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**Temperature Dependent Piezoelectric Properties of Lead-Free (1-x)K\(_{0.6}\)Na\(_{0.4}\)NbO\(_3\)–xBiFeO\(_3\) Ceramics**

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(1-x)K\(_{0.4}\)Na\(_{0.6}\)NbO\(_3\)–xBiFeO\(_3\) lead-free piezoelectric ceramics were successfully prepared in a single perovskite phase using the conventional solid-state synthesis. Relative permittivity (\(\varepsilon_r\)) as a function of temperature indicated that small additions of BiFeO\(_3\) not only broadened and lowered the cubic to tetragonal phase transition (\(T_C\)) but also shifted the tetragonal to orthorhombic phase transition (\(T_{O-T}\)) toward room temperature (RT). Ceramics with \(x = 1\) mol.% showed optimum properties with small and large signal piezoelectric coefficient, \(d_{33} = 182\) pC/N and \(d^*_{33} = 250\) pm/V, respectively, electromechanical coupling coefficient, \(k_p = 50\%\), and \(T_C = 355\,^\circ\)C. \(k_p\) varied by \(\sim 5\%\) from RT to 90\,°C, while \(d^*_{33}\) showed a variation of \(\sim 15\%\) from RT to 75°C, indicating that piezoelectric properties were stable with temperature in the orthorhombic phase field. However, above the onset of \(T_{O-T}\), the properties monotonically degraded in the tetragonal phase field as \(T_C\) was approached.

Keywords: piezoelectrics, lead free, K\(_{0.5}\)Na\(_{0.5}\)NbO\(_3\), temperature dependence, BiFeO\(_3\)

**INTRODUCTION**

Piezoelectric materials are essential in many applications and used in different electronic circuits as a sensor, actuator, or a transducer (Holtermann and Groen, 2013). Commercial piezoelectric materials contain about 60% of PbO by weight. The toxicity of lead is well documented and legislation against its use are becoming more stricter with time, which has increased interest in lead–free alternatives for piezoelectric applications (Rödel et al., 2015). Amongst the potentially useful lead-free piezoelectrics, only Ca\(^{2+}\) and Zr\(^{4+}\) modified BaTiO\(_3\) and (Na,K)NbO\(_3\)-based ceramics have low coercive fields similar to lead zirconate titanate (PZT). However, BaTiO\(_3\)-based piezoelectric ceramics generally exhibit a low Curie temperature (\(T_C < 100\,^\circ\)C), making them unsuitable for high temperature piezoelectric applications (Liu and Ren, 2009). (K,Na)NbO\(_3\) has a high Curie temperature of \(>350\,^\circ\)C and capable of operating at low drive fields. Compositional engineering of K\(_{1-x}\)Na\(_x\)NbO\(_3\) is usually carried out around \(x = 0.5\), i.e., part of the phase diagram where several various polymorphs have similar free energies. On cooling ceramics with \(x = 0.5\), the crystal structure successively changes from cubic to tetragonal, tetragonal to orthorhombic,
and orthorhombic to rhombohedral. Almost all compositions with large piezoelectric (d_{33}) and coupling coefficients (k_p) are optimized by substituents/dopants that shift the orthorhombic-tetragonal transition (T_{O-T}) toward room temperature (RT; Wu et al., 2015; Hussain et al., 2019). Recently new phase boundaries have been constructed in (K,Na)NbO_3 based ceramics by simultaneously moving the rhombohedral and tetragonal phases toward RT. Such a coexistence of rhombohedral-orthorhombic-tetragonal phase boundaries has been very successful in improving the d_{33} values and have significantly improved the temperature stability in these ceramics (Tao et al., 2019; Lv et al., 2020; Zheng et al., 2020). Although ceramics with x = 0.5 are most commonly investigated, piezoelectric properties are optimized in K_{1-x}Na_xNbO_3 for 0.4 ≤ x ≤ 0.6. The piezoelectric properties are similar throughout this compositional range but for compositions with x = 0.6 (Na⁺ rich) have lower T_{O-T} in comparison to x = 0.5 (Wu et al., 2008; Tellier et al., 2009).

BiFeO_3 is one of the most extensively investigated perovskite compounds because of its RT multiferroic properties (Khesro et al., 2016a). It is rarely, however, (Sun et al., 2008; Zuo et al., 2010) investigated in solid solution with (K,Na)NbO_3. BiFeO_3 could be an interesting choice for solid solution with KNN because of its relatively low melting point. Its ability to form a liquid phase can help in densification of KNN based ceramics (Na et al., 2011) in addition to the possibility of forming a phase boundary at RT.

Since, BiFeO_3 was expected to have only limited solid solubility (Jiang et al., 2010), K_{0.4}Na_{0.6}NbO_3 was chosen to increase the prospect of bringing the T_{O-T} closer to RT. Moreover, K⁺ rich compositions are prone to volatilization and are thus more difficult to process with precise stoichiometry (Wang et al., 2016). Therefore, in the present study, the dielectric, ferroelectric and piezoelectric properties of the solid solution (1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3 are studied. In situ measurements of the piezoelectricity were performed to verify the temperature stability of these ceramics.

**EXPERIMENTAL METHODS**

(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3 for x = (0, 0.5, 0.75, 1, 1.25, 1.5, 2, and 3) mol.% ceramics were prepared via a mixed oxide solid state route using K_2CO_3, Na_2CO_3, Bi_2O_3, Fe_2O_3, and Nb_2O_5 raw materials. K_2CO_3 and Na_2CO_3 were dried at 300°C, Bi_2O_3, and Fe_2O_3 were dried at 500°C and Nb_2O_5 was dried at 900°C. Raw materials were weighted according to the molar ratios of the compositions and mixed/milled for 1 h in an attrition mill using 3 mm diameter yttria-stabilized zirconia media in isopropanol. Powders were dried in an oven at 80°C, sieved, and calcined in a covered alumina crucible at 850°C for 6 h. The calcined powders were remilled, dried and sieved. Polyvinyl alcohol (PVA) binder solution was added and the powders were pressed into 10 mm diameter pellets using a uniaxial pellet press. After binder burnt out at 550°C, pellets were sintered in the temperature range 1100 to 1140°C for 6 h, at a heating/cooling rate of 5°C/min. Densities of the sintered pellets were measured using Mettler Toledo model MS104S digital densitometer.

Ceramics with x = 0.5, 0.75, and 1 mol.% showed a relative density >94% while the remaining samples ranged between 88–90%. Phase analysis of the sintered specimens was carried out using a Bruker D2-Phaser X-ray powder diffractometer (XRD). The microstructure of the samples was examined using a FEI Inspect-F scanning electron microscope (SEM). For electrical measurements, sintered samples were electrode with silver. Samples were poled at RT in silicone oil with at an applied field of 30–40 kV/cm. The small signal piezoelectric coefficient (d_{33}) was measured using a Piezotest PM300 d_{33} meter. Polarization hysteresis and strain-electric field measurements were carried out using an aixACCT TF 2000 ferroelectric tester at a frequency of 1 Hz from RT to 150°C, where the displacement data was synchronously captured by a laser interferometer. Relative permittivity (ε_r) and tan δ data was measured from RT to 500°C using an Agilent 4184A multifrequency precision LCR meter. The planar electromechanical coupling factor (k_p) was determined from the resonance and antiresonance frequencies peaks, which were measured using an Agilent 4294A impedance/gain-phase analyzer according to IEEE standards on piezoelectricity (American and Standard, 1988).

**RESULTS AND DISCUSSION**

Figure 1 shows RT XRD patterns of sintered (1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3 (x = 0–3 mol.%) ceramics. Traces were indexed according to a single perovskite phase with no secondary peaks. For K_{0.5}Na_{0.5}NbO_3-based ceramics, the (200) doublet peak is usually considered to define the structure. For orthorhombic structure, I_{002}/I_{020} = 2:1 (I = intensity; Feng et al., 2016) but for the tetragonal structure, an opposite trend is observed, having I_{002}/I_{020} = 1:2 (Zhou et al., 2015). In our samples at x = 0, obvious split of the 200 peak was detected at 20 ∼ 46° which is consistent with the orthorhombic phase frequently reported for K_{0.5}Na_{0.5}NbO_3 ceramics (Sun et al., 2010).
et al., 2008). With increase in concentration of BiFeO$_3$, the splitting became less apparent, coupled with a decrease in the intensity’s ratios. At $x = 1.25$ mol.%, the peaks merged, indicating a co-existence of tetragonal, and orthorhombic phases. At $x = 1.5$ mol.%, a shoulder was observed on the left-hand side of the (200) peak but without the clear splitting expected from a tetragonal structure. At $x = 3$ mol.%, the structure appears to be pseudocubic, showing only one broad peak which may be ascribed to nanoscale competition between tetragonal and orthorhombic phases (Bomlai et al., 2007). To confirm the phase evolution of KNN-BF, full-pattern Rietveld refinement of XRD data was conducted using a two-phase mix of orthorhombic (Bmm2), and tetragonal KMO (P4mm) as given in Figure 2. With the increase of BF content, coexistence of two phases was found at $x = 1.25$ mol.%, and then the fraction of tetragonal phase gradually increased and dominated as shown in Table 1.

Figure 3 shows SEM micrographs of sintered (1-$x$)K$_{0.4}$Na$_{0.6}$NbO$_3$-$x$BiFeO$_3$ ($x = 1–3$ mol.%) ceramics which revealed that the average grain size decreases with increase in $x$. For samples with $x = 0$ and 0.5 mol.%, few grains indicated abnormal growth of ($> 5$ μm). Such abnormal grain growth is usually associated with liquid phase sintering (Jo et al., 2006; Song et al., 2007; Han et al., 2012). Each large grain observed is believed to be the combination of many small grains which self-assemble into a larger cluster. The sintering temperature of K$_{0.5}$Na$_{0.5}$NbO$_3$ is close to its melting-point and consequently it is not easy to achieve a dense ceramic without liquid phase sintering (Wang and Li, 2012). It has been reported (Zhen and Li, 2007; Kim et al., 2009) that grain size and core-shell structures in such grains influence piezoelectric properties. The BF content is affecting the sintering temperature, for larger contents of BF the conditions don’t favor formation of large cluster and the constituent grains are disintegrated, thereby showing smaller grains. This is evident from a sharp decrease at $x = 0.75$ mol.%. With further increase of BiFeO$_3$ the grain size gradually decreased to ∼100–400 nm for $x = 3$ mol.%.

![Figure 2](image-url) Rietveld refinement analysis of (1-$x$)K$_{0.4}$Na$_{0.6}$NbO$_3$-$x$BiFeO$_3$ ($x = 0, 1.25, 2, and 3$ mol.%) using the GSAS + EXPGUI package.

<table>
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<tr>
<th>Space group</th>
<th>Cell volume/Å$^3$</th>
<th>Density/g/cm$^3$</th>
<th>Lattice parameter</th>
<th>Phase fraction</th>
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<td></td>
<td></td>
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<td>b/Å</td>
<td>c/Å</td>
<td>O/%</td>
<td>T/%</td>
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<td>4.549 (4)</td>
<td>5.6300 (3)</td>
<td>3.9368 (2)</td>
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<td>125.8 (2)</td>
<td>4.539 (7)</td>
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<td>P4mm</td>
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<td>3.9504 (12)</td>
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<tr>
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FIGURE 3 | SEM images of as sintered ($1-x$)K$_{0.4}$Na$_{0.6}$NbO$_3$–xBiFeO$_3$ ($x = 1–3$ mol.%) ceramics. Where (a) shows $x = 0$; (b) shows $x = 0.5$ mol.%; (c) shows $x = 0.75$ mol.%; (d) shows $x = 1$ mol.%; (e) shows $x = 1.25$ mol.%; (f) shows $x = 1.5$ mol.%; (g) shows $x = 2$ mol.%; and (h) shows $x = 3$ mol.%

FIGURE 5 | $d_{33}$ and relative density as a function of composition in the system ($1-x$)K$_{0.4}$Na$_{0.6}$NbO$_3$–xBiFeO$_3$ ($x = 0–3$ mol.%).

$\varepsilon_r$ versus temperature for all ($1-x$)K$_{0.4}$Na$_{0.6}$NbO$_3$–xBiFeO$_3$ compositions are shown in Figure 4. At $x = 0$, $T_{O-T}$ was observed at $\sim 175^\circ$C, which is lower than that for Na$_{0.5}$K$_{0.5}$NbO$_3$ ceramics.

FIGURE 4 | Relative permittivity and tan $\delta$ as a function of temperature at constant frequencies of 1, 10, 100, 250 kHz, and 1 MHz for ($1-x$)K$_{0.4}$Na$_{0.6}$NbO$_3$–xBiFeO$_3$ ($x = 1–3$ mol.%) ceramics.
FIGURE 6 | P–E loop at room temperature for sample at x = 1.5 mol.%. (i.e., ∼200°C). $T_{O-T}$ decreased with increasing BiFeO$_3$ amount from ∼176°C ($x = 0$) to ∼107°C ($x = 1$ mol.%). For sample with $x = 1.25$ mol.%, $T_{O-T}$ is not sharp but diffused consistent with the overlapped peaks observed in XRD plot (Figure 1). As BiFeO$_3$ concentration increases, no anomaly associated with the $T_{O-T}$ is observed. It is expected that $T_{O-T}$ may have been shifted below RT and/or may have smeared out because of chemical heterogeneity. It is noted that the sharp peak observed for the tetragonal to cubic transition ($T_C$) in samples with $x \leq 1$ mol. % has also broadened for $x > 1$ mol. % in addition, samples with $x > 1$ mol. % showed smaller magnitude of $\varepsilon_r$ at peak maxima which is strongly frequency dependent. Low $\varepsilon_r$ is attributed to low density, but its frequency dependence is most evident in the range 1 to 10 kHz. Above 100 kHz, $\varepsilon_r$ is frequency independent. Such behavior indicates contributions from space charge polarization at lower frequencies due to ion migration which relax at > 1 kHz (Lingval et al., 2006). The contribution from space charge and increased with increase in $x$, which may be due to vaporization of volatile species such as Bi, Na, and K ions. A similar trend was observed in the dielectric loss versus temperature where high $\tan \delta$ was noticed at low frequencies. We also note that $\tan \delta$ (100 kHz) is less than 5% at RT but the sample with $x > 1$ mol.% exhibit greater loss as a function of temperature in comparison to samples with $x \leq 1$ mol.%. Higher losses at $x > 1$ mol.% can be attributed to low densification and/or volatility of A-site Cations. Moreover, BF itself is intrinsically very leaky and its larger contents may be resulting in higher conductions. Figure 5 shows $d_{33}$ for $(1-x)K_0.4Na_0.6NbO_3-xBiFeO_3$ ($x = 1$–3 mol.%) ceramics after DC poling at 40 kV/mm for 5 min. At $x = 0$, $d_{33} = 82$ pC/N was obtained which was similar to previously reported data (Egerton and Dillon, 1959; Jaeger and Egerton, 1962). $d_{33}$ increased with BiFeO$_3$ concentration and reached a maximum of ∼182 pC/N at $x = 1$ mol.%. The increase in $d_{33}$ may be due to a decrease in $T_{O-T}$ as noticed in dielectric data (Figure 4) and/or an increase of the density, whereas the sharp decrease in $d_{33}$ observed for $x > 1$ mol.% may be correlated to the significantly lower densities, as shown in Figure 5. In addition, high electrical conductivities in these samples are responsible for low $d_{33}$ values, as they inhibit poling and often result in electrical breakdown. $T_{O-T}$ is supposed to be at RT for $x = 1.25$–1.5 mol.% which should lead to higher $d_{33}$ values, provided that ceramics exhibiting higher resistivities, and densities can be successfully fabricated. The higher conductivity exhibited by ceramics with

FIGURE 7 | Polarization and strain vs. electric field for (A) $x = 0$; (B) $x = 0.5$ mol.%; (C) 0.75 mol.%; and (D) $x = 1$ mol.%.
$x > 1$ mol.% leads to rounded polarization ($P$) vs. electric field ($E$) loops, with remanent polarization ($P_r$) higher than maximum polarization ($P_{\text{max}}$) which suggest high leakage current, Figure 6. Therefore, it is concluded that samples with $x > 1$ mol.% are unsuitable for large field measurements without further processing efforts to increase density and increase resistivity.

Figure 7 shows polarization and strain vs. electric field loops for samples $(1-x)K_0.4Na_0.6NbO_3-xBiFeO_3$ with 0–1 mol.%. Ceramics with $x = 0.5$ mol.% also exhibited high loss and hence the value of $P_r$ is meaningless but samples with $x = 0.75$ and 1 mol.% exhibited well saturated loops with a high $P_r$ of $\sim 28 \mu C/cm^2$ and low coercive field ($E_C$) of $<1$ kV/mm. It was also noted that the $P-E$ loops for $x = 0.75$ and 1 mol.% are square. According to Haertling and Zimmer (1966), the degree of squareness ($R_{sq}$) of a $P-E$ loop can be calculated from the empirical formula introduced in Eq. 1, which for an ideal square loop is equal to 2.

$$R_{sq} = \frac{P_r}{P_s} + \frac{P_{1.1}E_C}{P_r}$$  \hspace{1cm} (1)

where “$P_s$” is saturation polarization and $P_{1.1}E_C$ is the polarization at 1.1 times of coercive field ($E_C$).

Samples with $x = 0.75$ and 1 mol.% exhibited $R_{sq} = 1.94$ and 1.95, respectively, which is closer to the ideal value of 2, indicating uniform grain size and better homogeneity (Haertling, 1999). The strain was observed to increase from 0.06 to 0.09% with increase in $x$ from 0 to 1 mol.% at an applied $E = 4$ kV/mm.

Figure 8A shows that well saturated $P-E$ loops are obtained at an electric field of 2 kV/mm for optimized compositions with $x = 1$ mol.%. The coercive field was estimated to be 0.8 kV/mm from current (I) vs. $E$ curve (Figure 8B), where a sharp peak was observed at the point of switching. The sharp peaks are indicative of well-defined coercive fields because of instantaneous domain switching, which is consistent with the square loops observed for these samples. S–E loops with peak to peak strain of 0.08% at...
E = 2 kV/mm are shown in Figure 8C. However, for practical applications, only a positive strain of 0.05% is useful. The negative strain in S–E loops is indicative of long-range ferroelectric order, consistent with the P–E loops. Strain values are influenced by both intrinsic and extrinsic factors (Donnelly et al., 2007). The extrinsic contributions are mainly dominated by domain wall motion, which due to low coercive field contributes at lower electric field. The optimum $d^{*}_{33}$ value (250 pm/V) is therefore, observed at 2 kV/mm and further increase in electric field does not increase $d^{*}_{33}$, as shown in Figure 8D.

$(1-x)K_{0.4}Na_{0.6}NbO_{3}-xBiFeO_{3}$ ceramics have optimized piezoelectric properties at RT for ceramics with $x = 1$ mol.% ($d_{33} = 182$ pC/N, $d^{*}_{33} = 250$ pm/V, and $k_p = 50\%$). However, of equal importance for application are the temperature dependent of properties.

$k_p$ as a function of temperature for the sample with $x = 1$ mol.% is shown in Figure 9 which is stable up to 90°C with a variation of $\sim$5% and then linearly decreased at temperatures $>100^\circ$C to $\sim$50% of its efficiency at 300°C. $T_{O-T} = 108^\circ$C, therefore, it can be concluded that $k_p$ is stable in the orthorhombic state, but degradation occurs when the structure changes to tetragonal symmetry (Khesro et al., 2016b). Though the reason of this degradation is unclear at this point, however it may be possible that the samples starts depoling at the onset of the phase transition which results in lower values of $k_p$ as the temperature is increased.

Figure 10A shows P–E loops at selected temperatures from 22 to 90°C. The coercive field decreased with increase in temperature, associated with easy domain switching at higher temperatures but the maximum polarization remains unchanged. Figure 10B shows the corresponding bipolar S–E loops, which reveal a limited temperature dependence of the field-induced strain. The change in positive strain is about 15% from 22 to 75°C. With increasing temperature, as the phase transition is approached there are significant changes on both P–E and S–E responses, as illustrated in Figures 10C–D, respectively. In the
CONCLUSION

An investigation of the (1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3 system revealed that dense ceramics can be obtained for x ≤ 1 mol.%. Piezoelectric properties were enhanced as BiFeO_3 content increased to 1%, beyond which the piezoelectric properties degraded. The degradation in properties was associated with poor densification during sintering. Optimum properties were obtained for ceramics with x = 1 mol.% (d_33 = 182 PC/N, d_31^T = 250 pm/V, and k_p = 50%). Though the composition has a high T_C = 355°C, stability is limited by T_O-T (108°C). The sample is stable in orthorhombic phase with k_p showing a variation of only ~5% from RT–90°C. The strain-electric field curves (d_33^T) also showed stability RT–75°C, provided a variation of 15% is considered acceptable. At the onset of T_O-T, large variations in piezoelectric coefficients are observed. The piezoelectric coefficients are not stable in tetragonal phase and a continuous degradation is observed as T_C is approached. This study concludes that temperature stability in a limited range can be achieved in (1-x)K_{0.5}Na_{0.5}NbO_3-xBiFeO_3 as long as T_O-T is ~100–120°C (Khesro, 2016).

DATA AVAILABILITY STATEMENT

The datasets generated for this study are available on request to the corresponding author.

AUTHOR CONTRIBUTIONS

AK performed all the experimental work and wrote the manuscript. IR and DW supervised the work. FH and RM helped with processing of ceramics. GW helped with the rietveld refinements. AF helped with strain measurements. All authors provided critical feedback and contributed to the final manuscript.

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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