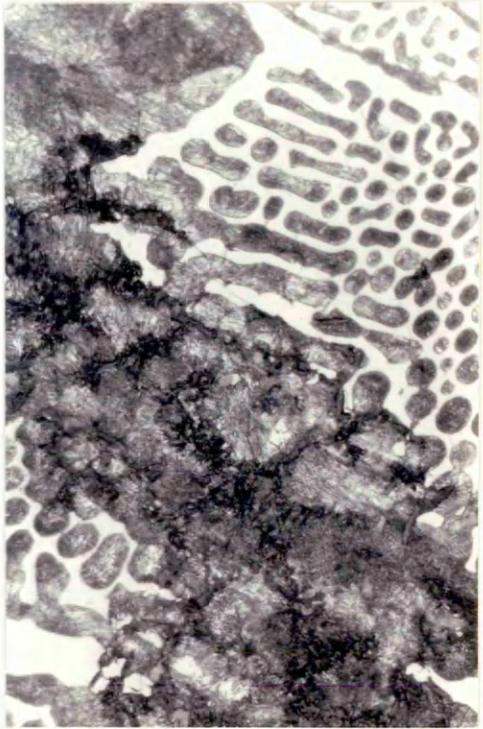


PLATE 160

B1' 177.8mm (28.6mm)

x 63

4.43°C/Min

PLATE 161

B2' 42.5mm (9.525mm)

x 16

22.91°C/Min

PLATE 162

B2' 38.1mm (10mm)

x 160

25.62°C/Min



PLATE 163

B2' 63.5mm (31.5mm)
x 160

12.33°C/Min

PLATE 164

B2' 89mm (33.1mm)
x 32

9.79°C/Min

PLATE 165

B2' 177.8mm (1.5mm)
x 63

4.43°C/Min

PLATE 166

B3' 25.4mm (19.05mm)
x 160

48.10°C/Min

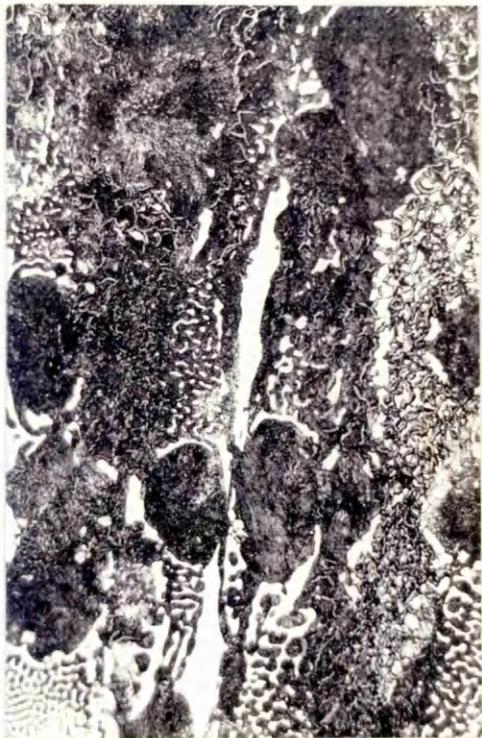


PLATE 167

B3° 63.5mm (19.05mm)
x 63
12.33°C/Min

PLATE 168

Enlargement of Plate 167
x 160
12.33°C/Min

PLATE 169

B3° 89mm (19.05mm)
9.79°C/Min

PLATE 170

B3° 127.1mm (27.6mm)
x 63
6.28°C/Min



PLATE 171

B3^o 177.8mm (12.5mm)
x 160

4.43^oC/Min

PLATE 172

C1^o 127.1mm (13mm)
x 63

6.28^oC/Min

PLATE 173

C1^o 127.1mm (31.1mm)
x 63

6.28^oC/Min

PLATE 174

C1^o 177.8mm (5mm)
x 32

4.43^oC/Min



PLATE 175

C2' 177.8mm (24.6mm)
x 63

4.43°C/Min

PLATE 176

C3' 177.8mm (23.1mm)
x 16

4.43°C/Min

PLATE 177

D1' 63.5mm (23.6mm)
x 160

12.33°C/Min

PLATE 178

D1' 63.5mm (19.05mm)
x 160

12.33°C/Min

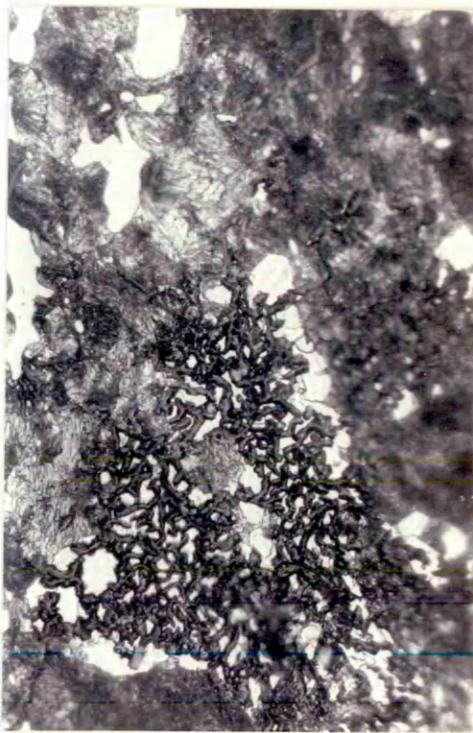
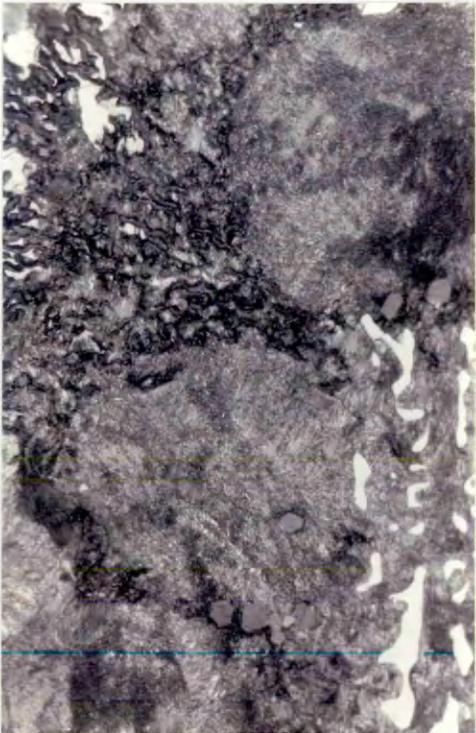
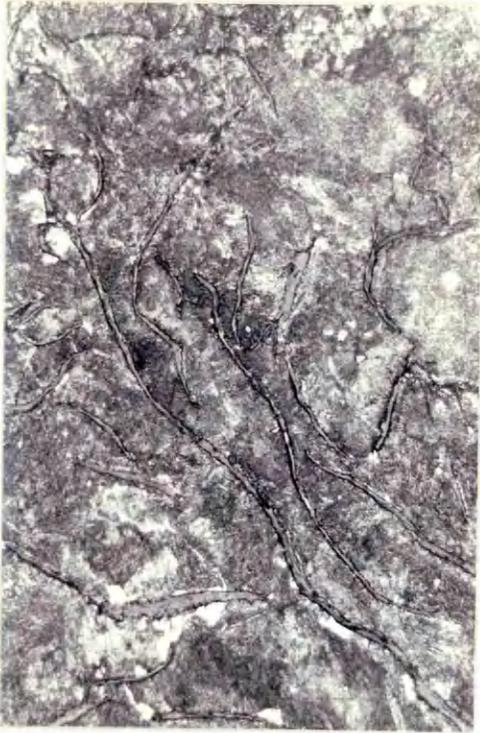


PLATE 179

D1' 89mm (15mm)

x 63

9.79°C/Min

PLATE 180

D1' 181.5mm (9.525mm)

x 160

4.32°C/Min

PLATE 181

D3' 89mm (8.5mm)

x 160

9.79°C/Min

PLATE 182

D3' 89mm (10mm)

x 160

9.79°C/Min

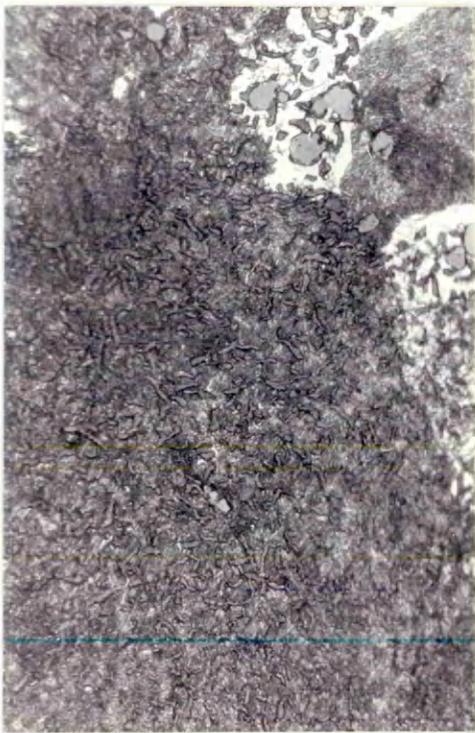


PLATE 183

D3'. 177.8mm (19.05mm)
x 16

4.43°C/Min

PLATE 184

F1'. 127.1mm (9.525mm)
x 63

6.28°C/Min

PLATE 185

F1'. 166.5mm (9.525mm)
x 160

4.76°C/Min

PLATE 186

F2'. 177.8mm (19.05mm)
x 16

4.43°C/Min



PLATE 187

F3'. 130.2mm (31.1mm)

x 160

6.14°C/Min

PLATE 188

F3'. 130.2mm (26.1mm)

x 160

6.14°C/Min

PLATE 189

F3'. 181mm (15.5mm)

x 63

4.35°C/Min



FRACTURED CASTINGS OF ADDITIONAL

HIGH NITROGEN CASTS

PLATE 190

Cast B3a^o

PLATE 191

Cast C2aⁱ

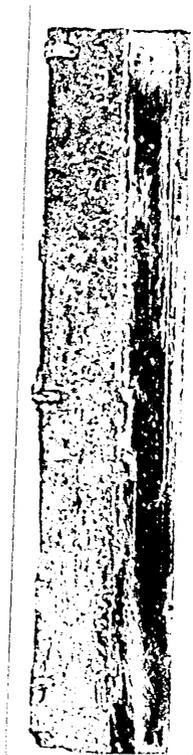


PLATE 193

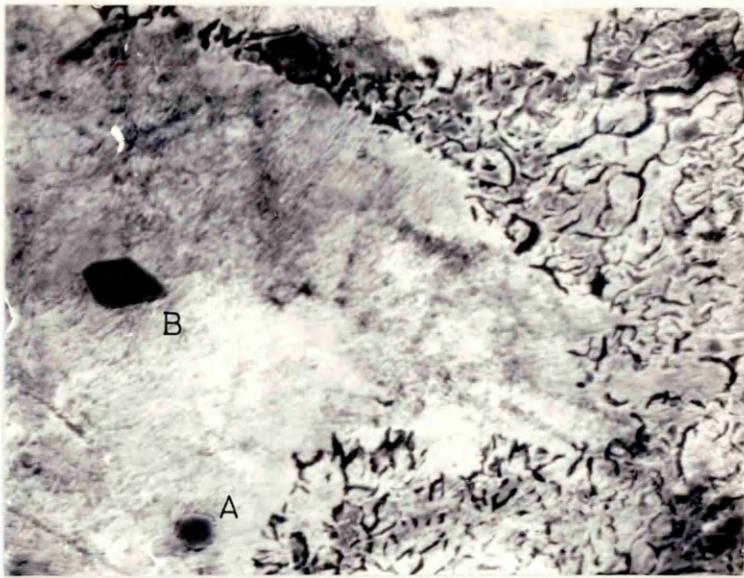
Melt G3 152.4 - 177.8mm x480

(a) Spectrum of Inclusion A shows the inclusion to be complex manganese titanium sulphide of the stoichiometry (Mn,Ti)S.

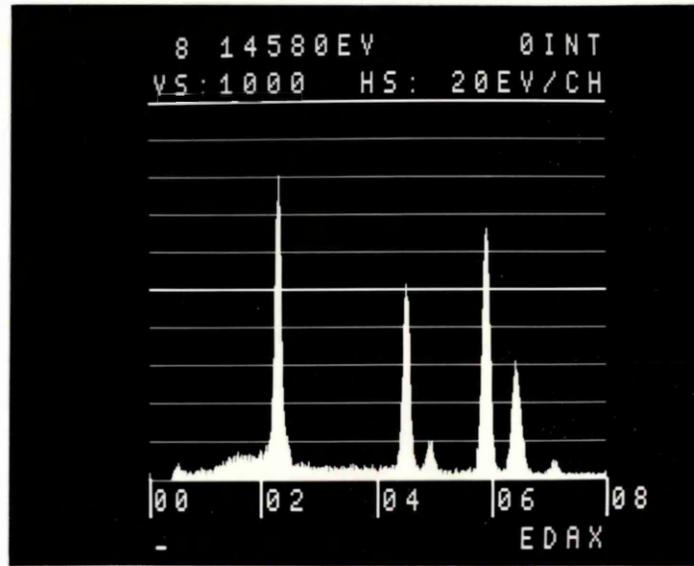
(b) Spectrum of Inclusion B shows :-

Sulphur integration peak height	6263
the background sulphur	<u>397</u>
	5866
Titanium integration peak height	<u>12,120</u>
the background titanium	340
	<u>11,780</u>

indicating a titanium : sulphur ratio of 2:1.
Thus the stoichiometry of the titanium sulphide inclusion is Ti_2S .

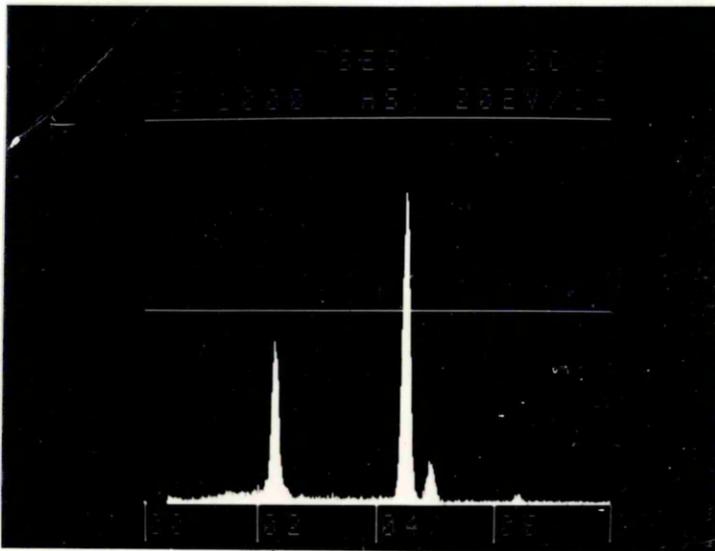


(a)



SK_α
TiK_α TiK_β MnK_α MnK_β+FeK_α FeK_β

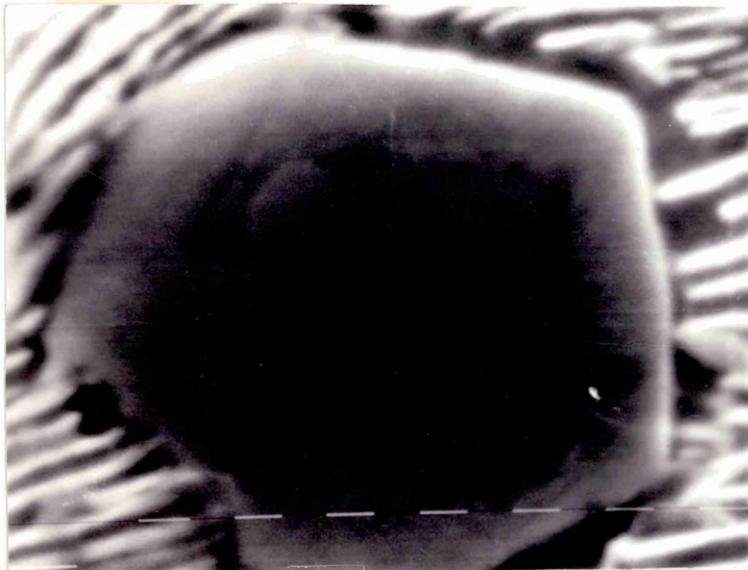
(b)



SK_α TiK_α TiK_β FeK_α

PLATE 194

Inclusion A from Plate 193. X8320

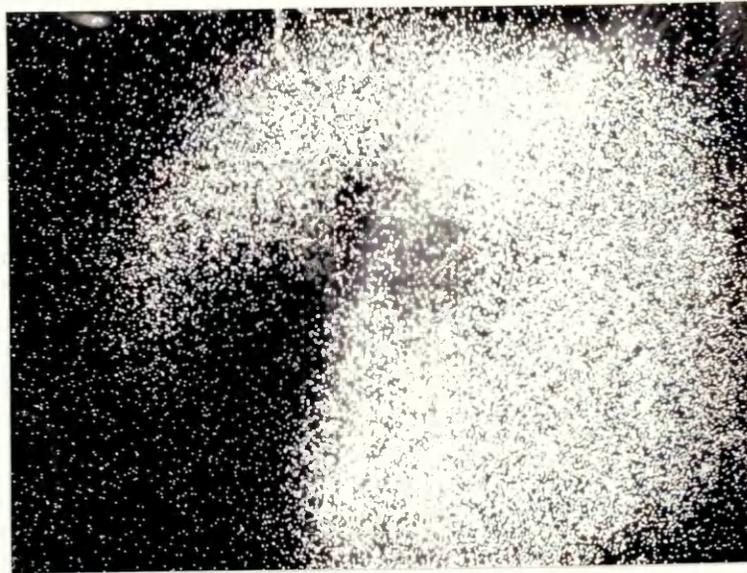


EDAX Scans for

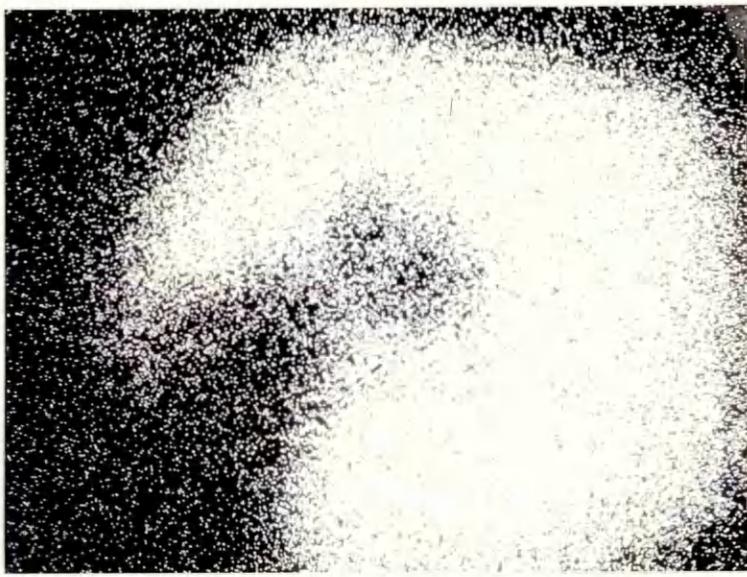
- (a) Manganese
- (b) Sulphur
- (c) Titanium

Show the inclusion to be basically MnS with a complex titanium inclusion at the centre. This complex is both titanium sulphide and possibly titanium carbonitride, cyanonitride or carbosulphide.

(a)



(b)



(c)

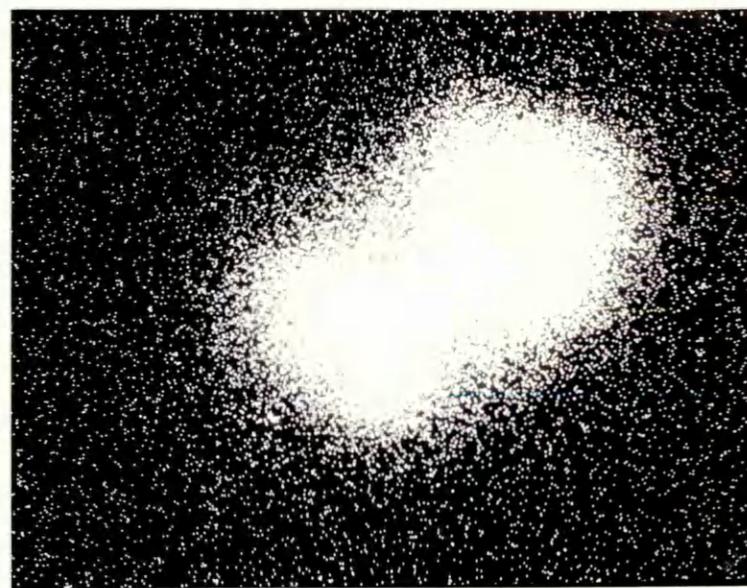


PLATE 195

Inclusion B from Plate 193. X 4160



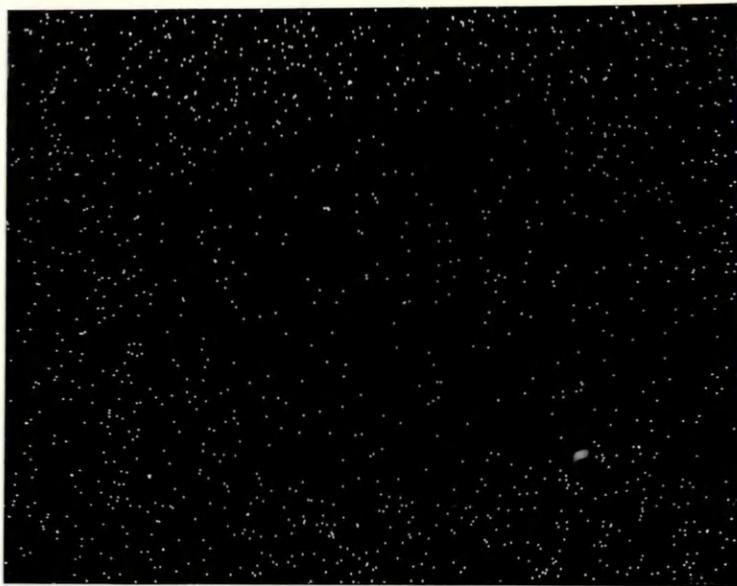
EDAX Scans for

(a) Manganese

(b) Sulphur

(c) Titanium

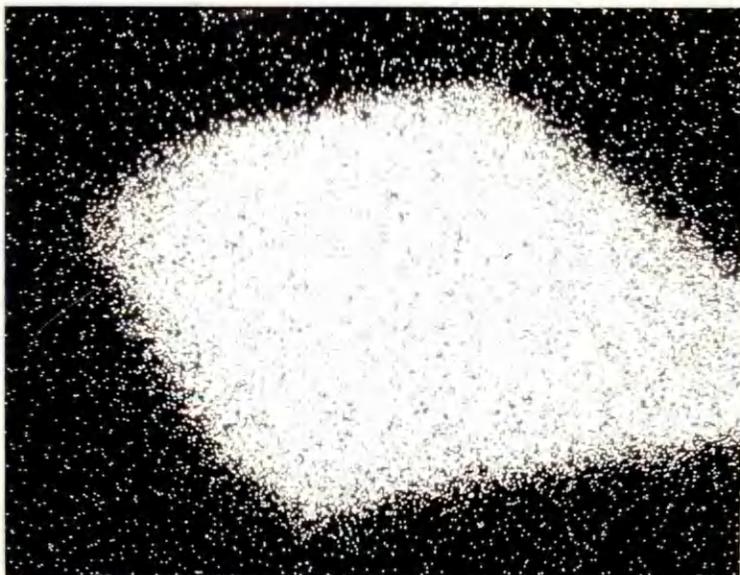
Confirm that Inclusion B is titanium sulphide of the Ti_2S configuration.



(a)



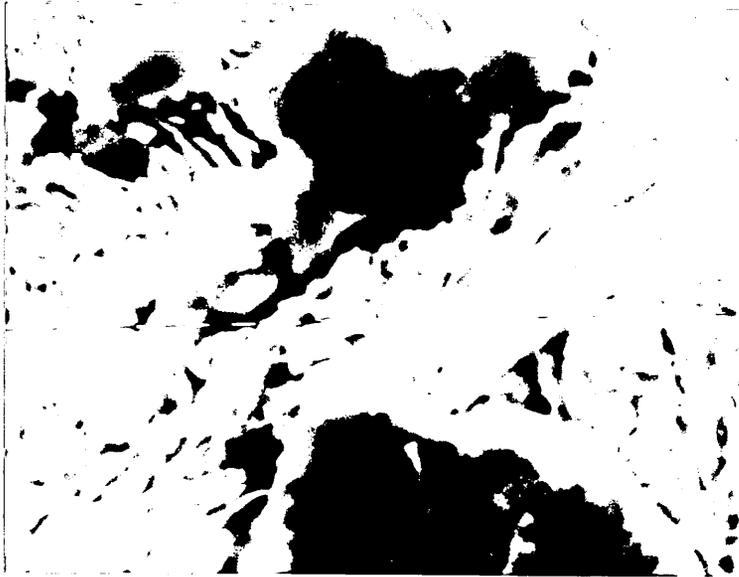
(b)



(c)

PLATE 196

G3 152.4mm - 177.8mm X 8320



EDAX scans for:

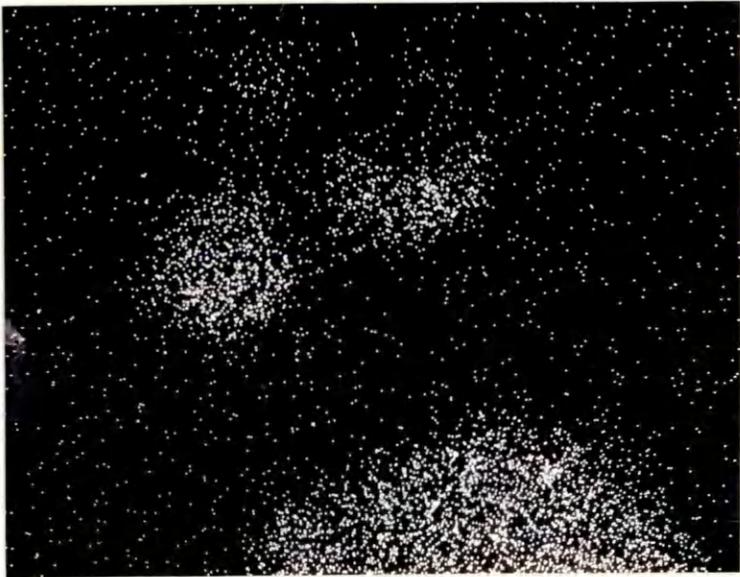
- (a) Manganese
- (b) Sulphur
- (c) Titanium

Show three MnS, one duplexed (TiMn)S and the rest complex titanium inclusions, in a pearlitic matrix.

(a)



(b)

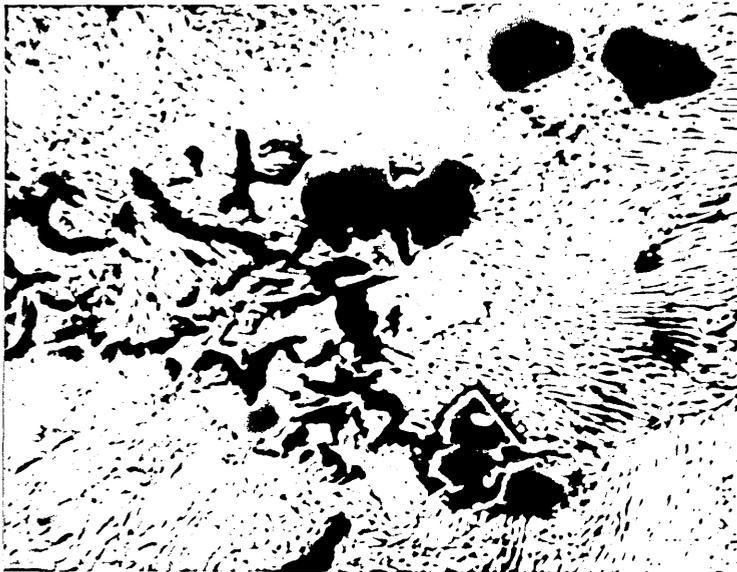


(c)



PLATE 197

G3 152.4mm - 177.8mm. X 480



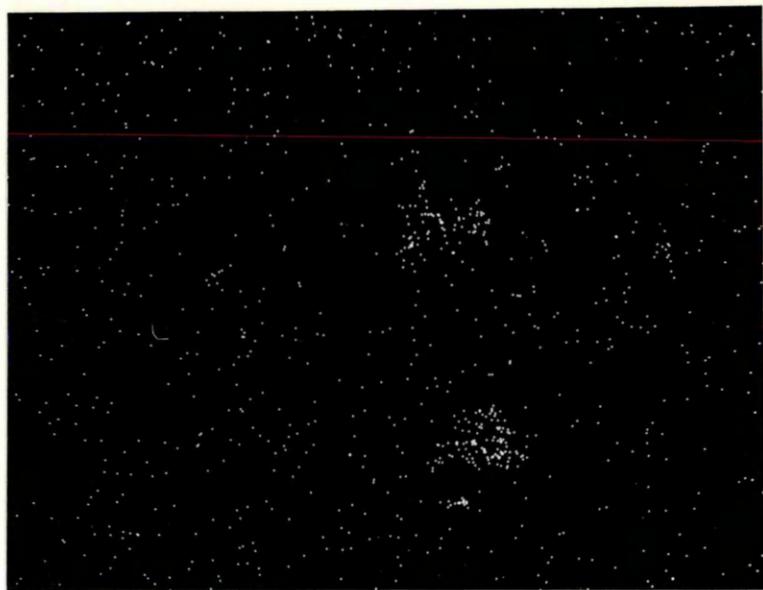
EDAX Scans for

(a) Manganese

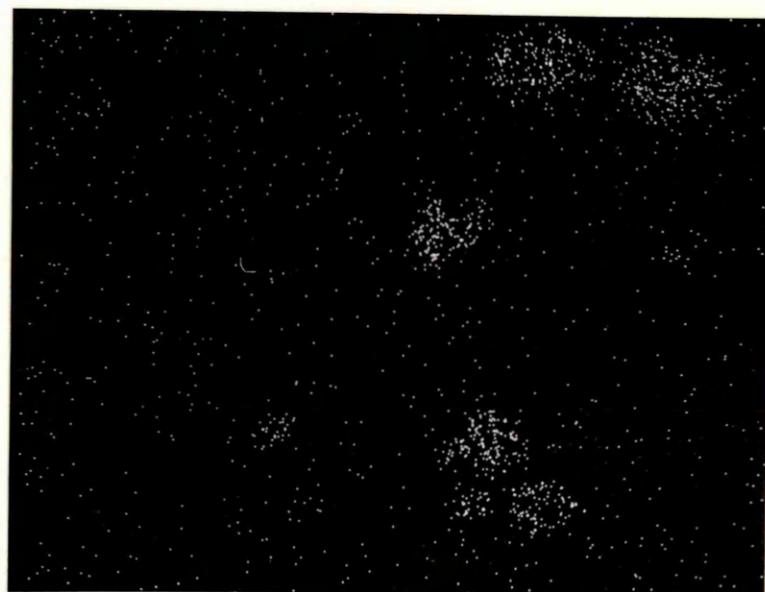
(b) Sulphur

(c) Titanium

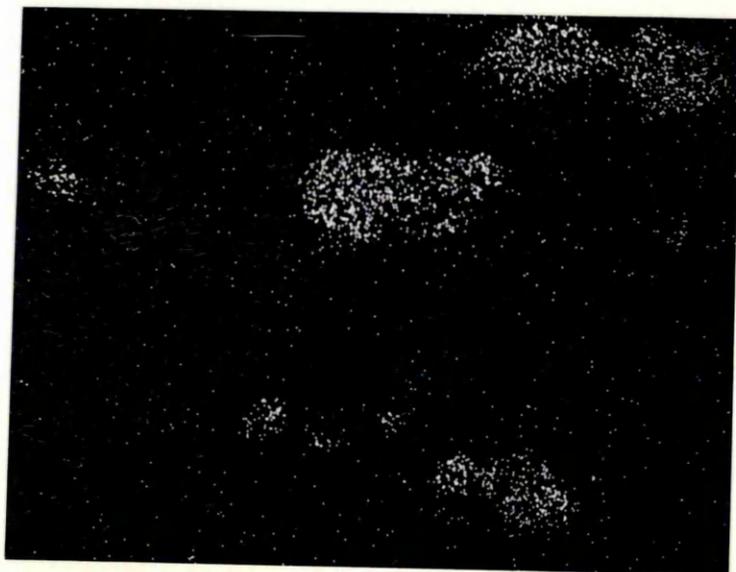
Show one MnS, one duplexed (MnTi)S, four Ti₂S and complex titanium inclusions in pearlite and associated with graphite.



(a)



(b)



(c)

PLATE 198

G3 152.4mm - 177.8mm. X2080



EDAX Scans for

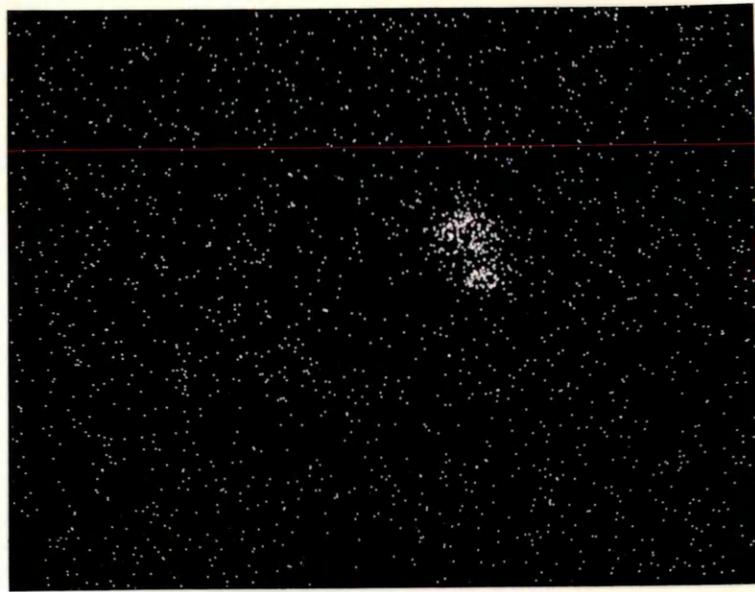
(a) Manganese

(b) Sulphur

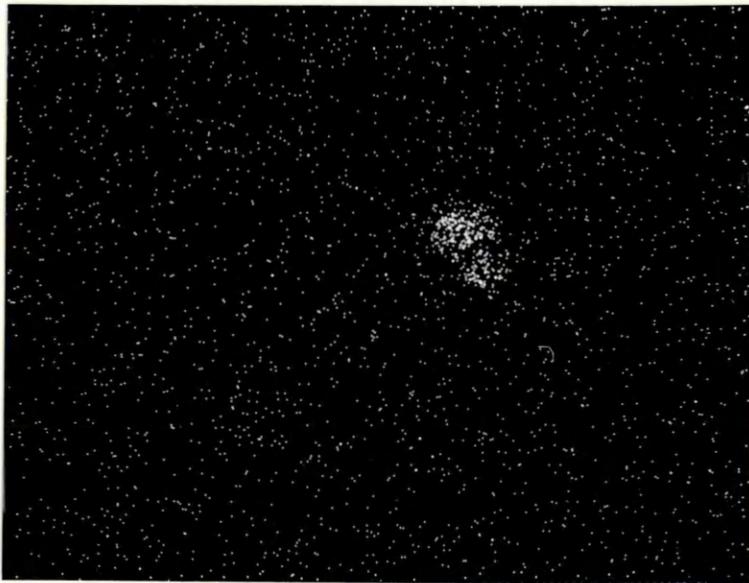
(c) Titanium

Show one MnS and seven complex titanium inclusions in a pearlitic matrix.

(a)



(b)



(c)

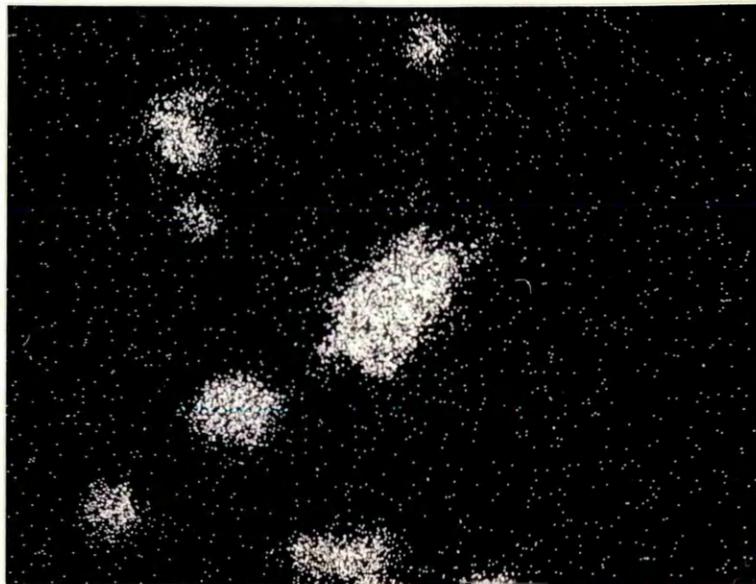
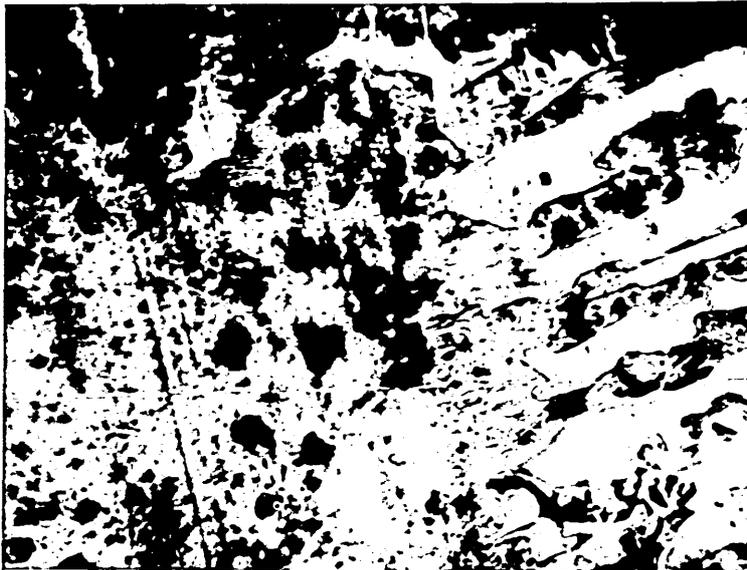


PLATE 199

F3' 177.8mm

X 520



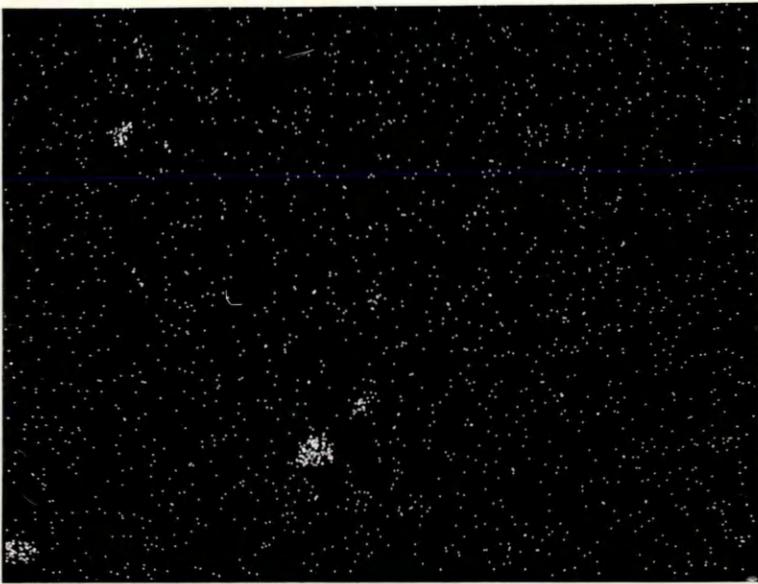
EDAX Scans for

(a) Manganese

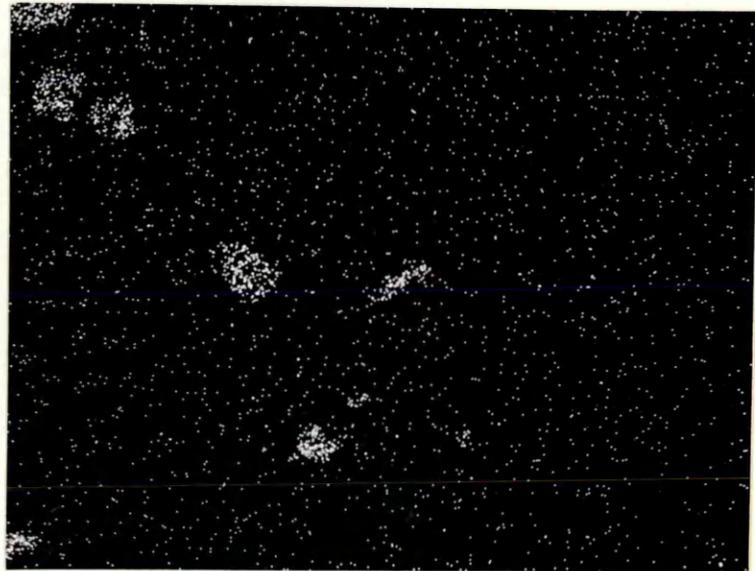
(b) Sulphur

(c) Titanium

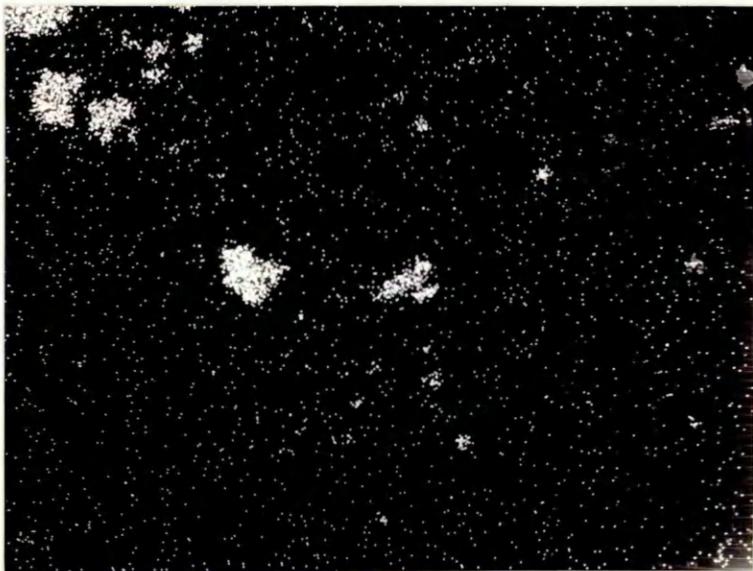
Show five Ti_2S , two duplexed $(MnTi)S$, one MnS and complex titanium inclusions in both pearlite and cementite with some graphite.



(a)



(b)



(c)

PLATE 200

F3' 163mm. X 520

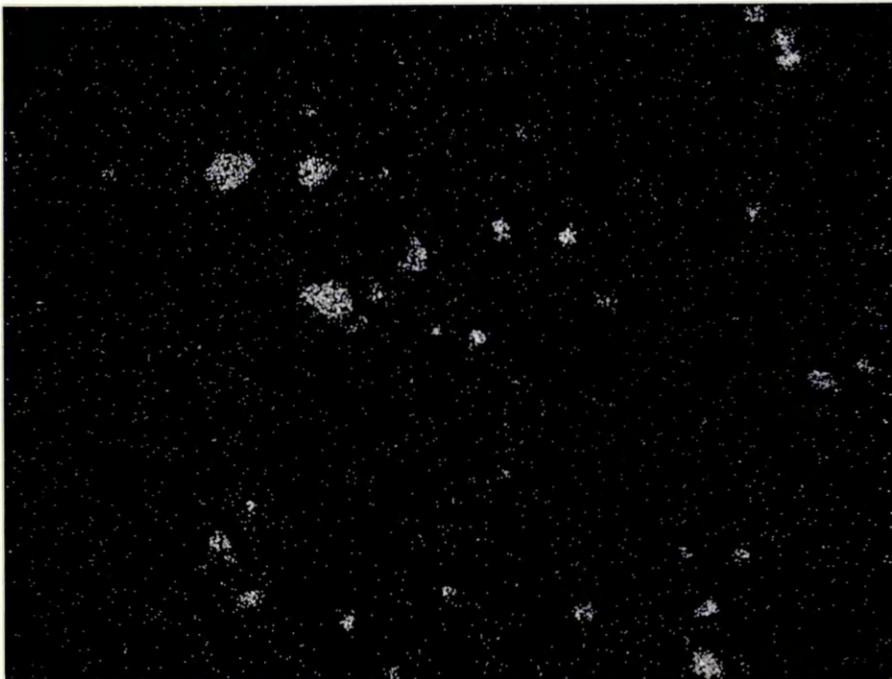
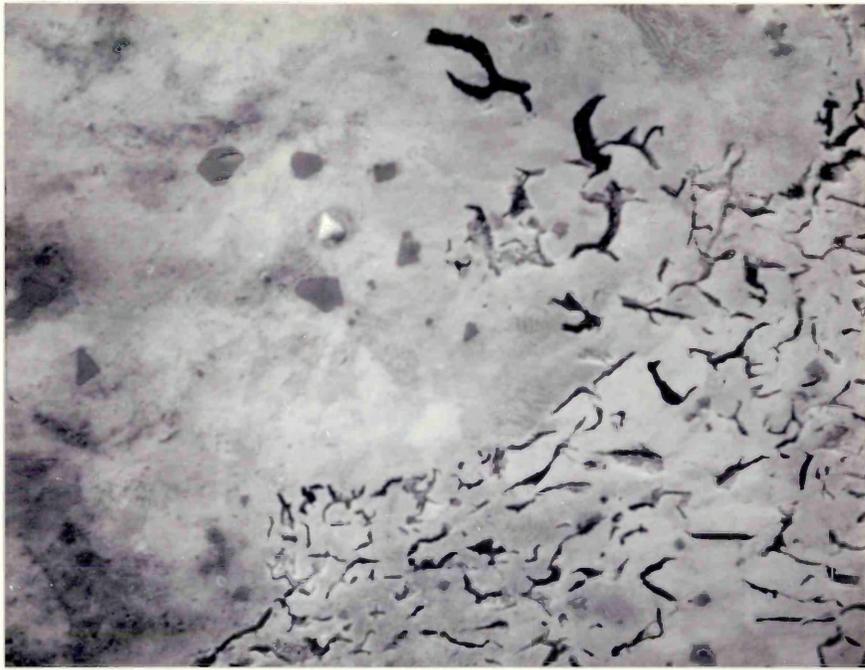
EDAX Scans for

(a) Manganese

(b) Sulphur

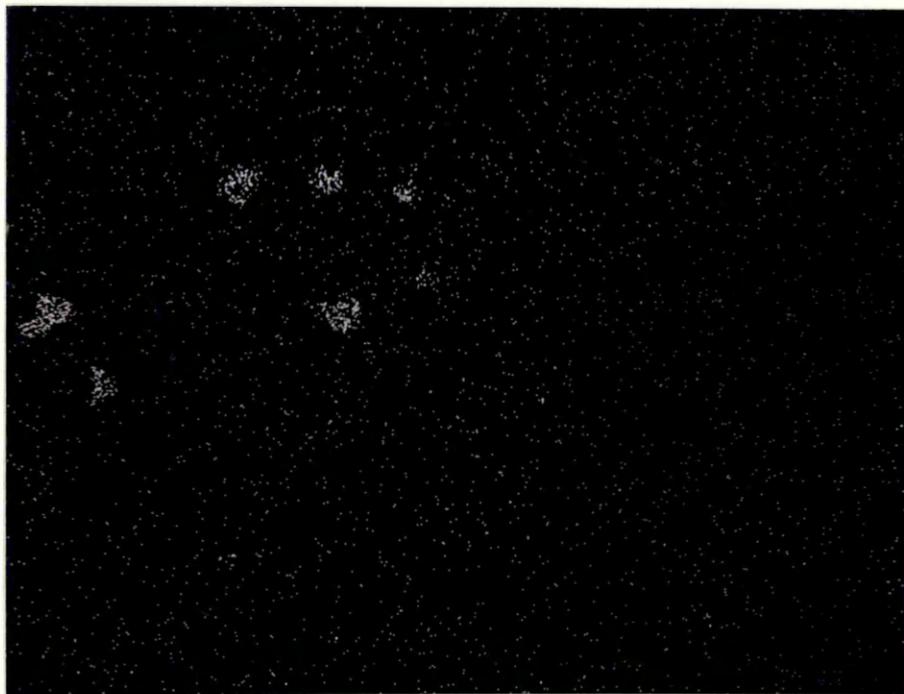
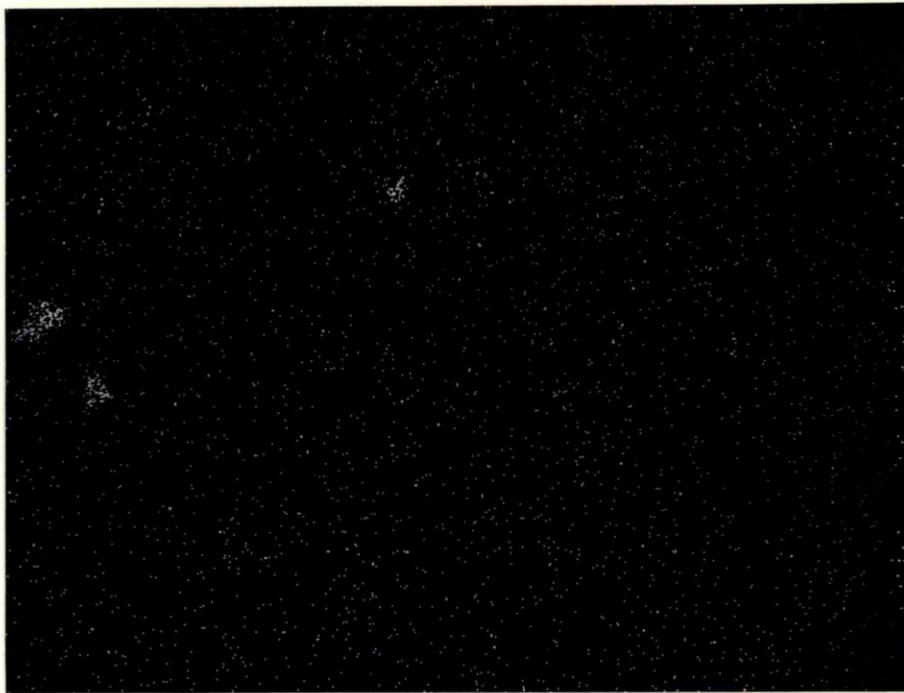
(c) Titanium

Show three MnS, four Ti_2S and thirty one complex titanium inclusions in a pearlitic matrix with 'D' type and a few compacted graphite flakes in the interdendritic spaces.



(c)

(a)



(b)

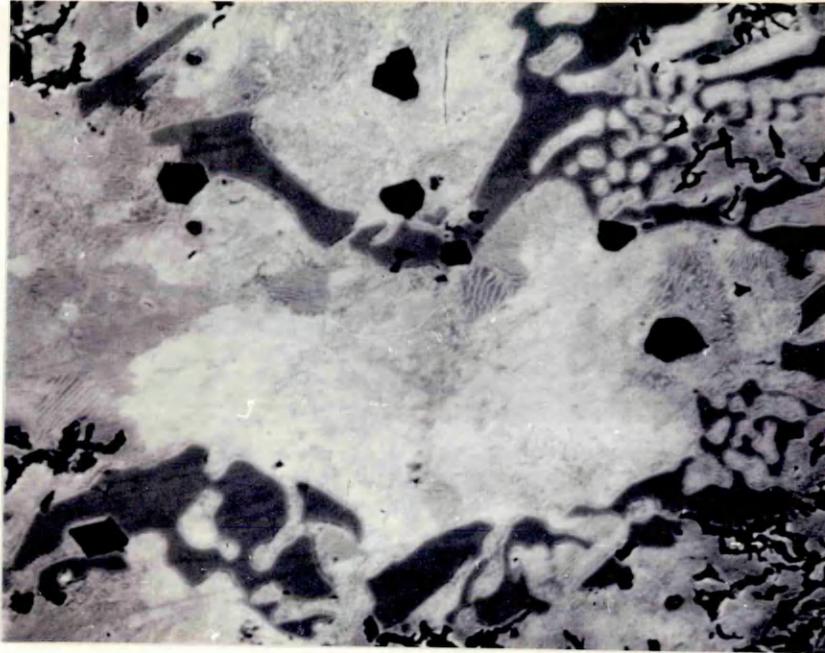
PLATE 201

F3' 163mm. X520

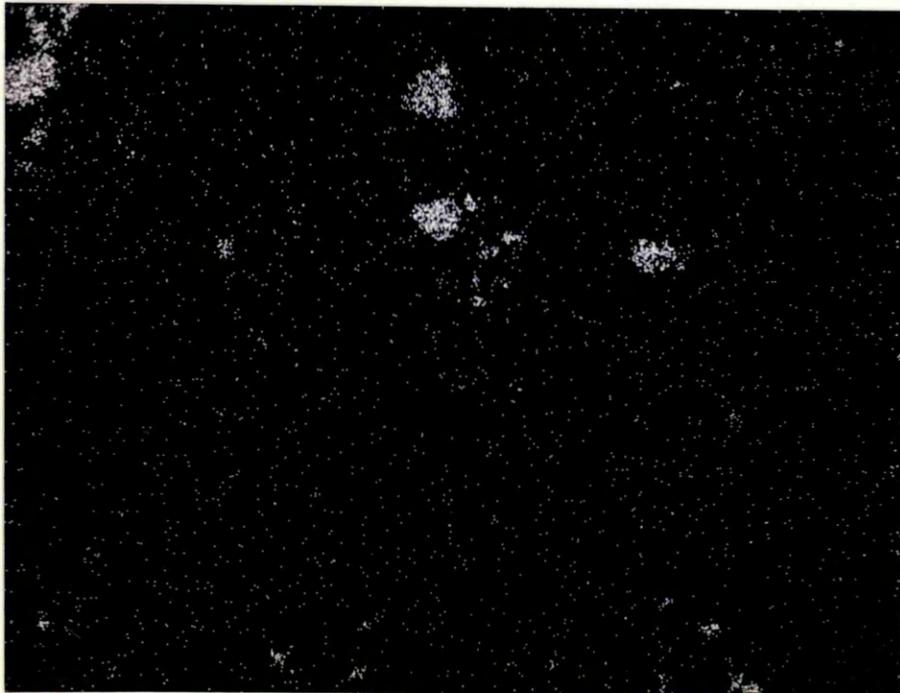
EDAX Scans for

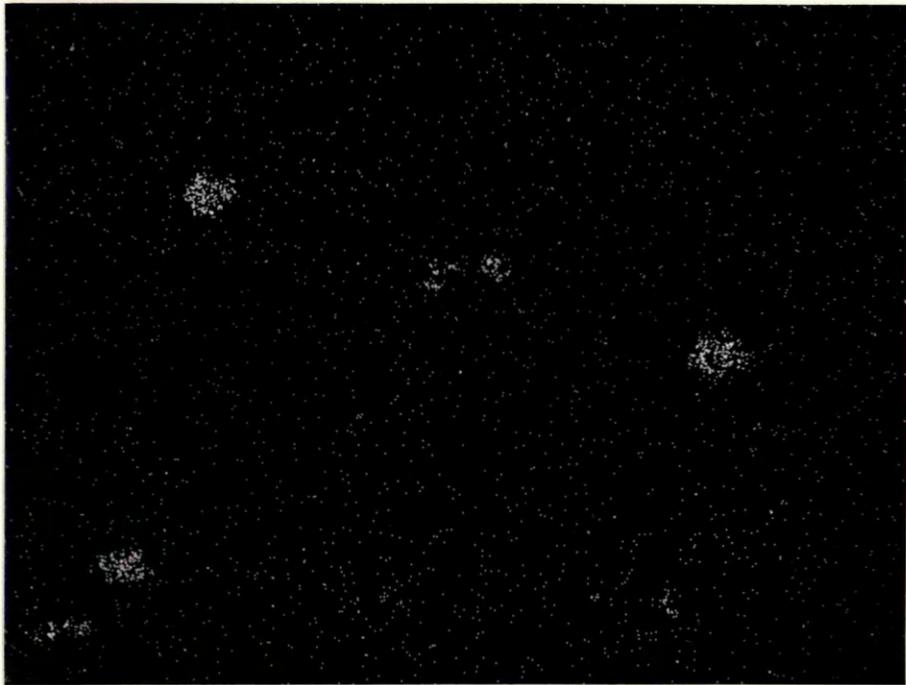
- (a) Manganese
- (b) Sulphur
- (c) Titanium

Shows seven MnS, four Ti_2S , two duplexed (TiMn)S and thirteen complex titanium inclusions in a ledeburitic matrix with 'D' type streamer graphite. The inclusions are mainly in the pearlite but some are visible in the cementite. None appear to be associated with the graphite.

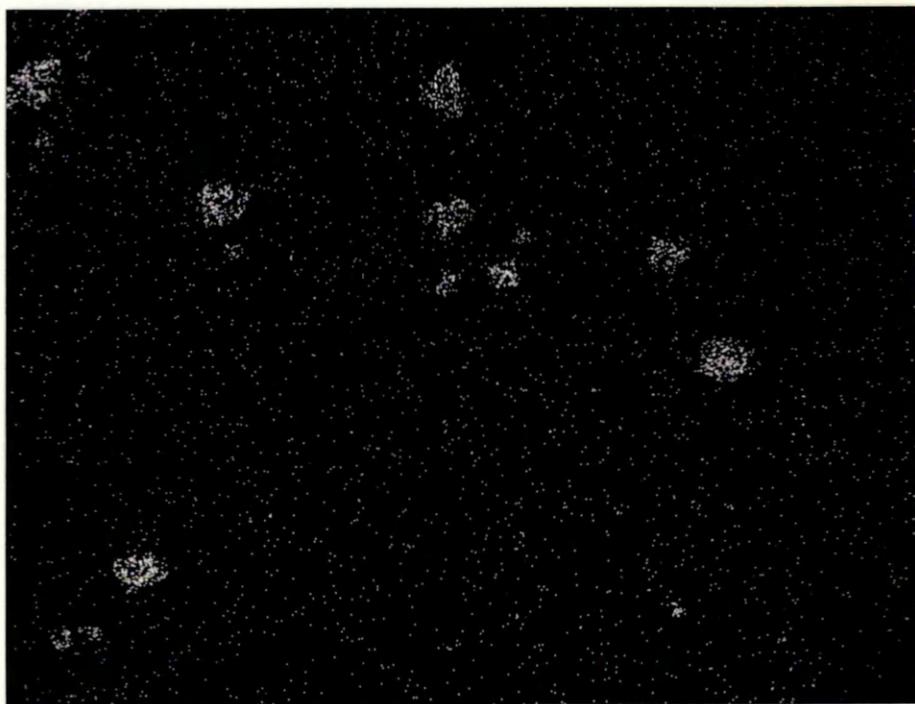


(c)





(a)



(b)

PLATE 202

F3' 127.1mm X 1040

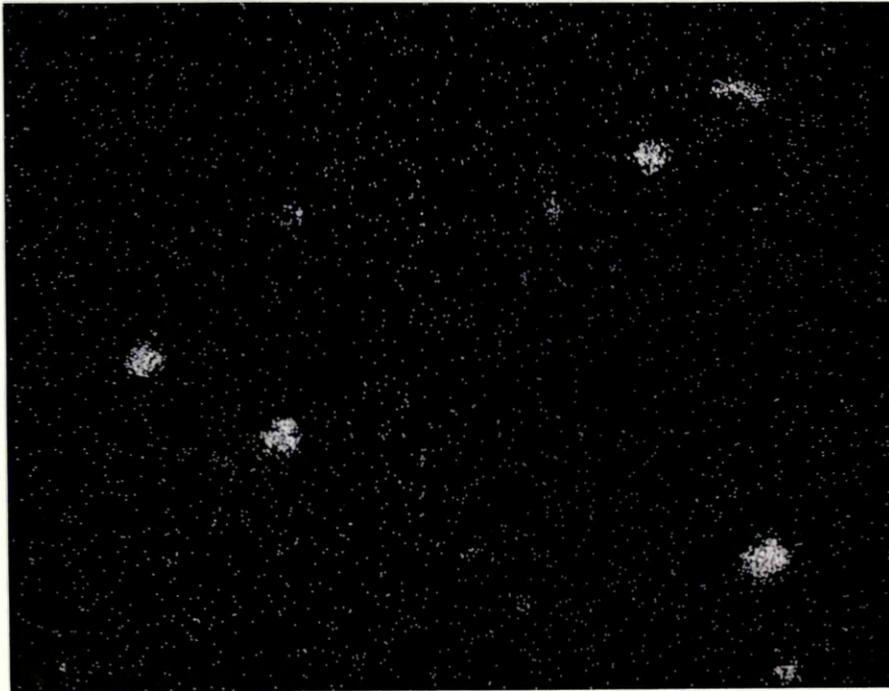
EDAX scans for:

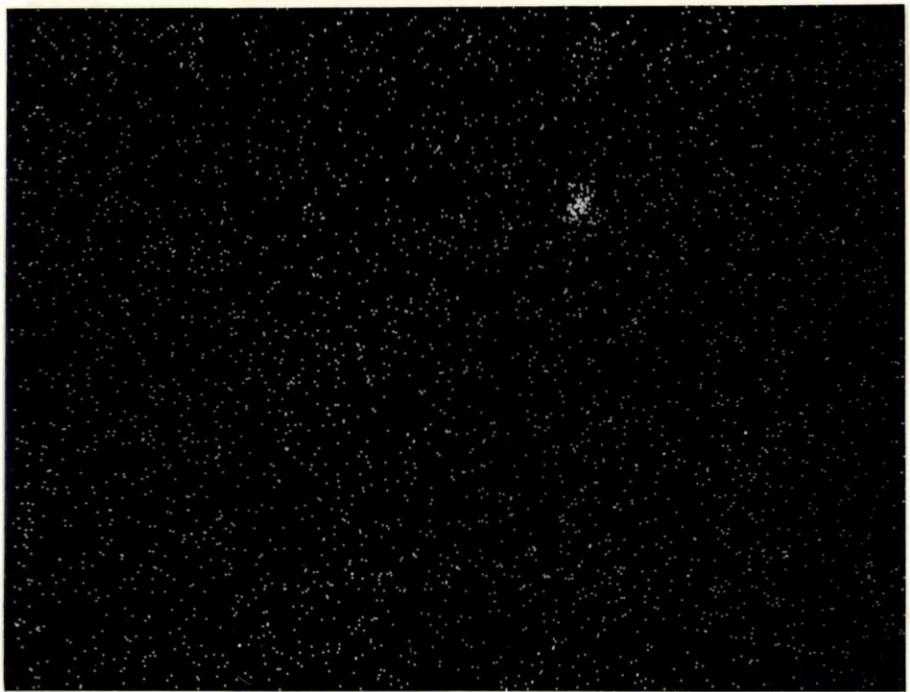
- (a) Manganese
- (b) Sulphur
- (c) Titanium

Show one MnS and ten complex titanium inclusions both in a cementite and a pearlite matrix.

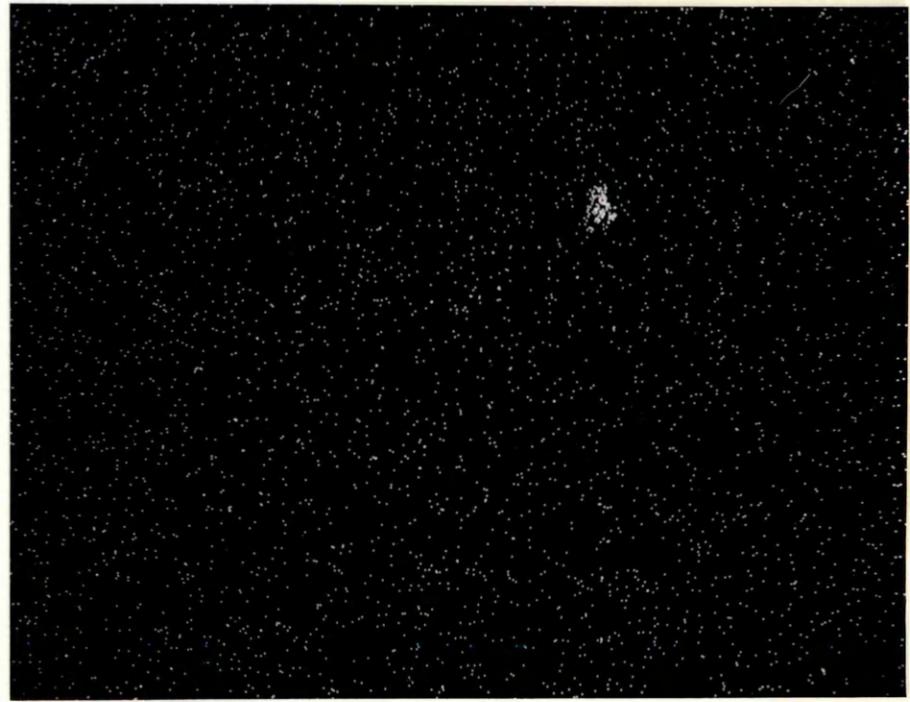


(c)





(a)



(b)



PLATE 203

B1' 166mm. X130

This shows Ti_2S , MnS and complex titanium inclusions and represents the overall area of which a specific, central area is shown in Plate 204.

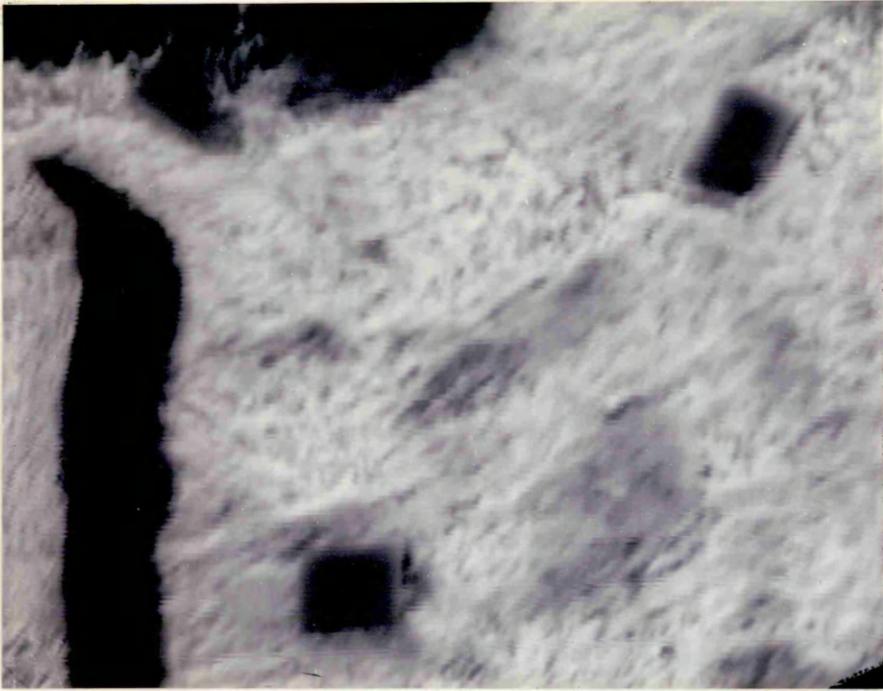
-175-
PLATE 204

Enlargement of a central region in
Plate 203. X 2080

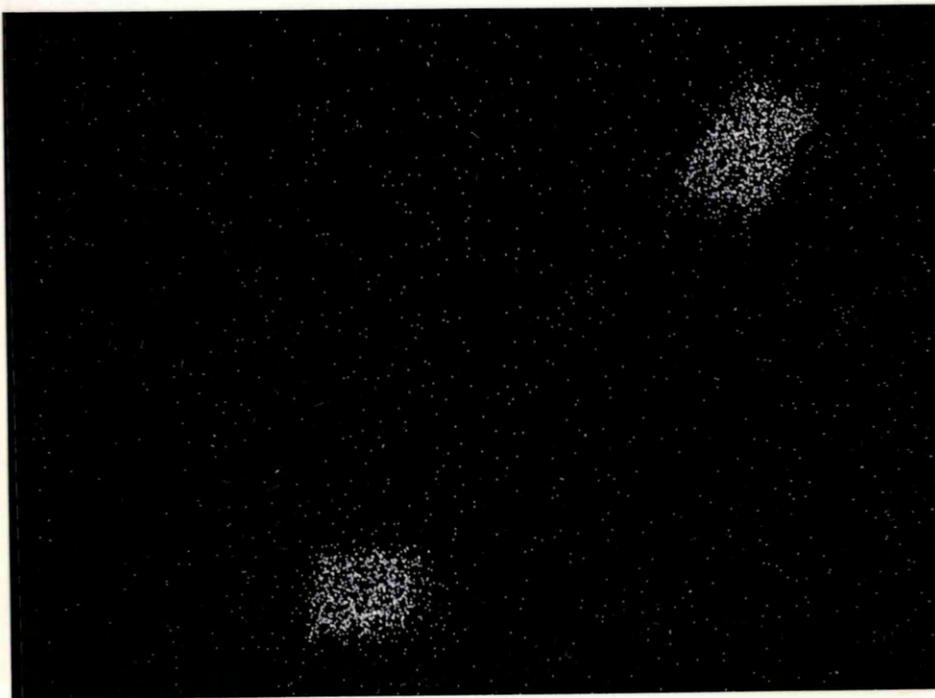
EDAX Scans for

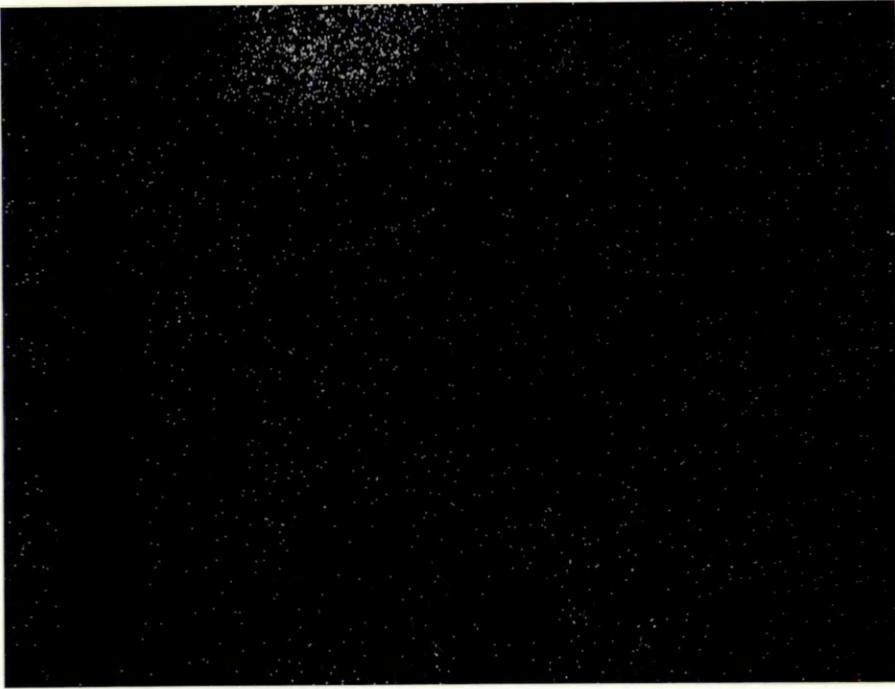
- (a) Manganese
- (b) Sulphur
- (c) Titanium

Show one MnS and two complex titanium
inclusions in a pearlitic matrix.

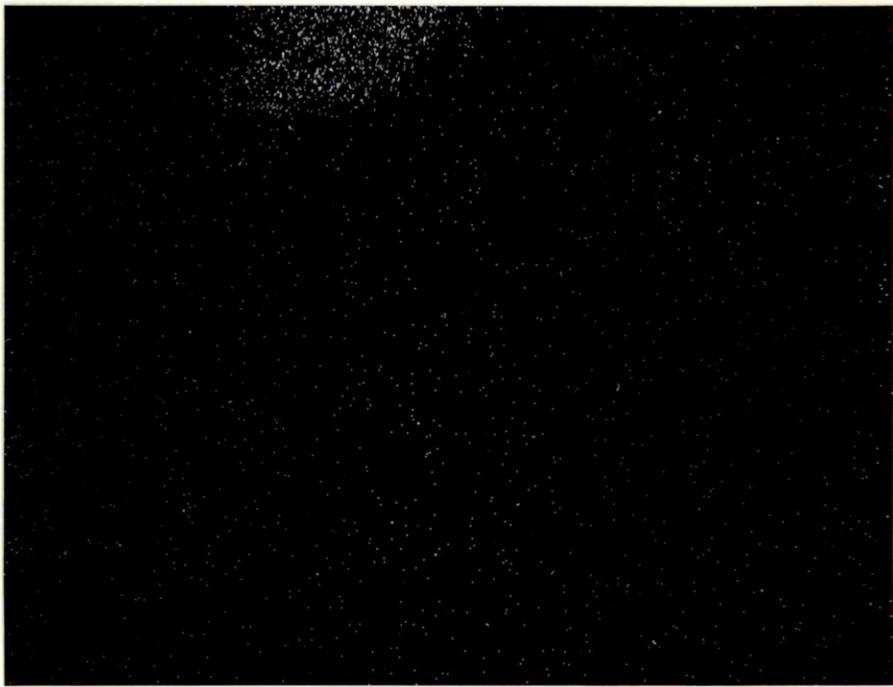


(c)





(a)



(b)

MICROSTRUCTURAL CRITERIA GIVEN IN TABLE 20

FOR THE 1160-1100°C TEMPERATURE RANGE

Sulphur Level	Cast Groups					
	A	B	C	E	F	G
1	123.97	123.97	47.86	25.62	25.62	25.62
2	123.97	48.10	48.10	25.62	25.62	48.10
3	43.65	25.62	46.24	38.02	123.97	40.74

Table 23a Streamer Graphite Start

Sulphur Level	Cast Groups					
	A	B	C	E	F	G
1	48.10	25.62	32.36	21.88	12.33	10.96
2	48.10	18.84	25.62	11.22	11.75	25.62
3	12.33	12.33	25.62	12.33	18.20	18.20

Table 23b 'Grey' Start

Sulphur Level	Cast Groups					
	A	B	C	E	F	G
1	12.33	12.16	9.79	6.28	6.28	5.89
2	12.33	10.96	12.33	5.69	7.03	6.28
3	11.22	7.85	9.55	6.28	6.28	6.28

Table 23c Graphitic Eutectic Cell Start

MICROSTRUCTURAL CRITERIA IN TABLE 22 FOR THE1160-1100°C TEMPERATURE RANGE

Sulphur Level	Cast Group				
	A'	B'	C'	D'	F'
1	48.10	25.62	92.26	95.50	25.62
2	48.10	48.10	123.97	-	25.62
3	40.74	100.00	63.10	48.10	41.69

Table 25a 'Streamer' Graphite Start

Sulphur Level	Cast Group				
	A'	B'	C'	D'	F'
1	23.99	9.79	25.62	25.12	-
2	22.91	25.62	25.62	-	-
3	12.33	25.62	25.62	15.14	6.17

Table 25b 'Grey' Start

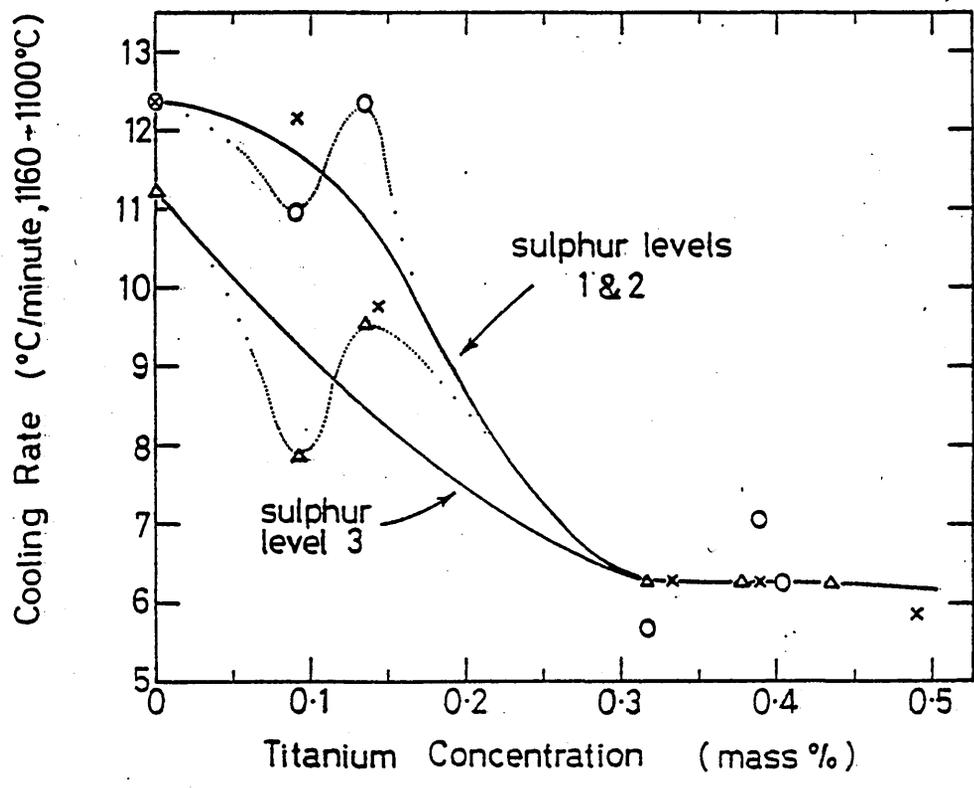
Sulphur Level	Cast Group				
	A'	B'	C'	D'	F'
1	9.79	8.00	12.33	9.79	6.28
2	9.79	12.33	12.33	-	7.94
3	6.28	9.79	9.44	9.79	6.17

Table 25c Graphitic Eutectic Cell Start

Figure 63 : the effect of titanium concentration on the maximum cooling rate for the formation of graphitic eutectic cells.

Sulphur Concentration :-
 x : level 1
 o : level 2
 Δ : level 3

(a) 'Low' nitrogen castings :



(b) 'High' nitrogen castings :

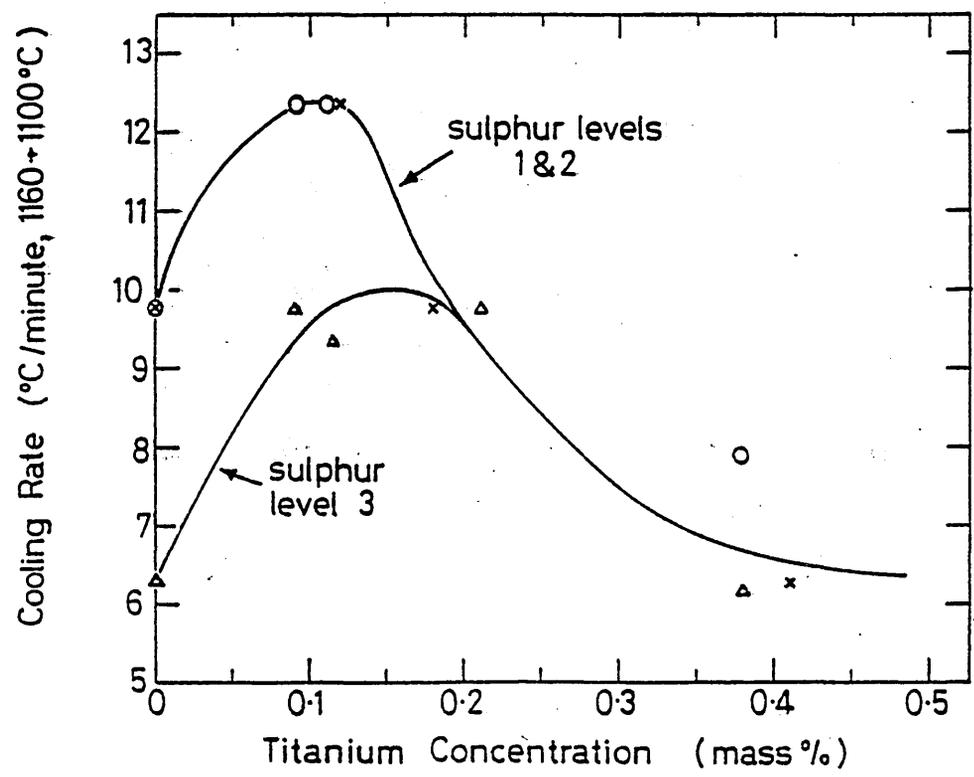
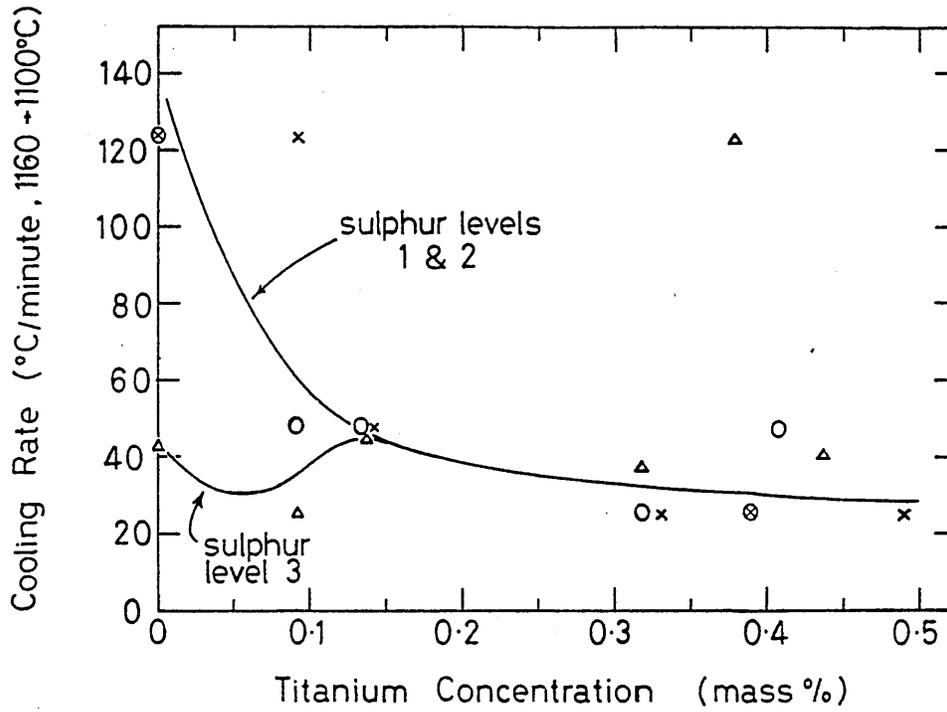


Figure 64 : The effect of titanium concentration on the maximum cooling rate for the formation of streamer graphite .

Sulphur Concentration :-
 x : level 1
 o : level 2
 Δ : level 3

(a) 'Low' nitrogen castings :



(b) 'High' nitrogen castings :

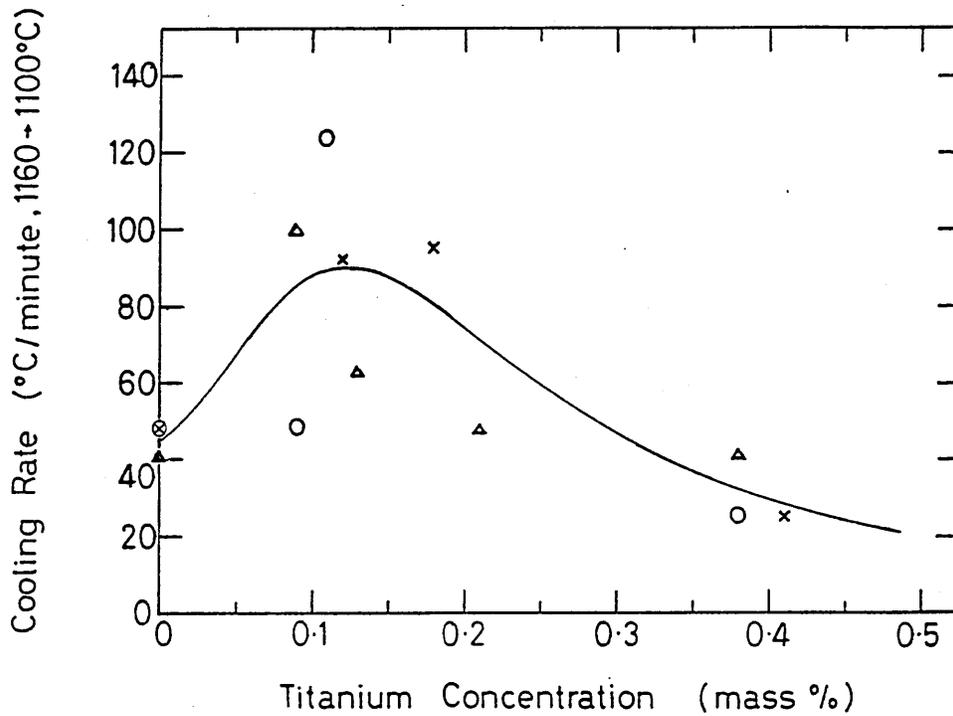
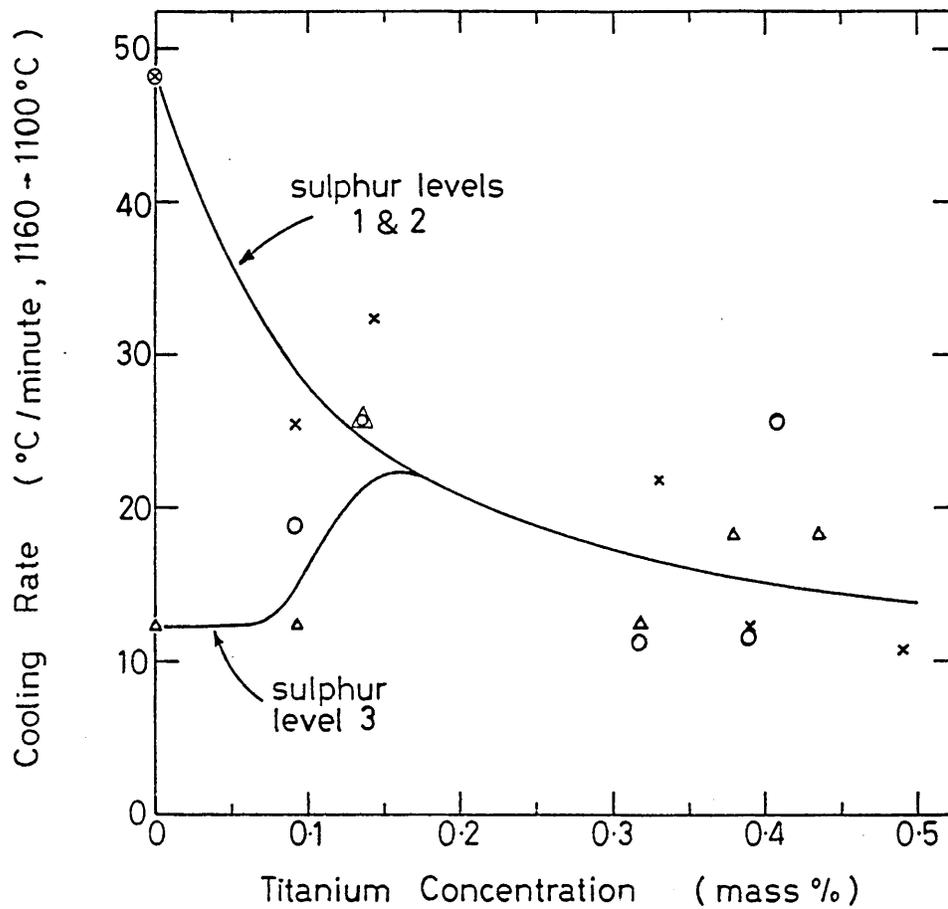


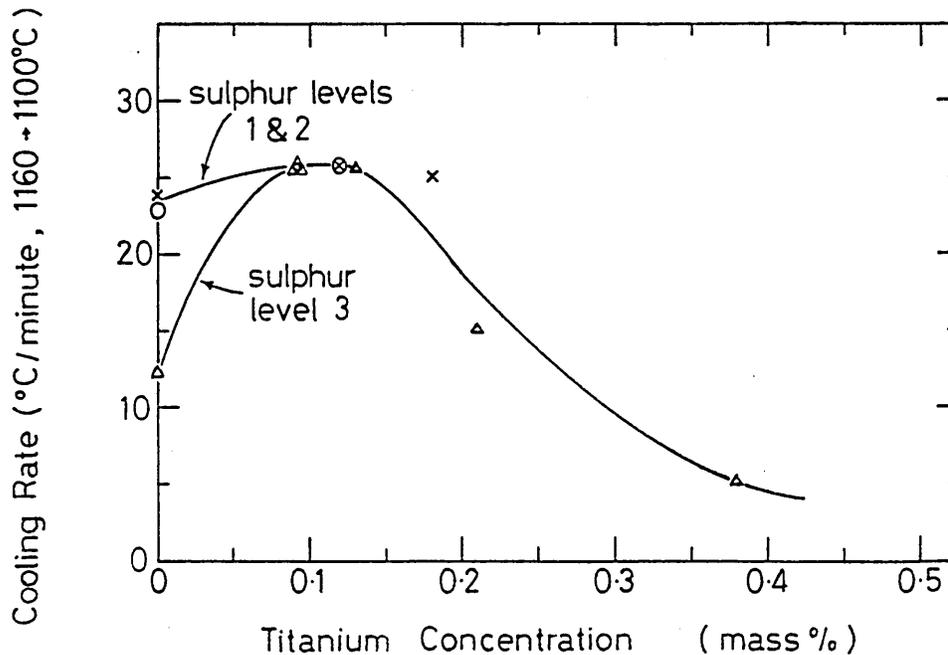
Figure 65 : The effect of titanium concentration on the maximum cooling rate for the 'grey' start.

Sulphur Concentration :-
 x : level 1
 o : level 2
 Δ : level 3

(a) 'Low' nitrogen castings :



(b) 'High' nitrogen castings :



EQUIVALENT COOLING RATES (°C/Min) FOR THE MICROSTRUCTURAL
CRITERIA FOR THE ADDITIONAL CASTS IN TABLE 21 FOR THE
1160-1100°C TEMPERATURE RANGE

Criteria	Ala	Alb	Alc	E1a	E3a	F2a
a) Streamer Start	91.20	123.97 48.1	-	123.97	12.33	48.10
b) 'Grey' Start	16.03	72.44	-	12.33	4.43	16.98
c) Graphitic Cell Start	11.48	18.16	-	6.28	-	8.433
d) Graphite Type at 177.8mm	Pred D/A	Pred D/A	Large A	D & Deg	D&Deg	D

Table 27a Low Nitrogen Additional Casts

Criteria	Ala'	B3a'	C2a'
(a) Streamer Start	48.1	48.1	123.97
(b) 'Grey' Start	25.62	12.33	25.62
(c) Cell Start	4.43	6.427	6.28
(d) Graphite Type at 177.8mm	A/V.little D	A/V.little D	Fine A/Deg.D

Table 27b High Nitrogen Additional Casts

Figure 66 : The manganese-sulphur equilibria for the liquid ingot mould cast iron, from Appendix 2.

